

COMUNE DI CASTEL MAGGIORE

3° SETTORE LL. PP. E AMBIENTE

NUOVO POLO SCOLASTICO

PROGETTO ESECUTIVO ai sensi del DPR 207/2010



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Tabulato di calcolo
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SCALA

TAVOLA

SR.08

DATA Dicembre 2017



Software e Servizi
per l'Ingegneria s.r.l.

PRO_SAP

PROfessional **S**tructural **A**nalysis **P**rogram

Relazione di calcolo strutturale impostata e redatta secondo le modalità previste nel D.M. 14 Gennaio 2008 cap. 10 “Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo”.

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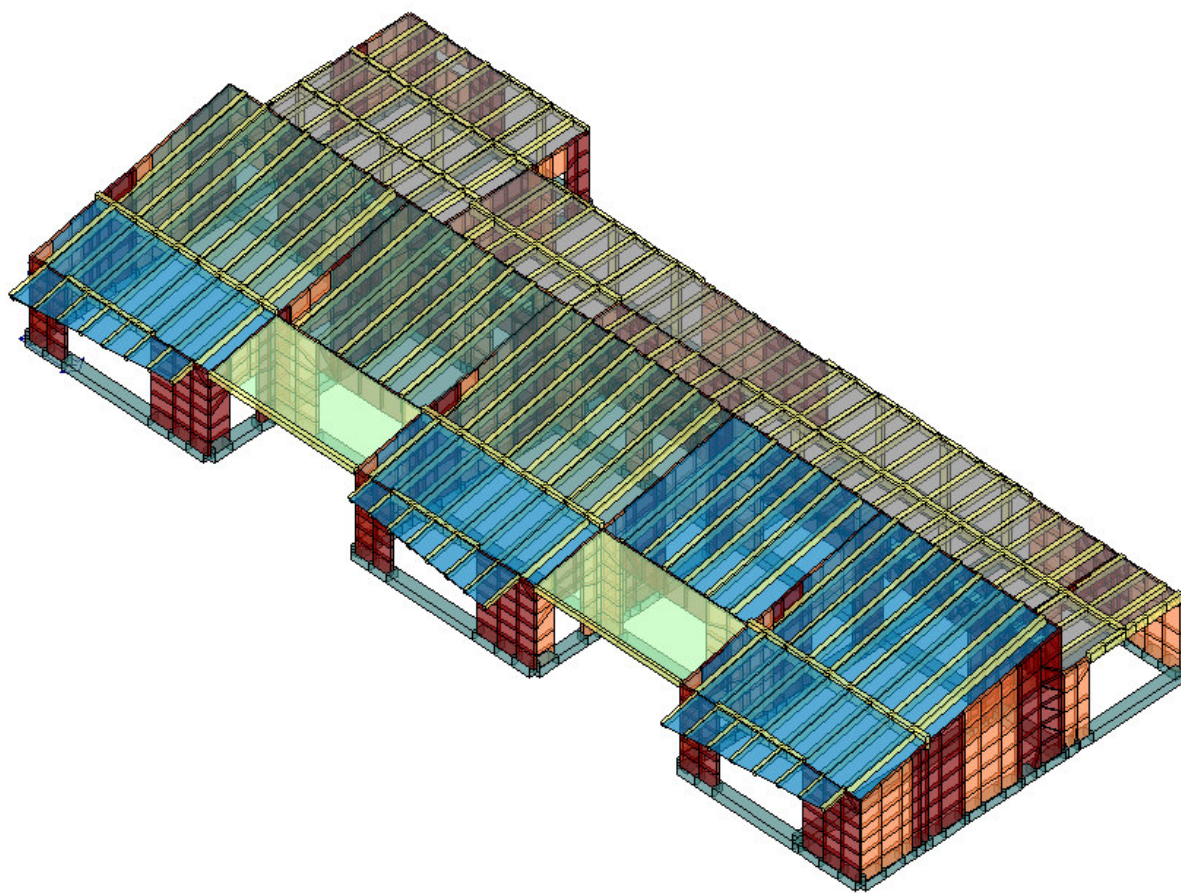
D.M. 14/01/08 cap. 10.2 Affidabilità dei codici utilizzati
<http://www.2si.it/software/Affidabilità.htm>

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INTESTAZIONE E CONTENUTI DELLA RELAZIONE

Progetto



Contenuti della relazione:

RELAZIONE DI CALCOLO STRUTTURALE

- *Origine e Caratteristiche dei Codici di Calcolo*
- *Affidabilità dei codici utilizzati*
- *Validazione dei codici*
- *Tipo di analisi svolta*
- *Modalità di presentazione dei risultati*
- *Informazioni generali sull'elaborazione*
- *Giudizio motivato di accettabilità dei risultati*

STAMPA DEI DATI DI INGRESSO

- *Normative prese a riferimento*
- *Criteri adottati per le misure di sicurezza*
- *Criteri seguiti nella schematizzazione della struttura, dei vincoli e delle sconnessioni*
- *Interazione tra terreno e struttura*
- *Legami costitutivi adottati per la modellazione dei materiali e dei terreni*
- *Schematizzazione delle azioni, condizioni e combinazioni di carico*
- *Metodologie numeriche utilizzate per l'analisi strutturale*
- *Metodologie numeriche utilizzate per la progettazione e la verifica degli elementi strutturali*

STAMPA DEI RISULTATI

RELAZIONE DI CALCOLO STRUTTURALE

Premessa

La presente relazione di calcolo strutturale, in conformità al §10.1 del DM 14/01/08, è comprensiva di una descrizione generale dell'opera e dei criteri generali di analisi e verifica. Segue inoltre le indicazioni fornite al §10.2 del DM stesso per quanto concerne analisi e verifiche svolte con l'ausilio di codici di calcolo.

Descrizione generale dell'opera

Descrizione generale dell'opera	
Fabbricato ad uso	
Ubicazione	Comune di CASTEL MAGGIORE (BO) (Regione EMILIA-ROMAGNA)
	Località CASTEL MAGGIORE (BO)
	Longitudine 11.363, Latitudine 44.575
Numero di piani	Fuori terra
	Interrati
le dimensioni dell'opera in pianta sono racchiuse in un rettangolo di dimensioni 39,8X18,8 m	
Tipo di fondazione	Travi rovesce 50X40

Parametri della struttura			
Classe d'uso	Vita Vn [anni]	Coeff. Uso	Periodo Vr [anni]
III	50.0	1.5	75.0

Fattore di struttura

Q=2

Quadro normativo di riferimento adottato

Le norme ed i documenti assunti quale riferimento per la progettazione strutturale vengono indicati di seguito. Nel capitolo "normativa di riferimento" è comunque presente l'elenco completo delle normative disponibili.

Progetto-verifica degli elementi	
Progetto cemento armato	D.M. 14-01-2008
Progetto acciaio	D.M. 14-01-2008
Progetto legno	D.M. 14-01-2008
Progetto muratura	D.M. 14-01-2008
Azione sismica	
Norma applicata per l'azione sismica	D.M. 14-01-2008

Azioni di progetto sulla costruzione

Nei capitoli "modellazione delle azioni" e "schematizzazione dei casi di carico" sono indicate le azioni sulla costruzioni.

Nel prosieguo si indicano tipo di analisi strutturale condotta (statico,dinamico, lineare o non lineare) e il metodo adottato per la risoluzione del problema strutturale nonché le metodologie seguite per la verifica o per il progetto-verifica delle sezioni. Si riportano le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti; le configurazioni studiate per la struttura in esame **sono risultate effettivamente esaustive per la progettazione-verifica.**

La verifica della sicurezza degli elementi strutturali avviene con i metodi della scienza delle costruzioni. L'analisi strutturale è condotta con il metodo degli spostamenti per la valutazione dello stato tensodeformativo indotto da carichi statici. L'analisi strutturale è condotta con il metodo dell'analisi modale e dello spettro di risposta in termini di accelerazione per la valutazione dello stato tensodeformativo indotto da carichi dinamici (tra cui quelli di tipo sismico).

L'analisi strutturale viene effettuata con il metodo degli elementi finiti. Il metodo sopraindicato si basa sulla schematizzazione della struttura in elementi connessi solo in corrispondenza di un numero prefissato di punti denominati nodi. I nodi sono definiti dalle tre coordinate cartesiane in un sistema di riferimento globale. Le incognite del problema (nell'ambito del metodo degli spostamenti) sono le componenti di spostamento dei nodi riferite al sistema di riferimento globale (traslazioni secondo X, Y, Z, rotazioni attorno X, Y, Z). La soluzione del problema si ottiene con un sistema di equazioni algebriche lineari i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati ai nodi:

$K \cdot u = F$ dove
K = matrice di rigidezza
u = vettore spostamenti nodali
F = vettore forze nodali

Dagli spostamenti ottenuti con la risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni di ogni elemento, riferite generalmente ad una terna locale all'elemento stesso.

Il sistema di riferimento utilizzato è costituito da una terna cartesiana destrorsa XYZ. Si assume l'asse Z verticale ed orientato verso l'alto.

Gli elementi utilizzati per la modellazione dello schema statico della struttura sono i seguenti:

• Elemento tipo TRUSS	(biella-D2)
• Elemento tipo BEAM	(trave-D2)
• Elemento tipo MEMBRANE	(membrana-D3)
• Elemento tipo PLATE	(piastra-guscio-D3)
• Elemento tipo BOUNDARY	(molla)
• Elemento tipo STIFFNESS	(matrice di rigidità)
• Elemento tipo BRICK	(elemento solido)
• Elemento tipo SOLAIO	(macro elemento composto da più membrane)

Modello numerico

In questa parte viene descritto il modello numerico utilizzato (o i modelli numerici utilizzati) per l'analisi della struttura. La presentazione delle informazioni deve essere, coerentemente con le prescrizioni del paragrafo 10.2 delle NTC-08, tale da garantirne la leggibilità, la corretta interpretazione e la riproducibilità

Tipo di analisi strutturale	
Statica lineare	SI
Statica non lineare	NO
Sismica statica lineare	NO
Sismica dinamica lineare	SI
Sismica statica non lineare (prop. masse)	NO
Sismica statica non lineare (prop. modo)	NO
Sismica statica non lineare (triangolare)	NO
Non linearità geometriche (fattore P delta)	NO

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Informazioni sul codice di calcolo	
Titolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2017-11-179)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara
Dati utente finale:	***** COMPLETARE *****
Codice Utente:	***** COMPLETARE *****
Codice Licenza:	Licenza dsi4773

Un attento esame preliminare della documentazione a corredo del software **ha consentito di valutarne l'affidabilità e soprattutto l'idoneità al caso specifico**. La documentazione, fornita dal produttore e distributore del software, contiene una esauriente descrizione delle basi teoriche e degli algoritmi impiegati, l'individuazione dei campi d'impiego, nonché casi prova interamente risolti e commentati, corredati dei file di input necessari a riprodurre l'elaborazione:

Affidabilità dei codici utilizzati	
2S.I. ha verificato l'affidabilità e la robustezza del codice di calcolo attraverso un numero significativo di casi prova in cui i risultati dell'analisi numerica sono stati confrontati con soluzioni teoriche. E' possibile reperire la documentazione contenente alcuni dei più significativi casi trattati al seguente link: http://www.2si.it/Software/Affidabilità.htm	

Modellazione della geometria e proprietà meccaniche:

nodi	1738
elementi D2 (per aste, travi, pilastri...)	568
elementi D3 (per pareti, platee, gusci...)	1307
elementi solaio	184
elementi solidi	0
Dimensione del modello strutturale [cm]:	
X min =	0.00
Xmax =	3950.00
Ymin =	-166.35
Ymax =	1800.00
Zmin =	0.00
Zmax =	546.00
Strutture verticali:	

Elementi di tipo asta	NO
Pilastri	SI
Pareti	SI
Setti (a comportamento membranale)	NO
Strutture non verticali:	
Elementi di tipo asta	NO
Travi	SI
Gusci	NO
Membrane	NO
Orizzontamenti:	
Solai con la proprietà piano rigido	NO
Solai senza la proprietà piano rigido	SI
Tipo di vincoli:	
Nodi vincolati rigidamente	NO
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	SI
Fondazioni di tipo platea	NO
Fondazioni con elementi solidi	NO

Modellazione delle azioni

Si veda il capitolo **“Schematizzazione dei casi di carico”** per le informazioni necessarie alla comprensione ed alla ricostruzione delle azioni applicate al modello numerico, coerentemente con quanto indicato nella parte *“2.6. Azioni di progetto sulla costruzione”*.

Combinazioni e/o percorsi di carico

Si veda il capitolo **“Definizione delle combinazioni”** in cui sono indicate le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti.

Combinazioni dei casi di carico

APPROCCIO PROGETTUALE	Approccio 2
Tensioni ammissibili	NO
SLU	SI
SLV (SLU con sisma)	SI
SLC	NO
SLD	SI
SLO	SI
SLU GEO A2 (per approccio 1)	NO
SLU EQU	NO
Combinazione caratteristica (rara)	SI
Combinazione frequente	SI
Combinazione quasi permanente (SLE)	SI
SLA (accidentale quale incendio)	SI

Principali risultati

I risultati devono costituire una sintesi completa ed efficace, presentata in modo da riassumere il comportamento della struttura, per ogni tipo di analisi svolta.

2.8.1. Risultati dell'analisi modale

Viene riportato il tipo di analisi modale condotta, restituiti i risultati della stessa e valutate le informazioni desumibili in merito al comportamento della struttura.

2.8.2. Deformate e sollecitazioni per condizioni di carico

Vengono riportati i principali risultati atti a descrivere il comportamento della struttura, in termini di stati di sollecitazione e di deformazione generalizzata, distinti per condizione elementare di carico o per combinazioni omogenee delle stesse.

2.8.3. Involuppo delle sollecitazioni maggiormente significative. L'analisi e la restituzione degli involuppi (nelle combinazioni considerate agli SLU e agli SLE) delle caratteristiche di sollecitazione devono essere finalizzate alla valutazione dello stato di sollecitazione nei diversi elementi della struttura.

2.8.4. Reazioni vincolari

Vengono riportate le reazioni dei vincoli nelle singole condizioni di carico e/o nelle combinazioni considerate.

2.8.5. Altri risultati significativi

Nella presente parte vengono riportati tutti gli altri risultati che il progettista ritiene di interesse per la descrizione e la comprensione del/i modello/i e del comportamento della struttura.

La presente relazione, oltre ad illustrare in modo esaustivo i dati in ingresso ed i risultati delle analisi in forma tabellare, riporta una serie di

immagini:

per i dati in ingresso:

- modello solido della struttura
- numerazione di nodi e ed elementi
- configurazioni di carico statiche
- configurazioni di carico sismiche con baricentri delle masse e eccentricità

per le combinazioni più significative (statisticamente più gravose per la struttura)

- configurazioni deformate
- diagrammi e involuppi delle azioni interne
- mappe delle tensioni
- reazioni vincolari
- mappe delle pressioni sul terreno

per il progetto-verifica degli elementi

- diagrammi di armatura
- percentuali di sfruttamento
- mappe delle verifiche più significative per i vari stati limite

Informazioni generali sull'elaborazione e giudizio motivato di accettabilità dei risultati.

Il programma prevede una serie di controlli automatici (check) che consentono l'individuazione di errori di modellazione. Al termine dell'analisi un controllo automatico identifica la presenza di spostamenti o rotazioni abnormi. Si può pertanto asserire che l'elaborazione sia corretta e completa. I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.) .

Verifiche agli stati limite ultimi

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità ed i criteri seguiti per valutare la sicurezza della struttura nei confronti delle possibili situazioni di crisi ed i risultati delle valutazioni svolte. In via generale, oltre alle verifiche di resistenza e di spostamento, devono essere prese in considerazione verifiche nei confronti dei fenomeni di instabilità, locale e globale, di fatica, di duttilità, di degrado.

Verifiche agli stati limite di esercizio

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità seguite per valutare l'affidabilità della struttura nei confronti delle possibili situazioni di perdita di funzionalità (per eccessive deformazioni, fessurazioni, vibrazioni, etc.) ed i risultati delle valutazioni svolte.

RELAZIONE SUI MATERIALI

Il capitolo Materiali riporta informazioni esaustive relative all'elenco dei materiali impiegati e loro modalità di posa in opera e ai valori di calcolo.

NORMATIVA DI RIFERIMENTO

1. D.Min. Infrastrutture Min. Interni e Prot. Civile 14 Gennaio 2008 e allegate "Norme tecniche per le costruzioni".
2. D.Min. Infrastrutture e trasporti 14 Settembre 2005 e allegate "Norme tecniche per le costruzioni".
3. D.M. LL.PP. 9 Gennaio 1996 "Norme tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato, normale e precompresso e per le strutture metalliche".
4. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>".
5. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche per le costruzioni in zone sismiche".
6. Circolare 4/07/96, n.156AA.GG./STC. istruzioni per l'applicazione delle "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>" di cui al D.M. 16/01/96.
7. Circolare 10/04/97, n.65AA.GG. istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. 16/01/96.
8. D.M. LL.PP. 20 Novembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
9. Circolare 4 Gennaio 1989 n. 30787 "Istruzioni in merito alle norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
10. D.M. LL.PP. 11 Marzo 1988 "Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione".
11. D.M. LL.PP. 3 Dicembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo delle costruzioni prefabbricate".
12. UNI 9502 - Procedimento analitico per valutare la resistenza al fuoco degli elementi costruttivi di conglomerato cementizio armato, normale e precompresso - edizione maggio 2001
13. Ordinanza del Presidente del Consiglio dei Ministri n. 3274 del 20 marzo 2003 "Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica" e successive modificazioni e integrazioni.
14. UNI EN 1990:2006 13/04/2006 Eurocodice 0 - Criteri generali di progettazione strutturale.
15. UNI EN 1991-1-1:2004 01/08/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-1: Azioni in generale - Pesi per unità di volume, pesi propri e sovraccarichi per gli edifici.
16. UNI EN 1991-2:2005 01/03/2005 Eurocodice 1 - Azioni sulle strutture - Parte 2: Carichi da traffico sui ponti.
17. UNI EN 1991-1-3:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-3: Azioni in generale - Carichi da neve.
18. UNI EN 1991-1-4:2005 01/07/2005 Eurocodice 1 - Azioni sulle strutture - Parte 1-4: Azioni in generale - Azioni del vento.
19. UNI EN 1991-1-5:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-5: Azioni in generale - Azioni termiche.
20. UNI EN 1992-1-1:2005 24/11/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
21. UNI EN 1992-1-2:2005 01/04/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-2: Regole generali - Progettazione strutturale contro l'incendio.
22. UNI EN 1993-1-1:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-1: Regole generali e regole per gli edifici.
23. UNI EN 1993-1-8:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-8: Progettazione dei collegamenti.
24. UNI EN 1994-1-1:2005 01/03/2005 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
25. UNI EN 1994-2:2006 12/01/2006 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 2: Regole generali e regole per i ponti.
26. UNI EN 1995-1-1:2005 01/02/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1: Regole generali - Regole comuni e regole per gli edifici.
27. UNI EN 1995-2:2005 01/01/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 2: Ponti.
28. UNI EN 1996-1-1:2006 26/01/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 1-1: Regole generali per strutture di muratura armata e non armata.
29. UNI EN 1996-3:2006 09/03/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 3: Metodi di calcolo semplificato per strutture di muratura non armata.
30. UNI EN 1997-1:2005 01/02/2005 Eurocodice 7 - Progettazione geotecnica - Parte 1: Regole generali.
31. UNI EN 1998-1:2005 01/03/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 1: Regole generali, azioni sismiche e regole per gli edifici.
32. UNI EN 1998-3:2005 01/08/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 3: Valutazione e adeguamento degli edifici.
- UNI EN 1998-5:2005 01/01/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.

NOTA sul capitolo "normativa di riferimento": riporta l'elenco delle normative implementate nel software. Le norme utilizzate per la struttura oggetto della presente relazione sono indicate nel precedente capitolo "RELAZIONE DI CALCOLO STRUTTURALE" "ANALISI E VERIFICHE SVOLTE CON L'AUSILIO DI CODICI DI CALCOLO". Laddove nei capitoli successivi vengano richiamate norme antecedenti al DM 14.01.08 è dovuto o a progettazione simulata di edificio esistente o ad applicazione del punto 2.7 del DM 14.01.08

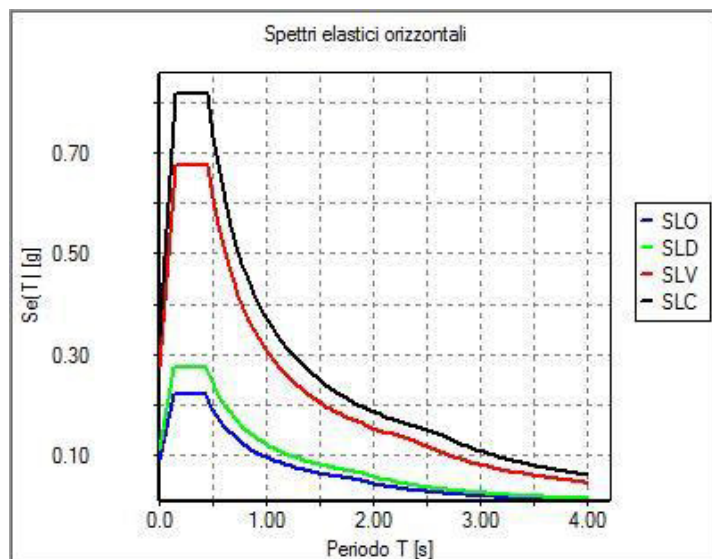


Fig.1 Spettri elastici Orizzontali

CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

<i>Young</i>	modulo di elasticità normale
<i>Poisson</i>	coefficiente di contrazione trasversale
<i>G</i>	modulo di elasticità tangenziale
<i>Gamma</i>	peso specifico
<i>Alfa</i>	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck Fctm	resistenza caratteristica cubica resistenza media a trazione semplice
2	acciaio	Ft Fy Fd Fdt Sadm Sadmt	tensione di rottura a trazione tensione di snervamento resistenza di calcolo resistenza di calcolo per spess. t>40 mm tensione ammissibile tensione ammissibile per spess. t>40 mm
3	muratura	Resist. Fk Resist. Fvko	resistenza caratteristica a compressione resistenza caratteristica a taglio
4	legno	Resist. fc0k Resist. ft0k Resist. fmk Resist. fvk Modulo E0,05 Lamellare	Resistenza caratteristica (tensione amm. per REGLES) per compressione Resistenza caratteristica (tensione amm. per REGLES) per trazione Resistenza caratteristica (tensione amm. per REGLES) per flessione Resistenza caratteristica (tensione amm. per REGLES) per taglio Modulo elastico parallelo caratteristico lamellare o massiccio

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Modellazione di strutture in c.a.

Test N°	Titolo
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE T.A. DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
51	FATTORE DI STRUTTURA
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
54	PARETI IN C.A. SNELLE IN ZONA SISMICA
80	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
120	PROGETTO E VERIFICA DI TRAVI PREM

Modellazione di strutture in acciaio

Test N°	Titolo
55	VERIFICA DI STABILITA' DI ASTE COMPRESSE IN ACCIAIO – METODO OMEGA
56	LUCE LIBERA DI TRAVI E ASTE IN ACCIAIO
57	LUCE LIBERA DI COLONNE IN ACCIAIO
58	SVERGOLAMENTO DI TRAVI IN ACCIAIO
59	FATTORE DI STRUTTURA
60	ACCIAIO D.M.2008
61	ACCIAIO EC3
62	GERARCHIA RESISTENZE STRUTTURE IN ACCIAIO
63	STABILITA' DI ASTE COMPOSTE IN ACCIAIO
73	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA IRRIGIDIMENTI TRASVERSALI
74	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI UN PIATTO DI RINFORZO SALDATO ALL'ANIMA DELLA COLONNA
75	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI DUE PIATTI DI RINFORZO SALDATI ALL'ANIMA DELLA COLONNA
76	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A DUE VIE SU ALI COLONNA
77	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A UNA VIA CON DUE COMBINAZIONI DI CARICO
78	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO SU ANIMA SENZA RINFORZI A QUATTRO FILE DI BULLONI DI CUI UNA SU PIASTRA INFERIORE E UNA SU PIASTRA SUPERIORE
79	VERIFICA DELLA PIASTRA NODO TRAVE COLONNA
85	TELAIO ACCIAIO: CONTROVENTI CONCENTRICI

Modellazione di strutture in muratura

Test N°	Titolo
81	ANALISI PUSHOVER DI UNA STRUTTURA IN MURATURA

84	ANALISI ELASTO PLASTICA INCREMENTALE, PARETE IN MURATURA
86	VERIFICA NON SISMICA DELLE MURATURE (D.M. 87 TA)
87	VERIFICA NON SISMICA DELLE MURATURE (D.M. 2005 SL)
88	FATTORE DI STRUTTURA

Modellazione di strutture in legno

Test N°	Titolo
17	SOLAIO: MISTO LEGNO-CALCESTRUZZO
89	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
90	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
91	FATTORE DI STRUTTURA
92	VERIFICHE EC5
93	SNELLEZZE EC5
94	VERIFICA AL FUOCO DI STRUTTURE IN LEGNO SECONDO EC5
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI
119	PROGETTO E VERIFICA DI SOLAI IN MATERIALE XLAM

Id	Tipo / Note		Young	Poisson	G	Gamma	Alfa
		daN/cm2	daN/cm2		daN/cm2	daN/cm3	
3	Calcestruzzo Classe C28/35		3.260e+05	0.20	1.358e+05	2.50e-03	1.00e-05
	Rck	350.0					
	fctm	28.4					
48	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)		8.052e+04	0.0	6900.0	3.80e-04	0.0
	Modulo E0,05		8.052e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareSi						
	Resist. fc0k	1.0					
	Resist. ft0k	1.0					
	Resist. fmk	1.0					
	Resist. fvk	1.0					
49	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)		8.052e+04	0.0	6900.0	3.80e-04	0.0
	Modulo E0,05		8.052e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareSi						
	Resist. fc0k	1.0					
	Resist. ft0k	1.0					
	Resist. fmk	1.0					
	Resist. fvk	1.0					
50	legno lamellare omogeneo GL24h E = 1.150e+05		1.150e+05	0.0	6500.0	4.20e-04	0.0
	Modulo E0,05		9.599e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareSi						
	Resist. fc0k	240.0					
	Resist. ft0k	192.0					
	Resist. fmk	240.0					
	Resist. fvk	35.0					

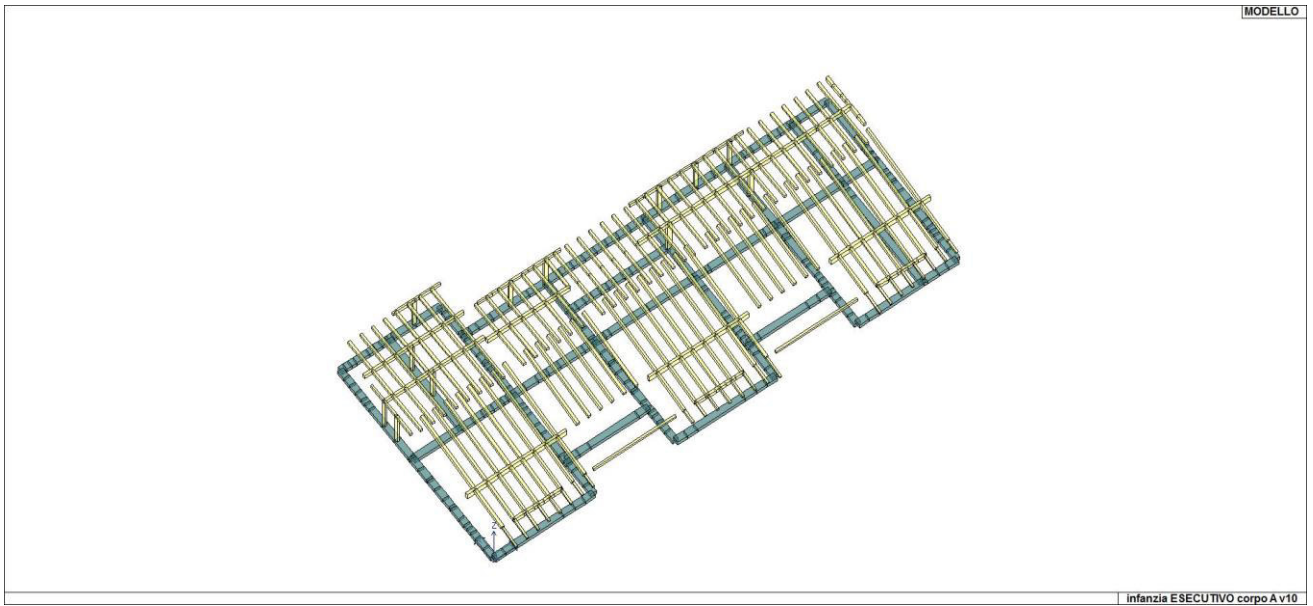


Fig.2 Materiali D2

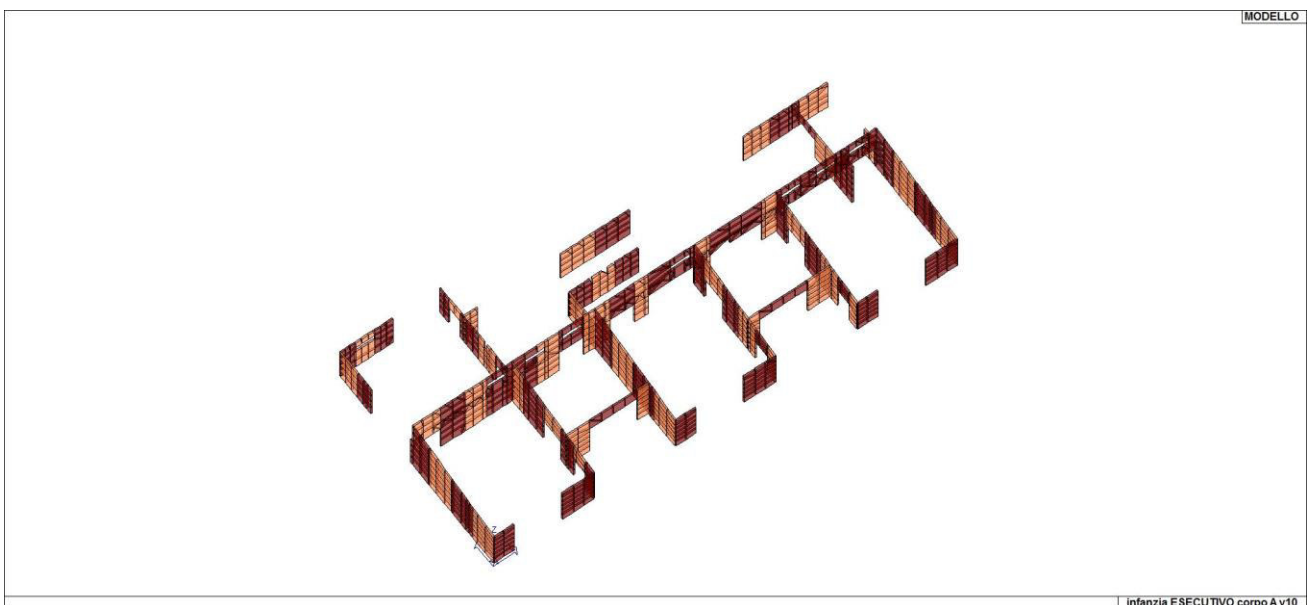


Fig.3 Materiali D3

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SR_08 Tabulato di Calcolo Scuola dell'Infanzia Corpo A

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Pag. **61** a **239**

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Pag. 74 a 239

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[illegible]

Pag. 95 a 239

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XLAM	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
	No	No	No	No	No	No
	No	No	No	No	No	No
	No	No	No	No	No	No
	No	No	No	No	No	No
	No	No	No	No	No	No
	No	No	No			

MODELLAZIONE DELLE SEZIONI

LEGENDA TABELLA DATI SEZIONI

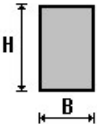
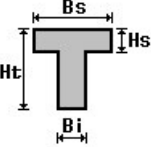
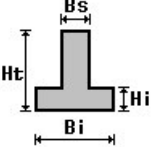
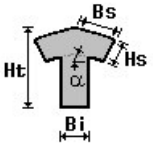
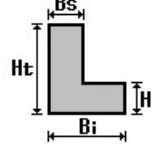
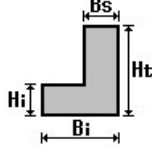
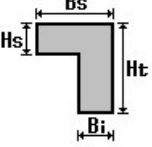
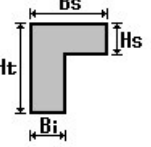
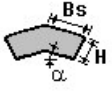
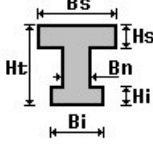
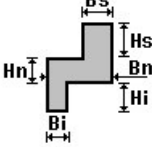
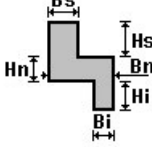
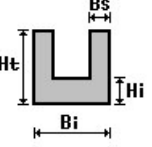
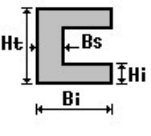
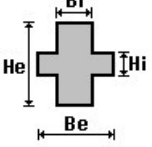
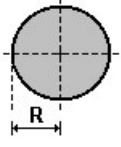
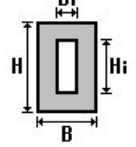
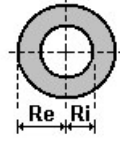
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

- 1 sezione di tipo generico
- 2 profilati semplici
- 3 profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

 rettangolare	 a T	 a T rovescia	 a T di colmo	 a L	 a L specchiata
 a L specchiata rovescia	 a L rovescia	 a L di colmo	 a doppio T	 a quattro specchiata	 a quattro
 a U	 a C	 a croce	 circolare	 rettangolare cava	 circolare cava

Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
1	CARATTERISTICHE GEOMETRICHE E INERZIALI
45	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
49	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
50	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
51	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
104	ANALISI DI RESISTENZA AL FUOCO

Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	Rettangolare: b=20 h=60	1200.00	1000.00	1000.00	1.264e+05	4.000e+04	3.600e+05	4000.00	1.200e+04	6000.00	1.800e+04
2	Rettangolare: b=20 h=28	560.00	466.67	466.67	4.187e+04	1.867e+04	3.659e+04	1866.67	2613.33	2800.00	3920.00
3	Rettangolare: b=14 h=40	560.00	466.67	466.67	2.852e+04	9146.67	7.467e+04	1306.67	3733.33	1960.00	5600.00
4	Rettangolare: b=14 h=32	448.00	373.33	373.33	2.120e+04	7317.33	3.823e+04	1045.33	2389.33	1568.00	3584.00
5	Rettangolare: b=20 h=52	1040.00	866.67	866.67	1.051e+05	3.467e+04	2.343e+05	3466.67	9013.33	5200.00	1.352e+04
6	Rettangolare: b=20 h=40	800.00	666.67	666.67	7.307e+04	2.667e+04	1.067e+05	2666.67	5333.33	4000.00	8000.00
7	Rettangolare: b=50 h=40	2000.00	1666.67	1666.67	5.498e+05	4.167e+05	2.667e+05	1.667e+04	1.333e+04	2.500e+04	2.000e+04
8	Rettangolare: b=16 h=20	320.00	266.67	266.67	1.408e+04	6826.67	1.067e+04	853.33	1066.67	1280.00	1600.00
9	Rettangolare: b=16 h=24	384.00	320.00	320.00	1.901e+04	8192.00	1.843e+04	1024.00	1536.00	1536.00	2304.00
10	Rettangolare: b=20 h=40	800.00	666.67	666.67	7.307e+04	2.667e+04	1.067e+05	2666.67	5333.33	4000.00	8000.00

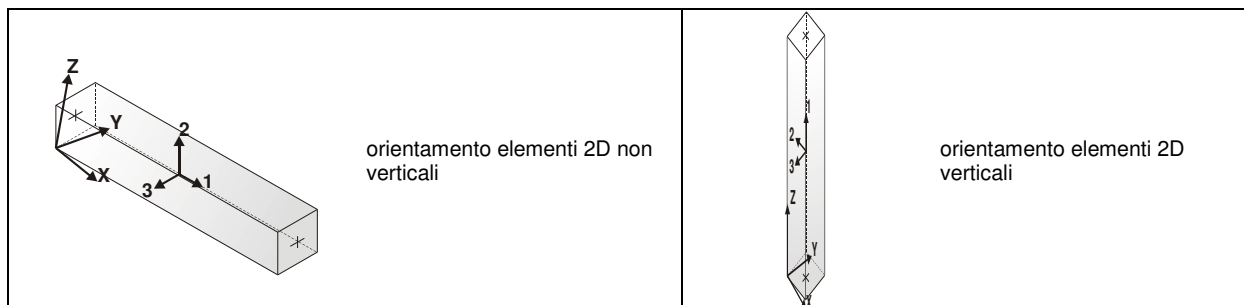
MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

TABELLA DATI TRAVI

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
2	TRAVI A UNA CAMPATA
3	TRAVE A PIU' CAMPATE
4	TRAVE A UNA CAMPATA SU TERRENO ALLA WINKLER
5	TRAVI SU TERRENO ALLA WINKLER CON CARICO TRASVERSALE
6	TELAI PIANI CON CERNIERE ALLA BASE
7	TELAI PIANI CON INCASTRI ALLA BASE
11	STRUTTURE SOGGETTE A VARIAZIONI TERMICHE
12	STRUTTURE SU TERRENO ALLA WINKLER SOTTOPOSTE A CARICHI DISTRIBUITI TRIANGOLARI
21	DRILLING
24	TENSIONI E ROTAZIONI RISPETTO ALLA CORDA DI ELEMENTI TRAVE
27	FRECCIA DI ELEMENTI TRAVE
42	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
43	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
44	VERIFICA ALLE TA DI STRUTTURE IN C.A.
45	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
47	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
49	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
50	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
51	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
52	FATTORE DI STRUTTURA
53	SOVRARESISTENZE
54	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
56	VERIFICA DI STABILITA' DI ASTE COMPRESSE IN ACCIAIO – METODO OMEGA
57	LUCE LIBERA DI TRAVI E ASTE IN ACCIAIO
58	LUCE LIBERA DI COLONNE IN ACCIAIO
59	SVERGOLAMENTO DI TRAVI IN ACCIAIO
64	STABILITA' DI ASTE COMPOSTE IN ACCIAIO
73	VALUTAZIONE EFFETTO P- δ SU PILASTRATA
74	VALUTAZIONE EFFETTO P- δ SU TELAIO 3D
85	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
87	ANALISI ELASTO PLASTICA INCREMENTALE
88	ANALISI ELASTO PLASTICA INCREMENTALE
98	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
99	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
102	SNELLEZZE EC5
130	PROGETTO E VERIFICA DI TRAVI PREM

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Rotaz. gradi	Svincolo I	Svincolo J	Wink V daN/cm3	Wink O daN/cm3
1	Trave	773	547	50	6		000011	000011		
2	Trave	777	633	50	6		000011	000011		
3	Trave	779	667	50	6		000011	000011		
4	Trave	793	672	50	6		000011	000011		
5	Trave	794	674	50	6		000011	000011		
6	Trave	795	676	50	6		000011	000011		
7	Trave	796	717	50	6		000011	000011		
8	Trave	829	724	50	6		000011	000011		
9	Pilas.	1659	1643	50	4	90.00	000011	000011		
10	Trave	832	727	50	6		000011	000011		

11	Trave	834	731	50	6	000011	000011		
12	Trave	996	744	50	6	000011	000011		
13	Trave	997	1013	50	6	000011	000011		
14	Trave	1015	663	50	6	000011	000011		
15	Trave	1016	673	50	6	000011	000011		
16	Trave	360	1083	50	2	000011	000011		
17	Trave	1640	537	50	2	000011	000011		
18	Trave	1143	184	50	2	000011	000011		
19	Trave	1088	1138	50	2	000011	000011		
20	Trave	1087	1048	50	2	000011	000011		
21	Trave	263	1024	50	2	000011	000011		
22	Trave	199	1023	50	2	000011	000011		
23	Trave	196	1021	50	2	000011	000011		
24	Trave	172	1019	50	2	000011	000011		
25	Trave	1667	1018	50	2	000011	000011		
26	Trave	1664	1017	50	2	000011	000011		
27	Trave f.	419	1610	3	7			0.95	0.54
28	Trave	664	1131	50	5				
29	Trave	679	680	50	1				
30	Trave	761	767	50	1				
31	Trave	796	829	50	1				
32	Trave	1209	1535	50	4				
33	Trave	1531	1533	50	4				
34	Trave	1535	1536	50	4				
35	Trave	1533	1209	50	4				
36	Trave	1536	1246	50	4		000011		
37	Trave	1420	1198	50	4	000011			
38	Trave	979	1671	50	4	000011			
39	Trave	1111	677	50	5	000011			
40	Trave	1334	1143	50	5				
41	Trave	1469	1640	50	5	000011			
42	Trave	100	735	50	6				
43	Pilas.	1289	1292	50	4	000011	000011		
44	Trave	729	100	50	6				
45	Trave	1403	1662	50	4	000011			
46	Trave	1615	1611	50	5				
47	Trave	1664	1667	50	6				
48	Trave	1643	1664	50	6	000011			
49	Trave	1088	1656	50	6		000011		
50	Trave f.	1361	1619	3	7			0.95	0.54
51	Trave	666	664	50	5				
52	Trave f.	1248	1251	3	7			0.95	0.54
53	Trave	360	1334	50	5				
54	Trave	680	682	50	1				
55	Trave	767	773	50	1				
56	Pilas.	1319	1322	50	10	000011	000011		
57	Pilas.	1330	1334	50	10	000011	000011		
58	Trave	829	832	50	1				
59	Pilas.	1307	1315	50	4	000011	000011		
60	Trave	1198	1220	50	4				
61	Trave	1265	1098	50	4				
62	Trave	13	1322	50	5				
63	Trave	14	1469	50	5		000011		
64	Trave	843	1633	50	5		000011		
65	Trave	1643	1259	50	4		000011		
66	Trave	853	1043	50	5		000011		
67	Trave	1667	172	50	6				
68	Trave	1699	1023	50	6				
69	Trave f.	1627	1361	3	7			0.95	0.54
70	Trave f.	1370	1562	3	7			0.95	0.54
71	Trave	1003	360	50	5				
72	Trave	1671	1265	50	4				
73	Trave	677	13	50	5				
74	Trave	380	14	50	5				
75	Trave	850	843	50	5				
76	Trave f.	675	204	3	7			0.95	0.53
77	Trave	1006	853	50	5				
78	Trave f.	1619	419	3	7			0.95	0.54
79	Trave f.	1251	1263	3	7			0.95	0.54
80	Trave	682	689	50	1				
81	Trave	773	777	50	1				
82	Trave	832	834	50	1				
83	Trave	1220	1458	50	4				
84	Trave	1275	348	50	4				
85	Trave	172	196	50	6				
86	Trave f.	1638	1627	3	7			0.95	0.54

87	Trave f.	1602	1370	3	7				0.95	0.54
88	Trave	1025	1003	50	5					
89	Trave	391	380	50	5					
90	Trave	1640	850	50	5					
91	Trave	1473	1006	50	5					
92	Trave	1532	1275	50	4					
93	Trave f.	1382	1678	3	7				0.95	0.54
94	Trave	1662	1643	50	4					
95	Trave f.	1263	1269	3	7				0.95	0.54
96	Trave	689	710	50	1					
97	Trave	777	779	50	1					
98	Trave	834	996	50	1					
99	Trave	1230	1463	50	4					
100	Trave	1282	573	50	4					
101	Trave	196	1192	50	6					
102	Trave f.	1610	1602	3	7				0.95	0.54
103	Trave	1131	1025	50	5					
104	Trave	397	391	50	5					
105	Trave	1604	1473	50	5					
106	Trave	1098	1532	50	4					
107	Trave f.	1350	1382	3	7				0.95	0.54
108	Trave	1458	1230	50	4					
109	Trave	348	1282	50	4					
110	Trave f.	1396	1661	3	7				0.95	0.54
111	Trave f.	1269	1276	3	7				0.95	0.54
112	Trave	710	747	50	1					
113	Trave	779	793	50	1					
114	Trave	996	997	50	1					
115	Trave	1243	1468	50	4					
116	Trave	1292	808	50	4					
117	Trave	199	263	50	6					
118	Trave	1143	397	50	5					
119	Pilas.	1661	1662	50	4	90.00	000011	000011		
120	Trave	1611	1604	50	5					
121	Trave f.	1562	1350	3	7				0.95	0.54
122	Trave f.	1663	1396	3	7				0.95	0.54
123	Trave f.	148	1638	3	7				0.95	0.54
124	Trave	1463	1243	50	4					
125	Trave	1322	666	50	5					
126	Trave	573	758	50	4					
127	Trave f.	1659	1248	3	7				0.95	0.54
128	Trave	429	679	50	1		000011			
129	Trave	452	761	50	1		000011			
130	Trave	476	796	50	1		000011			
131	Trave f.	1276	1283	3	7				0.95	0.54
132	Trave	747	751	50	1					
133	Trave	793	794	50	1					
134	Pilas.	1206	1209	50	4		000011	000011		
135	Trave	997	1015	50	1					
136	Trave	135	1068	50	6					
137	Trave	1255	811	50	4					
138	Pilas.	1225	1230	50	4		000011	000011		
139	Trave	1068	1591	50	6			000011		
140	Pilas.	1247	1255	50	4		000011	000011		
141	Trave	1304	1083	50	4					
142	Trave	263	1087	50	6					
143	Trave f.	1666	1663	3	7				0.95	0.54
144	Trave f.	1661	1659	3	7				0.95	0.54
145	Trave	1468	1255	50	4					
146	Trave	808	1304	50	4					
147	Trave	758	1292	50	4					
148	Trave f.	1283	1288	3	7				0.95	0.54
149	Trave	751	757	50	1					
150	Trave	794	795	50	1					
151	Trave	1015	1016	50	1					
152	Trave	811	991	50	4			000011		
153	Trave	1315	184	50	4					
154	Trave	1087	1088	50	6					
155	Trave f.	1678	1666	3	7				0.95	0.54
156	Trave	1083	1093	50	4					
157	Trave	757	432	50	1			000011		
158	Trave	795	464	50	1			000011		
159	Trave	1016	488	50	1			000011		
160	Trave	184	943	50	4			000011		
161	Trave	1093	1315	50	4					
162	Trave	540	41	50	9		000011	000011		

163	Trave	1684	195	50	8		
164	Trave	283	661	50	8		
165	Trave	1689	648	50	8		
166	Trave	842	735	50	8		
167	Trave	1690	658	50	8		
168	Trave	1323	1531	50	4	000011	
169	Trave	1697	1068	50	8		
170	Trave	1688	718	50	8		
171	Trave	852	1022	50	8		
172	Trave	1686	698	50	8		
173	Trave	1687	712	50	8		
174	Trave	1008	729	50	8		
175	Trave	1685	695	50	8		
176	Trave	848	665	50	8		
177	Trave	735	135	50	6		
178	Pilas.	1270	1275	50	4	000011	000011
179	Trave	195	679	50	6	000011	000011
180	Trave	695	680	50	6	000011	000011
181	Trave	698	682	50	6	000011	000011
182	Trave	712	689	50	6	000011	000011
183	Trave	718	710	50	6	000011	000011
184	Trave	648	747	50	6	000011	000011
185	Trave	658	751	50	6	000011	000011
186	Trave	365	757	50	6	000011	000011
187	Trave	370	761	50	6	000011	000011
188	Trave	1020	767	50	6		000011
189	Trave	353	773	50	6	000011	000011
190	Trave	661	777	50	6	000011	000011
191	Trave	665	779	50	6	000011	000011
192	Trave	1022	793	50	6	000011	000011
193	Trave	400	794	50	6	000011	000011
194	Trave	494	795	50	6	000011	000011
195	Trave	809	796	50	6	000011	000011
196	Trave	720	829	50	6	000011	000011
197	Trave	725	832	50	6	000011	000011
198	Trave	729	834	50	6	000011	000011
199	Trave	735	996	50	6	000011	000011
200	Trave	1068	997	50	6	000011	000011
201	Trave	844	1015	50	6	000011	000011
202	Trave	846	1016	50	6	000011	000011
203	Trave	850	542	50	2	000011	000011
204	Trave	854	725	50	8		
205	Trave	273	400	50	8		
206	Trave	258	720	50	8		
207	Trave	670	494	50	8		
208	Trave	745	809	50	8		
209	Trave f.	678	79	3	7		0.97 0.55
210	Trave	1691	365	50	8		
211	Trave	1692	370	50	8		
212	Trave	1693	846	50	8		
213	Trave	1694	1020	50	8		
214	Trave	1695	844	50	8		
215	Trave	1696	353	50	8		
216	Trave	1138	1536	50	2	000011	000011
217	Trave	391	513	50	2	000011	000011
218	Trave	1048	1535	50	2	000011	000011
219	Trave	380	518	50	2	000011	000011
220	Trave	14	519	50	2	000011	000011
221	Trave	1322	1098	50	2	000011	000011
222	Trave	253	1088	50	2	000011	000011
223	Trave	226	1087	50	2	000011	000011
224	Trave	225	263	50	2	000011	000011
225	Trave	224	199	50	2	000011	000011
226	Trave	218	196	50	2	000011	000011
227	Trave	202	172	50	2	000011	000011
228	Trave	760	1667	50	2	000011	000011
229	Trave	759	1664	50	2	000011	000011
230	Trave	397	507	50	2	000011	000011
231	Trave	1615	468	50	2	000011	000011
232	Trave	478	1611	50	2	000011	000011
233	Trave	492	1604	50	2	000011	000011
234	Trave	774	1473	50	2	000011	000011
235	Trave	765	1006	50	2	000011	000011
236	Trave	763	853	50	2	000011	000011
237	Trave	1334	1093	50	2	000011	000011
238	Trave	677	458	50	2	000011	000011

239	Trave	13	1671	50	2	000011	000011
240	Trave	666	1532	50	2	000011	000011
241	Trave	664	348	50	2	000011	000011
242	Trave	552	568	50	2	000011	
243	Trave	776	569	50	2	000011	
244	Trave	775	570	50	2	000011	
245	Trave	565	571	50	2	000011	
246	Trave	792	572	50	2	000011	
247	Trave	785	1118	50	2	000011	
248	Trave	783	677	50	2	000011	000011
249	Trave	781	13	50	2	000011	000011
250	Trave	566	666	50	2	000011	000011
251	Trave	797	664	50	2	000011	000011
252	Trave	799	1131	50	2	000011	000011
253	Trave	801	1025	50	2	000011	000011
254	Trave	806	1003	50	2	000011	000011
255	Trave	567	360	50	2	000011	000011
256	Trave	816	1143	50	2	000011	000011
257	Trave	818	397	50	2	000011	000011
258	Trave	820	391	50	2	000011	000011
259	Trave	825	380	50	2	000011	000011
260	Trave	827	14	50	2	000011	000011
261	Trave	1010	850	50	2	000011	000011
262	Trave	1012	843	50	2	000011	000011
263	Trave	999	1640	50	2	000011	000011
264	Trave	1024	1533	50	2	000011	000011
265	Trave	1023	1531	50	2	000011	000011
266	Trave	1021	363	50	2	000011	000011
267	Trave	501	685	50	6	000011	000011
268	Trave	1134	197	50	6	000011	000011
269	Trave	554	721	50	6	000011	000011
270	Trave	575	311	50	6	000011	000011
271	Trave	588	239	50	6	000011	000011
272	Trave	10	278	50	6	000011	000011
273	Trave	11	762	50	6	000011	000011
274	Trave	641	807	50	6	000011	000011
275	Trave	642	788	50	6	000011	000011
276	Trave	586	815	50	6	000011	000011
277	Trave	15	814	50	6	000011	000011
278	Trave	585	791	50	6	000011	000011
279	Trave	1019	1529	50	2	000011	000011
280	Trave	568	811	50	2	000011	000011
281	Trave	569	418	50	2	000011	000011
282	Trave	570	428	50	2	000011	000011
283	Trave	571	443	50	2	000011	000011
284	Trave	572	448	50	2	000011	000011
285	Trave	1118	453	50	2	000011	000011
286	Trave	1131	573	50	2	000011	000011
287	Trave	1018	749	50	2	000011	000011
288	Trave	1017	309	50	2	000011	000011
289	Trave	1025	758	50	2	000011	000011
290	Trave	1043	1255	50	2	000011	000011
291	Trave	1169	1322	50	2	000011	000011
292	Trave	1172	1334	50	2	000011	000011
293	Trave	1003	808	50	2	000011	000011
294	Trave	1615	1195	50	2	000011	000011
295	Trave	1611	1198	50	2	000011	000011
296	Trave	1604	1458	50	2	000011	000011
297	Trave	1473	1230	50	2	000011	000011
298	Trave	1006	1463	50	2	000011	000011
299	Trave	853	1468	50	2	000011	000011
300	Trave	843	546	50	2	000011	000011
301	Trave	679	659	50	6	000011	000011
302	Trave	680	696	50	6	000011	000011
303	Trave	682	323	50	6	000011	000011
304	Trave	689	328	50	6	000011	000011
305	Trave	710	338	50	6	000011	000011
306	Trave	747	373	50	6	000011	000011
307	Trave	751	387	50	6	000011	000011
308	Trave	757	403	50	6	000011	000011
309	Trave	761	823	50	6	000011	000011
310	Trave	767	312	50	6	000011	000011
311	Trave	1017	1018	50	6		
312	Trave	1267	1017	50	6	000011	
313	Trave	1138	1375	50	6		000011
314	Trave	1018	1019	50	6		

315	Trave	1019	1021	50	6		
316	Trave	1021	1699	50	6		
317	Trave	1023	1024	50	6		
318	Trave	1024	1048	50	6		
319	Trave	1048	1138	50	6		
320	Trave f.	148	43	3	7	0.97	0.55
321	Trave f.	8	1166	3	7	0.95	0.54
322	Trave f.	1337	1392	3	7	0.95	0.53
323	Trave f.	1337	1216	3	7	0.95	0.54
324	Trave f.	1288	1308	3	7	0.97	0.55
325	Trave f.	1663	222	3	7	0.95	0.53
326	Trave f.	746	1499	3	7	0.95	0.53
327	Trave f.	1499	405	3	7	0.95	0.53
328	Trave f.	533	270	3	7	0.95	0.54
329	Trave f.	435	490	3	7	0.97	0.55
330	Trave f.	34	703	3	7	0.95	0.54
331	Trave f.	1430	1517	3	7	0.95	0.54
332	Trave f.	17	355	3	7	0.95	0.54
333	Trave f.	26	416	3	7	0.95	0.54
334	Trave f.	1500	1511	3	7	0.95	0.54
335	Trave f.	678	1500	3	7	0.95	0.54
336	Trave f.	1039	1061	3	7	0.97	0.55
337	Trave f.	1319	1683	3	7	0.95	0.54
338	Trave f.	1330	1642	3	7	0.95	0.54
339	Trave f.	1307	931	3	7	0.95	0.53
340	Trave f.	405	847	3	7	0.95	0.54
341	Trave f.	880	886	3	7	0.95	0.53
342	Trave f.	1216	1224	3	7	0.95	0.54
343	Trave f.	1206	1242	3	7	0.97	0.55
344	Trave f.	675	1700	3	7	0.97	0.55
345	Trave f.	112	1404	3	7	0.95	0.54
346	Trave	1657	1633	50	6		
347	Trave f.	441	631	3	7	0.95	0.54
348	Trave f.	275	868	3	7	0.95	0.54
349	Trave f.	281	746	3	7	0.95	0.54
350	Trave f.	1445	1430	3	7	0.95	0.54
351	Trave f.	1044	1092	3	7	0.97	0.55
352	Trave f.	34	382	3	7	0.97	0.55
353	Trave f.	420	405	3	7	0.95	0.54
354	Trave f.	911	916	3	7	0.95	0.53
355	Trave f.	1294	1354	3	7	0.97	0.55
356	Trave f.	49	12	3	7	0.95	0.53
357	Trave f.	183	112	3	7	0.95	0.54
358	Trave f.	490	508	3	7	0.97	0.55
359	Trave f.	651	441	3	7	0.95	0.54
360	Trave f.	305	275	3	7	0.95	0.54
361	Trave f.	316	404	3	7	0.95	0.54
362	Trave f.	1499	1501	3	7	0.95	0.54
363	Trave f.	1049	1044	3	7	0.97	0.55
364	Trave f.	26	1129	3	7	0.97	0.55
365	Trave f.	847	1503	3	7	0.95	0.54
366	Trave f.	886	898	3	7	0.95	0.53
367	Trave f.	1224	1229	3	7	0.95	0.54
368	Trave f.	750	766	3	7	0.95	0.53
369	Trave f.	171	1165	3	7	0.95	0.54
370	Trave f.	454	603	3	7	0.97	0.55
371	Trave f.	544	1005	3	7	0.95	0.54
372	Trave f.	861	1319	3	7	0.95	0.54
373	Trave f.	746	1330	3	7	0.95	0.54
374	Trave f.	1069	1159	3	7	0.97	0.55
375	Trave f.	43	53	3	7	0.97	0.55
376	Trave f.	477	1050	3	7	0.95	0.54
377	Trave f.	931	934	3	7	0.95	0.53
378	Trave f.	1297	1294	3	7	0.97	0.55
379	Trave f.	85	49	3	7	0.95	0.53
380	Trave f.	188	183	3	7	0.95	0.54
381	Trave f.	693	1431	3	7	0.95	0.54
382	Trave f.	315	1203	3	7	0.95	0.54
383	Trave f.	327	316	3	7	0.95	0.54
384	Trave f.	1511	1499	3	7	0.95	0.54
385	Trave f.	1061	1049	3	7	0.97	0.55
386	Trave f.	861	750	3	7	0.95	0.53
387	Trave f.	178	171	3	7	0.95	0.54
388	Trave f.	550	544	3	7	0.95	0.54
389	Trave f.	868	861	3	7	0.95	0.54
390	Trave f.	1074	1069	3	7	0.97	0.55

391	Trave f.	382	543	3	7	0.97	0.55
392	Trave f.	916	926	3	7	0.95	0.53
393	Trave f.	1312	1206	3	7	0.97	0.55
394	Trave f.	508	593	3	7	0.97	0.55
395	Trave f.	393	281	3	7	0.95	0.54
396	Trave f.	1501	1445	3	7	0.95	0.54
397	Trave f.	75	91	3	7	0.97	0.55
398	Trave f.	857	864	3	7	0.95	0.54
399	Trave f.	898	905	3	7	0.95	0.53
400	Trave f.	1229	1242	3	7	0.95	0.54
401	Trave f.	766	819	3	7	0.95	0.53
402	Trave f.	1165	1174	3	7	0.95	0.54
403	Trave f.	521	560	3	7	0.97	0.55
404	Trave f.	1005	1029	3	7	0.95	0.54
405	Trave f.	1099	1319	3	7	0.97	0.55
406	Trave f.	1090	477	3	7	0.95	0.54
407	Trave f.	953	958	3	7	0.95	0.53
408	Trave f.	1308	1297	3	7	0.97	0.55
409	Trave	1192	199	50	6		
410	Trave f.	227	188	3	7	0.95	0.54
411	Trave f.	703	693	3	7	0.95	0.54
412	Trave f.	355	315	3	7	0.95	0.54
413	Trave f.	336	1489	3	7	0.95	0.54
414	Trave f.	1404	178	3	7	0.95	0.54
415	Trave f.	580	550	3	7	0.95	0.54
416	Trave f.	1092	1074	3	7	0.97	0.55
417	Trave f.	1316	1660	3	7	0.97	0.55
418	Trave f.	404	393	3	7	0.95	0.54
419	Trave f.	79	75	3	7	0.97	0.55
420	Trave f.	1503	857	3	7	0.95	0.54
421	Trave f.	603	521	3	7	0.97	0.55
422	Trave f.	1105	1099	3	7	0.97	0.55
423	Trave f.	53	95	3	7	0.97	0.55
424	Trave f.	480	1502	3	7	0.95	0.54
425	Trave f.	934	947	3	7	0.95	0.53
426	Trave f.	1431	651	3	7	0.95	0.54
427	Trave f.	454	1123	3	7	0.95	0.54
428	Trave f.	543	805	3	7	0.97	0.55
429	Trave f.	926	1517	3	7	0.95	0.53
430	Trave f.	593	441	3	7	0.97	0.55
431	Trave f.	91	8	3	7	0.97	0.55
432	Trave f.	864	905	3	7	0.95	0.54
433	Trave f.	819	838	3	7	0.95	0.53
434	Trave f.	1174	1178	3	7	0.95	0.54
435	Trave f.	560	466	3	7	0.97	0.55
436	Trave f.	1029	1034	3	7	0.95	0.54
437	Trave f.	1125	1439	3	7	0.95	0.54
438	Trave f.	980	986	3	7	0.95	0.53
439	Trave f.	152	141	3	7	0.95	0.53
440	Trave f.	235	395	3	7	0.95	0.54
441	Trave f.	347	466	3	7	0.95	0.54
442	Trave f.	601	1422	3	7	0.95	0.54
443	Trave f.	1326	1316	3	7	0.97	0.55
444	Trave f.	1129	1146	3	7	0.97	0.55
445	Trave f.	1159	1105	3	7	0.97	0.55
446	Trave f.	684	1459	3	7	0.95	0.54
447	Trave f.	1203	454	3	7	0.95	0.54
448	Trave f.	958	969	3	7	0.95	0.53
449	Trave f.	171	647	3	7	0.95	0.53
450	Trave f.	1489	327	3	7	0.95	0.54
451	Trave f.	69	116	3	7	0.97	0.55
452	Trave f.	1502	420	3	7	0.95	0.54
453	Trave f.	947	911	3	7	0.95	0.53
454	Trave f.	998	305	3	7	0.95	0.54
455	Trave f.	802	872	3	7	0.97	0.55
456	Trave f.	1517	880	3	7	0.95	0.53
457	Trave f.	838	746	3	7	0.95	0.53
458	Trave f.	1178	1645	3	7	0.95	0.54
459	Trave f.	1034	1039	3	7	0.95	0.54
460	Trave f.	1166	1125	3	7	0.95	0.54
461	Trave f.	1212	1225	3	7	0.95	0.53
462	Trave f.	164	1472	3	7	0.95	0.53
463	Trave f.	270	235	3	7	0.95	0.54
464	Trave f.	406	347	3	7	0.95	0.54
465	Trave f.	612	601	3	7	0.95	0.54
466	Trave f.	1333	1326	3	7	0.97	0.55

467	Trave f.	913	684	3	7				0.95	0.54
468	Trave f.	95	69	3	7				0.97	0.55
469	Trave f.	1078	998	3	7				0.95	0.54
470	Trave f.	805	802	3	7				0.97	0.55
471	Trave f.	1439	1090	3	7				0.95	0.54
472	Trave f.	986	994	3	7				0.95	0.53
473	Trave f.	395	435	3	7				0.95	0.54
474	Trave f.	466	336	3	7				0.95	0.54
475	Trave f.	1422	580	3	7				0.95	0.54
476	Trave f.	1146	678	3	7				0.97	0.55
477	Trave f.	1459	480	3	7				0.95	0.54
478	Trave f.	969	976	3	7				0.95	0.53
479	Trave f.	175	85	3	7				0.95	0.53
480	Trave f.	116	533	3	7				0.97	0.55
481	Trave f.	872	17	3	7				0.97	0.55
482	Trave f.	1188	1194	3	7				0.95	0.54
483	Trave f.	1380	1212	3	7				0.95	0.53
484	Trave f.	181	164	3	7				0.95	0.53
485	Trave f.	416	406	3	7				0.95	0.54
486	Trave f.	624	1414	3	7				0.95	0.54
487	Trave f.	1340	1333	3	7				0.97	0.55
488	Trave f.	957	1448	3	7				0.95	0.54
489	Trave f.	1123	1481	3	7				0.95	0.54
490	Trave f.	249	134	3	7				0.95	0.53
491	Trave f.	1645	1188	3	7				0.95	0.54
492	Trave f.	1225	1236	3	7				0.95	0.53
493	Trave f.	1472	152	3	7				0.95	0.53
494	Trave f.	994	953	3	7				0.95	0.53
495	Trave f.	435	227	3	7				0.95	0.54
496	Trave f.	976	1260	3	7				0.95	0.53
497	Trave f.	1642	1307	3	7				0.95	0.53
498	Trave f.	1194	1201	3	7				0.95	0.54
499	Trave f.	1392	1380	3	7				0.95	0.53
500	Trave f.	204	181	3	7				0.95	0.53
501	Trave f.	631	624	3	7				0.95	0.54
502	Trave f.	1354	1340	3	7				0.97	0.55
503	Trave f.	1050	957	3	7				0.95	0.54
504	Trave f.	647	688	3	7				0.95	0.53
505	Trave f.	1414	612	3	7				0.95	0.54
506	Trave f.	1448	913	3	7				0.95	0.54
507	Trave f.	1481	1078	3	7				0.95	0.54
508	Trave f.	261	175	3	7				0.95	0.53
509	Trave f.	1236	1247	3	7				0.95	0.53
510	Trave f.	1260	1683	3	7				0.95	0.53
511	Trave f.	1201	1210	3	7				0.95	0.54
512	Trave f.	212	675	3	7				0.95	0.53
513	Trave f.	544	261	3	7				0.95	0.53
514	Trave f.	1660	1312	3	7				0.97	0.55
515	Trave f.	1247	980	3	7				0.95	0.53
516	Trave f.	1270	1279	3	7				0.95	0.53
517	Trave f.	1210	1337	3	7				0.95	0.54
518	Trave f.	222	212	3	7				0.95	0.53
519	Trave f.	1683	1270	3	7				0.95	0.53
520	Trave f.	711	723	3	7				0.95	0.53
521	Trave f.	1279	1289	3	7				0.95	0.53
522	Trave f.	723	249	3	7				0.95	0.53
523	Trave f.	1289	1300	3	7				0.95	0.53
524	Trave f.	1300	1642	3	7				0.95	0.53
525	Trave	23	32	50	9		000011	000011		
526	Pilas.	1698	1699	50	3	90.00	000011	000011		
527	Pilas.	1700	1192	50	3	90.00	000011	000011		
528	Trave	1701	1615	50	5					
529	Trave f.	1700	1698	3	7				0.97	0.55
530	Trave f.	1698	1660	3	7				0.97	0.55
531	Trave f.	141	1703	3	7				0.95	0.53
532	Trave f.	1703	171	3	7				0.95	0.53
533	Trave f.	688	1713	3	7				0.95	0.53
534	Trave f.	1713	711	3	7				0.95	0.53
535	Trave f.	12	1721	3	7				0.95	0.53
536	Trave f.	1721	861	3	7				0.95	0.53
537	Trave f.	134	544	3	7				0.95	0.53
538	Trave	58	695	50	6		000011			
539	Trave	695	67	50	6					
540	Trave	67	698	50	6					
541	Trave	698	97	50	6					
542	Trave	97	712	50	6					

543	Trave	712	119	50	6				
544	Trave	119	718	50	6				
545	Trave	718	378	50	6				
546	Trave	378	648	50	6				
547	Trave	648	64	50	6				
548	Trave	621	1020	50	6	000011	000011		
549	Trave	1020	798	50	6				
550	Trave	798	353	50	6				
551	Trave	353	830	50	6				
552	Trave	830	661	50	6				
553	Trave	661	876	50	6				
554	Trave	876	665	50	6				
555	Trave	665	1124	50	6				
556	Trave	1124	1022	50	6				
557	Trave	1022	655	50	6		000011		
558	Trave	1585	720	50	6	000011			
559	Trave	720	1593	50	6				
560	Trave	1593	725	50	6				
561	Trave	725	81	50	6				
562	Trave	81	729	50	6				
563	Trave f.	1039	1247	3	7			0.95	0.54
564	Trave	878	1657	50	6	000011			
565	Trave	1569	910	50	6		000011		
566	Trave	1580	1569	50	6				
567	Trave	1587	1580	50	6				
568	Trave	1633	1587	50	6				

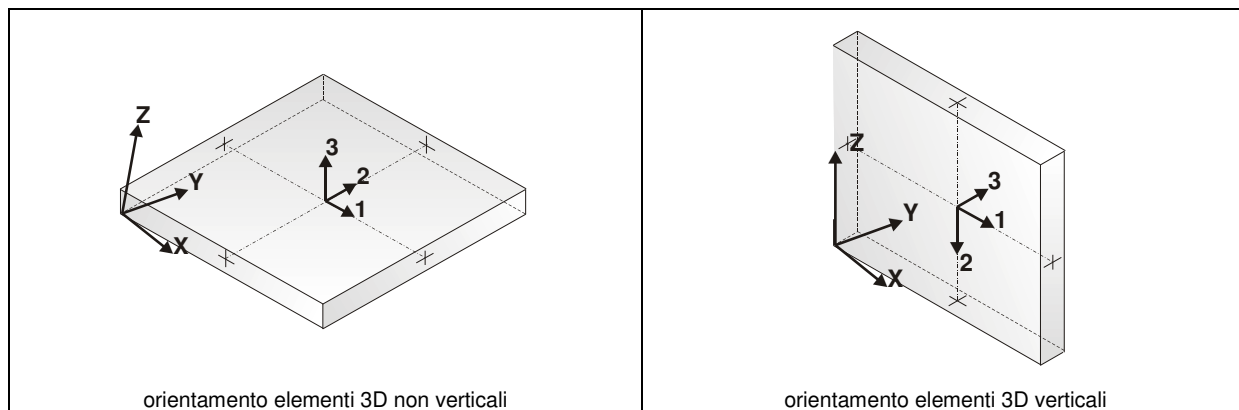
MODELLAZIONE STRUTTURA: ELEMENTI SHELL

LEGENDA TABELLA DATI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell.

Ogni elemento shell è individuato dai nodi I, J, K, L (L=I per gli elementi a tre nodi).

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: <i>Guscio</i> (elemento guscio in elevazione non verticale) <i>Guscio fond.</i> (elemento guscio su suolo elastico) <i>Setto</i> (elemento guscio in elevazione verticale) <i>Membrana</i> (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
8	MENSOLE CON ELEMENTI PLATE E MATERIALE ORTOTROPO
10	PIASTRA CON ELEMENTI PLATE E MATERIALE ORTOTROPO
21	DRILLING
25	TENSIONI DI ELEMENTI PLATE
31	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON PUNTI FISSI IMPORTATA DA FILE .DXF
32	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON SEGMENTI E FORI INTERNI IMPORTATA DA FILE .DXF
33	REALIZZAZIONE DI MESH PIANE SU GEOMETRIE COSTRUITE IN PRO_SAP
34	ANALISI DI BUCKLING DI PIASTRA ISOTROPA
35	ANALISI DI BUCKLING DI UN CILINDRO COMPRESSO INCASTRATO ALLA BASE
36	ANALISI DI PARETI FORATE
37	BIMETALLIC STRIP (NAFEMS EXERCISE 6)
38	ANALISI ELASTICA DI PIASTRA CON INTAGLIO CIRCOLARE (FLAT BAR WITH EDGE NOTCHES-NAFEMS EXERCISE 9)
39	PLATEA NERVATA
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Spessore cm	Wink V daN/cm3	Wink O daN/cm3
2	Setto	1673	257	256	1402	49	13.7		
3	Setto	1675	659	257	1673	49	13.7		
4	Setto	556	272	262	551	49	13.7		
5	Setto	551	262	1651	548	49	13.7		
6	Setto	1651	165	175	261	49	13.7		
7	Setto	1724	877	1169	1725	48	13.7		
8	Setto	1726	881	877	1724	48	13.7		
9	Setto	781	1724	1725		48	13.7		
11	Setto	548	1651	261	544	49	13.7		
12	Setto	262	180	165	1651	49	13.7		
13	Setto	145	267	266	277	48	13.7		
14	Setto	676	1727	1726		48	13.7		
15	Setto	1646	271	269	1644	48	13.7		
16	Setto	564	1648	274	561	49	13.7		
17	Setto	1080	1011	1014	1084	48	13.7		
18	Setto	1649	276	264	1648	49	13.7		
19	Setto	272	124	180	262	49	13.7		
20	Setto	1653	145	783		48	13.7		
21	Setto	1727	889	881	1726	48	13.7		
22	Setto	5	674	1644	1655	48	13.7		
23	Setto	577	823	1648	564	49	13.7		
24	Setto	1648	264	132	274	49	13.7		
25	Setto	274	132	124	272	49	13.7		
26	Setto	30	1653	785		48	13.7		
27	Setto	35	1655	1653	30	48	13.7		
28	Setto	40	667	1655	35	48	13.7		
29	Setto	45	9	12	49	49	13.7		
30	Setto	52	20	9	45	49	13.7		
31	Setto	60	25	20	52	49	13.7		
32	Setto	65	30	25	60	49	13.7		
33	Setto	70	35	30	65	49	13.7		
34	Setto	74	40	35	70	49	13.7		
35	Setto	77	45	49	85	49	13.7		
36	Setto	90	52	45	77	49	13.7		
37	Setto	99	60	52	90	49	13.7		
38	Setto	107	65	565		49	13.7		
39	Setto	115	70	65	107	49	13.7		
40	Setto	120	633	70	115	49	13.7		
41	Setto	264	155	150	132	48	13.7		

42	Setto	276	312	155	264	48	13.7
43	Setto	132	150	776		48	13.7
44	Setto	150	107	775		48	13.7
45	Setto	155	115	107	150	48	13.7
46	Setto	160	547	115	155	48	13.7
47	Setto	538	483	524	540	48	13.7
48	Setto	533	270	473	532	48	13.7
49	Setto	504	260	265	505	49	13.7
50	Setto	1062	900	893	1063	48	13.7
51	Setto	998	305	907	995	48	13.7
52	Setto	939	298	302	940	49	13.7
53	Setto	22	1241	1252	23	49	13.7
54	Setto	18	1360	1372	19	49	13.7
55	Setto	16	1348	1360	18	49	13.7
56	Setto	420	405	409	412	48	13.7
57	Setto	412	409	1541	430	48	13.7
58	Setto	430	425	1547	437	48	13.7
59	Setto	437	434	1548	450	48	13.7
60	Setto	450	445	1549	460	48	13.7
61	Setto	460	455	465	470	48	13.7
62	Setto	480	1502	412	475	48	13.7
63	Setto	475	412	430	484	48	13.7
64	Setto	484	430	437	487	48	13.7
65	Setto	487	437	450	495	48	13.7
66	Setto	495	450	460	500	48	13.7
67	Setto	500	460	470	506	48	13.7
68	Setto	957	1448	1450	954	48	13.7
69	Setto	1459	480	475	1461	48	13.7
70	Setto	1461	475	484	1462	48	13.7
71	Setto	1462	484	487	1464	48	13.7
72	Setto	1464	487	495	1466	48	13.7
73	Setto	1466	495	500	1467	48	13.7
74	Setto	1467	500	506	1470	48	13.7
75	Setto	913	684	515	906	49	13.7
76	Setto	906	515	687	921	49	13.7
77	Setto	921	687	738	924	49	13.7
78	Setto	924	738	885	927	49	13.7
79	Setto	927	885	892	941	49	13.7
80	Setto	941	892	899	944	49	13.7
81	Setto	1448	913	906	1450	49	13.7
82	Setto	1450	906	921	1451	49	13.7
83	Setto	1451	921	924	1453	49	13.7
84	Setto	1453	924	927	1454	49	13.7
85	Setto	1454	927	941	1455	49	13.7
86	Setto	1455	941	944	1456	49	13.7
87	Setto	1050	957	954	1045	48	13.7
88	Setto	1045	954	967	1054	48	13.7
89	Setto	1054	967	970	1057	48	13.7
90	Setto	1057	970	972	1065	48	13.7
91	Setto	1065	972	1026	1070	48	13.7
92	Setto	1070	1026	1040	1075	48	13.7
93	Setto	477	1050	1045	479	48	13.7
94	Setto	479	1045	1054	481	48	13.7
95	Setto	481	1054	1057	482	48	13.7
96	Setto	482	1057	1065	485	48	13.7
97	Setto	485	1065	1070	486	48	13.7
98	Setto	486	1070	1075	488	48	13.7
99	Setto	1439	1090	1081	1441	48	13.7
100	Setto	1441	1081	1095	1442	48	13.7
101	Setto	1442	1095	1100	1443	48	13.7
102	Setto	1443	1100	1104	1444	48	13.7
103	Setto	1444	1104	1107	1446	48	13.7
104	Setto	1446	1107	1115	1447	48	13.7
105	Setto	1166	1125	1120	1158	49	13.7
106	Setto	1158	1120	1132	1171	49	13.7
107	Setto	1171	1132	1140	1176	49	13.7
108	Setto	1176	1140	1145	1180	49	13.7
109	Setto	1180	1145	1150	1183	49	13.7
110	Setto	1183	1150	1155	1191	49	13.7
111	Setto	954	1450	1451	967	48	13.7
112	Setto	8	1166	1158	7	49	13.7
113	Setto	7	1158	1171	1	49	13.7
114	Setto	1	1171	1176	2	49	13.7
115	Setto	2	1176	1180	3	49	13.7
116	Setto	3	1180	1183	4	49	13.7
117	Setto	4	1183	1191	6	49	13.7

118	Setto	143	42	43	148	48	13.7
119	Setto	158	44	42	143	48	13.7
120	Setto	967	1451	1453	970	48	13.7
121	Setto	163	46	44	158	48	13.7
122	Setto	168	47	46	163	48	13.7
123	Setto	169	48	47	168	48	13.7
124	Setto	170	195	48	169	48	13.7
125	Setto	42	51	53	43	48	13.7
126	Setto	44	54	51	42	48	13.7
127	Setto	46	55	54	44	48	13.7
128	Setto	47	56	55	46	48	13.7
129	Setto	48	57	56	47	48	13.7
130	Setto	50	58	57	48	48	13.7
131	Setto	1556	1540	1539		48	13.7
132	Setto	121	534	532	114	48	13.7
133	Setto	122	535	534	121	48	13.7
134	Setto	125	536	535	122	48	13.7
135	Setto	126	538	536	125	48	13.7
136	Setto	1563	1592	205	1561	48	13.7
137	Setto	127	365	538	126	48	13.7
138	Setto	734	1122	874	251	49	13.7
139	Setto	379	68	69	95	48	13.7
140	Setto	59	71	68	379	48	13.7
141	Setto	61	72	71	59	48	13.7
142	Setto	1564	727	1592	1563	48	13.7
143	Setto	62	106	72	61	48	13.7
144	Setto	63	109	106	62	48	13.7
145	Setto	64	658	109	63	48	13.7
146	Setto	68	114	116	69	48	13.7
147	Setto	71	121	114	68	48	13.7
148	Setto	714	492	728		49	13.7
149	Setto	72	122	121	71	48	13.7
150	Setto	106	125	122	72	48	13.7
151	Setto	109	126	125	106	48	13.7
152	Setto	111	127	126	109	48	13.7
153	Setto	114	532	533	116	48	13.7
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155	Setto	36	384	381	33	48	13.7
156	Setto	37	386	384	36	48	13.7
157	Setto	38	493	386	37	48	13.7
158	Setto	39	512	493	38	48	13.7
159	Setto	41	370	512	39	48	13.7
160	Setto	381	541	543	382	48	13.7
161	Setto	384	545	541	381	48	13.7
162	Setto	386	614	545	384	48	13.7
163	Setto	493	615	614	386	48	13.7
164	Setto	512	618	615	493	48	13.7
165	Setto	539	621	618	512	48	13.7
166	Setto	970	1453	1454	972	48	13.7
167	Setto	142	1704	1702	139	48	13.7
168	Setto	1114	18	16	870	48	13.7
169	Setto	1116	19	18	1114	48	13.7
170	Setto	1117	21	19	1116	48	13.7
171	Setto	1119	22	21	1117	48	13.7
172	Setto	1169	566	753		49	13.7
173	Setto	1121	494	22	1119	48	13.7
174	Setto	1710	98	93	1709	48	13.7
175	Setto	1126	800	802	805	48	13.7
176	Setto	623	803	800	1126	48	13.7
177	Setto	646	804	803	623	48	13.7
178	Setto	144	1705	1704	142	48	13.7
179	Setto	653	831	804	646	48	13.7
180	Setto	654	833	831	653	48	13.7
181	Setto	655	400	833	654	48	13.7
182	Setto	800	870	872	802	48	13.7
183	Setto	803	1114	870	800	48	13.7
184	Setto	692	1715	1714	690	49	13.7
185	Setto	804	1116	1114	803	48	13.7
186	Setto	972	1454	1455	1026	48	13.7
187	Setto	1026	1455	1456	1040	48	13.7
188	Setto	1084	1014	1053	1086	48	13.7
189	Setto	1086	1053	1062	1103	48	13.7
190	Setto	1103	1062	1063	1112	48	13.7
191	Setto	1481	1078	1073	1482	48	13.7
192	Setto	1482	1073	1080	1483	48	13.7
193	Setto	1483	1080	1084	1484	48	13.7

194	Setto	1484	1084	1086	1486	48	13.7
195	Setto	1486	1086	1103	1487	48	13.7
196	Setto	1487	1103	1112	1488	48	13.7
197	Setto	454	1123	1113	456	49	13.7
198	Setto	456	1113	1128	457	49	13.7
199	Setto	457	1128	1130	459	49	13.7
200	Setto	459	1130	1136	461	49	13.7
201	Setto	461	1136	1137	462	49	13.7
202	Setto	462	1137	1153	464	49	13.7
203	Setto	315	1203	1154	320	49	13.7
204	Setto	320	1154	1204	325	49	13.7
205	Setto	325	1204	1217	335	49	13.7
206	Setto	335	1217	1218	340	49	13.7
207	Setto	340	1218	1223	345	49	13.7
208	Setto	345	1223	1228	350	49	13.7
209	Setto	21	1233	1241	22	49	13.7
210	Setto	19	1372	1233	21	49	13.7
211	Setto	17	355	1348	16	49	13.7
212	Setto	1373	1253	1327	1378	48	13.7
213	Setto	1378	1327	1342	1383	48	13.7
214	Setto	684	1459	1461	515	49	13.7
215	Setto	515	1461	1462	687	49	13.7
216	Setto	687	1462	1464	738	49	13.7
217	Setto	738	1464	1466	885	49	13.7
218	Setto	885	1466	1467	892	49	13.7
219	Setto	831	1117	1116	804	48	13.7
220	Setto	833	1119	1117	831	48	13.7
221	Setto	835	1121	1119	833	48	13.7
222	Setto	870	16	17	872	48	13.7
223	Setto	892	1467	1470	899	49	13.7
224	Setto	162	1471	1472	164	49	13.7
225	Setto	166	1475	1471	162	49	13.7
226	Setto	1383	1342	1343	1388	48	13.7
227	Setto	167	1476	1475	166	49	13.7
228	Setto	174	1478	1476	167	49	13.7
229	Setto	176	1479	1478	174	49	13.7
230	Setto	1253	335	340	1327	48	13.7
231	Setto	1327	340	345	1342	48	13.7
232	Setto	177	1480	1479	176	49	13.7
233	Setto	1123	1481	1482	1113	49	13.7
234	Setto	1113	1482	1483	1128	49	13.7
235	Setto	554	575	574	529	48	13.7
236	Setto	24	1127	1129	26	48	13.7
237	Setto	1128	1483	1484	1130	49	13.7
238	Setto	1130	1484	1486	1136	49	13.7
239	Setto	1136	1486	1487	1137	49	13.7
240	Setto	27	1133	1127	24	48	13.7
241	Setto	28	1135	1133	27	48	13.7
242	Setto	29	1139	1135	28	48	13.7
243	Setto	31	1141	1139	29	48	13.7
244	Setto	1137	1487	1488	1153	49	13.7
245	Setto	336	1489	1491	334	49	13.7
246	Setto	334	1491	1492	337	49	13.7
247	Setto	32	809	1141	31	48	13.7
248	Setto	1127	1144	1146	1129	48	13.7
249	Setto	1133	1147	1144	1127	48	13.7
250	Setto	1135	1149	1147	1133	48	13.7
251	Setto	1139	1151	1149	1135	48	13.7
252	Setto	337	1492	1493	339	49	13.7
253	Setto	339	1493	1495	341	49	13.7
254	Setto	341	1495	1496	342	49	13.7
255	Setto	342	1496	1498	344	49	13.7
256	Setto	1500	1511	1509	1508	48	13.7
257	Setto	1508	1509	1513	1512	48	13.7
258	Setto	1512	1513	1516	1515	48	13.7
259	Setto	1515	1516	1519	1518	48	13.7
260	Setto	1518	1519	1521	1520	48	13.7
261	Setto	1520	1521	1522	1504	48	13.7
262	Setto	1511	1499	1523	1509	48	13.7
263	Setto	1509	1523	1524	1513	48	13.7
264	Setto	1141	1152	1151	1139	48	13.7
265	Setto	1142	1585	1152	1141	48	13.7
266	Setto	1707	83	73	1711	48	13.7
267	Setto	101	1	7	89	48	13.7
268	Setto	1513	1524	1526	1516	48	13.7
269	Setto	1516	1526	1527	1519	48	13.7

270	Setto	1519	1527	1538	1521	48	13.7
271	Setto	1521	1528	1506	1522	48	13.7
272	Setto	1499	1501	1477	1523	48	13.7
273	Setto	1523	1477	1485	1524	48	13.7
274	Setto	1524	1485	1490	1526	48	13.7
275	Setto	1526	1490	1507	1527	48	13.7
276	Setto	1576	1568	1567	1575	48	13.7
277	Setto	673	1734	1733		48	13.7
278	Setto	1731	1549	445	1732	48	13.7
279	Setto	743	1584	1641	790	48	13.7
280	Setto	1658	1543	816	1595	48	13.7
281	Setto	1584	717	1544	1641	48	13.7
282	Setto	1527	1566	999		48	13.7
283	Setto	102	2	1	101	48	13.7
284	Setto	130	3	2	102	48	13.7
285	Setto	131	4	3	130	48	13.7
286	Setto	1184	1654	1701	1186	49	13.7
287	Setto	1538	1601	1566	1527	48	13.7
288	Setto	133	846	4	131	48	13.7
289	Setto	1177	1647	1650	1181	49	13.7
290	Setto	136	1594	75	79	48	13.7
291	Setto	1586	76	1594	136	48	13.7
292	Setto	1588	78	76	1586	48	13.7
294	Setto	1589	84	78	1588	48	13.7
295	Setto	1590	86	84	1589	48	13.7
296	Setto	1591	844	86	1590	48	13.7
297	Setto	1594	89	91	75	48	13.7
298	Setto	76	101	89	1594	48	13.7
299	Setto	839	1148	780		49	13.7
300	Setto	78	102	101	76	48	13.7
301	Setto	84	130	102	78	48	13.7
302	Setto	86	131	130	84	48	13.7
303	Setto	87	133	131	86	48	13.7
304	Setto	89	7	8	91	48	13.7
305	Setto	1702	1163	171	1703	48	13.7
306	Setto	1704	1167	1163	1702	48	13.7
307	Setto	1705	73	1167	1704	48	13.7
309	Setto	1708	93	83	1706	48	13.7
311	Setto	151	139	141	152	48	13.7
312	Setto	154	142	139	151	48	13.7
313	Setto	156	144	142	154	48	13.7
314	Setto	157	146	144	156	48	13.7
315	Setto	708	1719	1718	706	49	13.7
316	Setto	1506	1013	1601	1528	48	13.7
317	Setto	1543	1552	1551	1542	48	13.7
318	Setto	1595	816	1542	1736	48	13.7
319	Setto	1546	1555	1553	1544	48	13.7
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321	Setto	1471	151	152	1472	48	13.7
322	Setto	1475	154	151	1471	48	13.7
323	Setto	1476	156	154	1475	48	13.7
324	Setto	1478	157	226		48	13.7
325	Setto	1717	492	714	1715	49	13.7
326	Setto	1480	387	159	1479	48	13.7
327	Setto	179	162	164	181	49	13.7
328	Setto	182	166	162	179	49	13.7
329	Setto	1539	1540	1733		48	13.7
330	Setto	1733	455	1549	1731	48	13.7
331	Setto	187	167	166	182	49	13.7
332	Setto	189	174	225		49	13.7
333	Setto	191	176	174	189	49	13.7
334	Setto	1568	1731	1732	1012	48	13.7
335	Setto	1552	1561	818		48	13.7
336	Setto	192	373	176	191	49	13.7
337	Setto	203	179	181	204	49	13.7
338	Setto	206	182	179	203	49	13.7
339	Setto	207	187	182	206	49	13.7
341	Setto	209	191	189	208	49	13.7
342	Setto	210	338	191	209	49	13.7
343	Setto	211	203	675	212	48	13.7
344	Setto	213	206	203	211	48	13.7
345	Setto	214	207	206	213	48	13.7
346	Setto	216	208	218		48	13.7
347	Setto	586	15	555	643	48	13.7
348	Setto	217	209	208	216	48	13.7
349	Setto	219	328	209	217	48	13.7

350	Setto	221	211	212	222	48	13.7
351	Setto	229	213	211	221	48	13.7
352	Setto	231	214	213	229	48	13.7
354	Setto	234	217	216	232	48	13.7
355	Setto	236	323	217	234	48	13.7
356	Setto	1122	561	556	874	49	13.7
357	Setto	92	564	561	1122	49	13.7
358	Setto	828	577	564	92	49	13.7
359	Setto	245	232	760		49	13.7
360	Setto	246	234	232	245	49	13.7
361	Setto	248	696	234	246	49	13.7
362	Setto	1738	765	740	66	48	13.7
363	Setto	1729	737	734	1572	48	13.7
364	Setto	1720	278	737	1729	48	13.7
365	Setto	281	746	778	279	48	13.7
366	Setto	279	778	780	282	48	13.7
367	Setto	282	780	1148	284	48	13.7
368	Setto	284	1148	782	286	48	13.7
369	Setto	286	789	790	287	48	13.7
370	Setto	287	790	743	289	48	13.7
371	Setto	393	281	279	394	48	13.7
372	Setto	394	279	282	396	48	13.7
373	Setto	396	282	284	398	48	13.7
374	Setto	398	284	286	399	48	13.7
375	Setto	399	286	287	401	48	13.7
376	Setto	401	287	289	402	48	13.7
377	Setto	321	301	292	322	48	13.7
378	Setto	314	293	303	317	48	13.7
379	Setto	296	399	401	297	49	13.7
380	Setto	253	1711	1705	144	48	13.7
381	Setto	1555	724	1563	1553	48	13.7
382	Setto	1566	1576	1010		48	13.7
383	Setto	1540	673	1733		48	13.7
384	Setto	304	295	296	306	49	13.7
385	Setto	1622	663	1578	1601	48	13.7
386	Setto	306	296	297	307	49	13.7
387	Setto	307	297	299	308	49	13.7
388	Setto	319	300	301	321	48	13.7
389	Setto	1561	205	820		48	13.7
390	Setto	1592	1573	1571	205	48	13.7
391	Setto	1592	727	1573		48	13.7
392	Setto	1342	345	350	1343	48	13.7
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394	Setto	1233	1378	1383	1241	48	13.7
395	Setto	1241	1383	1388	1252	48	13.7
396	Setto	1581	1634	827		48	13.7
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398	Setto	295	398	399	296	49	13.7
399	Setto	300	304	306	301	49	13.7
400	Setto	301	306	307	292	49	13.7
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402	Setto	327	316	314	326	48	13.7
403	Setto	326	314	317	329	48	13.7
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405	Setto	330	319	321	331	48	13.7
406	Setto	331	321	322	332	48	13.7
407	Setto	332	322	324	333	48	13.7
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412	Setto	1495	331	332	1496	48	13.7
413	Setto	1496	332	333	1498	48	13.7
414	Setto	466	336	334	467	49	13.7
415	Setto	467	334	337	469	49	13.7
416	Setto	469	337	339	471	49	13.7
417	Setto	471	339	341	472	49	13.7
418	Setto	472	341	342	474	49	13.7
419	Setto	474	342	344	476	49	13.7
420	Setto	406	347	346	407	49	13.7
421	Setto	407	346	349	410	49	13.7
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423	Setto	411	351	352	413	49	13.7
424	Setto	413	352	354	414	49	13.7
425	Setto	414	354	356	415	49	13.7
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427	Setto	28	372	357	29	49	13.7
428	Setto	26	416	369	24	49	13.7
429	Setto	385	362	364	388	48	13.7
430	Setto	388	364	366	390	48	13.7
431	Setto	390	366	367	392	48	13.7
432	Setto	362	411	413	364	48	13.7
433	Setto	364	413	414	366	48	13.7
434	Setto	366	414	415	367	48	13.7
435	Setto	372	385	388	357	48	13.7
436	Setto	357	388	390	359	48	13.7
437	Setto	359	390	392	361	48	13.7
438	Setto	322	292	291	324	48	13.7
439	Setto	316	404	293	314	48	13.7
440	Setto	297	401	402	299	49	13.7
441	Setto	31	359	361	32	49	13.7
442	Setto	27	371	372	28	49	13.7
443	Setto	24	369	371	27	49	13.7
444	Setto	1619	419	421	1618	48	13.7
445	Setto	1618	421	422	1620	48	13.7
446	Setto	1620	422	424	1621	48	13.7
447	Setto	1621	424	426	1623	48	13.7
448	Setto	1623	426	427	1624	48	13.7
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450	Setto	433	431	432	442	48	13.7
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452	Setto	423	438	431	433	48	13.7
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454	Setto	417	440	438	423	48	13.7
455	Setto	389	436	439	408	48	13.7
456	Setto	651	441	444	650	48	13.7
457	Setto	650	444	446	652	48	13.7
458	Setto	652	446	447	657	48	13.7
459	Setto	657	447	449	660	48	13.7
460	Setto	660	449	451	662	48	13.7
461	Setto	294	879	883	298	48	13.7
462	Setto	298	883	890	302	48	13.7
463	Setto	1053	952	900	1062	48	13.7
464	Setto	686	1712	1713	688	49	13.7
465	Setto	995	907	965	1011	48	13.7
466	Setto	938	294	298	939	49	13.7
467	Setto	966	914	938	982	49	13.7
468	Setto	1583	744	1558	1582	48	13.7
469	Setto	982	938	939	983	49	13.7
470	Setto	983	939	940	984	49	13.7
471	Setto	1571	1581	825		48	13.7
472	Setto	690	1714	1712	686	49	13.7
473	Setto	662	451	452	681	48	13.7
474	Setto	1203	454	456	1154	49	13.7
475	Setto	1154	456	457	1204	49	13.7
476	Setto	1204	457	459	1217	49	13.7
477	Setto	256	245	242	254	49	13.7
478	Setto	1574	731	1582	1573	48	13.7
479	Setto	1634	1527	1526	1632	48	13.7
480	Setto	257	246	245	256	49	13.7
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482	Setto	742	1572	1735	765	48	13.7
483	Setto	1558	1528	1538	1634	48	13.7
484	Setto	765	1735	117	740	48	13.7
485	Setto	1559	1506	1528	1558	48	13.7
486	Setto	733	311	1722	732	48	13.7
487	Setto	1666	1663	1394	1665	48	13.7
488	Setto	1665	1394	1397	1668	48	13.7
489	Setto	1668	1397	1399	1670	48	13.7
490	Setto	1670	1669	1402	1672	48	13.7
491	Setto	1217	459	461	1218	49	13.7
492	Setto	1218	461	462	1223	49	13.7
493	Setto	1672	1402	1673	1674	48	13.7
494	Setto	1674	1673	1675	1676	48	13.7
495	Setto	1223	462	464	1228	49	13.7
496	Setto	347	466	467	346	49	13.7
497	Setto	1678	1666	1665	1677	48	13.7
498	Setto	1677	1665	1668	1679	48	13.7
499	Setto	346	467	469	349	49	13.7
500	Setto	349	469	471	351	49	13.7
501	Setto	1679	1668	1670	1680	48	13.7
502	Setto	1680	1670	1672	1681	48	13.7

503	Setto	1681	1672	1674	1682	48	13.7
504	Setto	1682	1674	1676	1234	48	13.7
505	Setto	1382	1678	1677	1385	48	13.7
506	Setto	1385	1677	1679	1386	48	13.7
507	Setto	1386	1679	1680	1387	48	13.7
508	Setto	1387	1680	1681	1390	48	13.7
509	Setto	1390	1681	1682	1391	48	13.7
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511	Setto	1562	1350	1349	1457	49	13.7
512	Setto	1457	1349	1351	1577	49	13.7
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514	Setto	588	10	597	587	48	13.7
515	Setto	1596	1352	1353	1597	49	13.7
516	Setto	1597	1353	1358	1598	49	13.7
517	Setto	1598	1358	1359	1599	49	13.7
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519	Setto	1371	1457	1577	1374	49	13.7
520	Setto	1374	1577	1596	1376	49	13.7
521	Setto	1376	1596	1597	1377	49	13.7
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523	Setto	1379	1598	1599	1381	49	13.7
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525	Setto	1609	1600	1603	1612	48	13.7
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528	Setto	1614	1606	1607	1616	48	13.7
529	Setto	351	471	472	352	49	13.7
530	Setto	642	586	643	644	48	13.7
531	Setto	352	472	474	354	49	13.7
532	Setto	591	444	441	593	49	13.7
533	Setto	354	474	476	356	49	13.7
534	Setto	1090	477	479	1081	48	13.7
535	Setto	1081	479	481	1095	48	13.7
536	Setto	1095	481	482	1100	48	13.7
537	Setto	1100	482	485	1104	48	13.7
538	Setto	1104	485	486	1107	48	13.7
539	Setto	1107	486	488	1115	48	13.7
540	Setto	436	489	490	435	49	13.7
541	Setto	439	491	489	436	49	13.7
542	Setto	440	496	491	439	49	13.7
543	Setto	438	497	496	440	49	13.7
544	Setto	431	499	497	438	49	13.7
545	Setto	432	501	499	431	49	13.7
546	Setto	489	502	508	490	49	13.7
547	Setto	491	509	502	489	49	13.7
548	Setto	496	510	509	491	49	13.7
549	Setto	497	514	510	496	49	13.7
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552	Setto	459	606	604	457	49	13.7
553	Setto	461	637	606	459	49	13.7
554	Setto	462	638	637	461	49	13.7
555	Setto	464	639	638	462	49	13.7
556	Setto	641	642	644	640	48	13.7
557	Setto	517	1134	529	516	48	13.7
558	Setto	597	451	449	596	49	13.7
559	Setto	598	452	451	597	49	13.7
560	Setto	456	602	603	454	49	13.7
561	Setto	457	604	602	456	49	13.7
562	Setto	639	11	640	638	48	13.7
563	Setto	1163	645	647	171	48	13.7
564	Setto	1167	668	645	1163	48	13.7
565	Setto	73	669	668	1167	48	13.7
566	Setto	83	671	468	73	48	13.7
567	Setto	93	683	671	83	48	13.7
568	Setto	98	685	683	93	48	13.7
569	Setto	645	686	688	647	48	13.7
570	Setto	668	690	686	645	48	13.7
571	Setto	594	446	444	591	49	13.7
572	Setto	669	692	690	668	48	13.7
573	Setto	468	704	478		48	13.7
574	Setto	704	1716	1717	692	49	13.7
575	Setto	685	197	706	683	48	13.7
576	Setto	1712	709	711	1713	49	13.7
577	Setto	1714	713	709	1712	49	13.7
578	Setto	1715	714	713	1714	49	13.7

579	Setto	1716	715	492	1717	49	13.7
580	Setto	1718	719	715	1716	49	13.7
581	Setto	1719	721	719	1718	49	13.7
582	Setto	709	722	723	711	49	13.7
583	Setto	713	726	722	709	49	13.7
584	Setto	714	728	726	713	49	13.7
585	Setto	1181	1650	1654	1184	49	13.7
586	Setto	719	732	730	715	49	13.7
587	Setto	721	733	732	719	49	13.7
588	Setto	80	548	544	134	49	13.7
589	Setto	656	551	548	80	49	13.7
590	Setto	874	556	551	656	49	13.7
591	Setto	862	748	750	861	49	13.7
592	Setto	869	752	748	862	49	13.7
593	Setto	873	754	752	869	49	13.7
594	Setto	250	656	80	241	49	13.7
595	Setto	881	756	755	877	49	13.7
596	Setto	889	762	756	881	49	13.7
597	Setto	748	764	766	750	49	13.7
598	Setto	752	768	764	748	49	13.7
599	Setto	1616	1607	1608	1617	48	13.7
600	Setto	419	1610	1609	421	48	13.7
601	Setto	421	1609	1612	422	48	13.7
602	Setto	422	1612	1613	424	48	13.7
603	Setto	424	1613	1614	426	48	13.7
604	Setto	754	769	768	752	49	13.7
605	Setto	566	770	769	754	49	13.7
606	Setto	756	771	770	755	49	13.7
607	Setto	762	772	771	756	49	13.7
608	Setto	426	1614	1616	427	48	13.7
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610	Setto	1361	1619	1618	1362	48	13.7
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614	Setto	1366	1623	1624	1368	48	13.7
615	Setto	1368	1624	1625	1369	48	13.7
616	Setto	1638	1627	1626	1637	49	13.7
617	Setto	1637	1626	1628	1639	49	13.7
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619	Setto	104	1630	1631	108	49	13.7
620	Setto	108	1631	1635	110	49	13.7
621	Setto	110	1635	1636	138	49	13.7
622	Setto	148	1638	1637	143	49	13.7
623	Setto	143	1637	1639	158	49	13.7
624	Setto	158	1639	104	163	49	13.7
625	Setto	163	104	108	168	49	13.7
626	Setto	168	108	110	169	49	13.7
627	Setto	169	110	138	170	49	13.7
628	Setto	178	171	1163	173	49	13.7
629	Setto	173	1163	1167	186	49	13.7
630	Setto	186	1167	73	82	49	13.7
631	Setto	82	73	83	88	49	13.7
632	Setto	88	83	93	94	49	13.7
633	Setto	94	93	98	103	49	13.7
634	Setto	1404	178	173	1406	49	13.7
635	Setto	1406	173	186	1407	49	13.7
636	Setto	1407	186	82	1408	49	13.7
637	Setto	826	129	841	824	49	13.7
638	Setto	836	791	129	826	49	13.7
639	Setto	837	778	746	838	49	13.7
640	Setto	770	786	797		48	13.7
641	Setto	771	787	786	770	48	13.7
642	Setto	772	807	787	771	48	13.7
643	Setto	839	780	778	837	49	13.7
644	Setto	840	782	1148	839	49	13.7
645	Setto	567	789	1172		49	13.7
647	Setto	787	813	812	786	48	13.7
648	Setto	788	815	813	787	48	13.7
649	Setto	129	790	789	841	49	13.7
650	Setto	791	743	790	129	49	13.7
651	Setto	824	841	567	822	49	13.7
652	Setto	801	824	806		48	13.7
653	Setto	813	826	824	812	48	13.7
654	Setto	815	814	826	813	48	13.7
655	Setto	817	837	838	819	49	13.7

656	Setto	821	839	837	817	49	13.7
657	Setto	822	840	839	821	49	13.7
658	Setto	405	847	845	409	48	13.7
659	Setto	1541	845	849	425	48	13.7
660	Setto	1547	849	851	434	48	13.7
661	Setto	1548	851	855	445	48	13.7
662	Setto	847	1503	856	845	49	13.7
663	Setto	845	856	858	849	49	13.7
664	Setto	849	858	859	851	49	13.7
665	Setto	851	859	860	855	49	13.7
666	Setto	857	864	863	856	49	13.7
667	Setto	856	863	866	858	49	13.7
668	Setto	858	866	867	859	49	13.7
669	Setto	859	867	878	860	49	13.7
670	Setto	882	884	886	880	49	13.7
671	Setto	887	888	884	882	49	13.7
672	Setto	891	894	888	887	49	13.7
673	Setto	895	542	894	891	49	13.7
674	Setto	884	897	898	886	49	13.7
675	Setto	888	901	897	884	49	13.7
676	Setto	894	902	901	888	49	13.7
677	Setto	896	903	902	894	49	13.7
678	Setto	897	904	905	898	49	13.7
679	Setto	901	908	904	897	49	13.7
680	Setto	902	909	908	901	49	13.7
681	Setto	903	546	909	902	49	13.7
682	Setto	912	915	916	911	48	13.7
683	Setto	917	918	915	912	48	13.7
684	Setto	919	920	918	917	48	13.7
685	Setto	922	518	920	919	48	13.7
686	Setto	915	925	926	916	48	13.7
687	Setto	918	928	925	915	48	13.7
688	Setto	920	929	928	918	48	13.7
689	Setto	923	519	929	920	48	13.7
690	Setto	1514	882	880	1517	48	13.7
691	Setto	1525	887	882	1514	48	13.7
692	Setto	1530	891	887	1525	48	13.7
693	Setto	1534	537	891	1530	48	13.7
694	Setto	932	933	934	931	49	13.7
695	Setto	935	936	933	932	49	13.7
696	Setto	937	942	936	935	49	13.7
697	Setto	943	507	942	937	49	13.7
698	Setto	933	946	947	934	49	13.7
699	Setto	936	948	946	933	49	13.7
700	Setto	942	949	948	936	49	13.7
701	Setto	945	513	949	942	49	13.7
702	Setto	946	912	911	947	49	13.7
703	Setto	948	917	912	946	49	13.7
704	Setto	949	919	917	948	49	13.7
705	Setto	950	922	919	949	49	13.7
706	Setto	955	956	958	953	48	13.7
707	Setto	959	960	956	955	48	13.7
708	Setto	961	962	960	959	48	13.7
709	Setto	963	448	962	961	48	13.7
710	Setto	956	968	969	958	48	13.7
711	Setto	960	971	968	956	48	13.7
712	Setto	962	973	971	960	48	13.7
713	Setto	964	453	973	962	48	13.7
714	Setto	968	975	976	969	48	13.7
715	Setto	971	977	975	968	48	13.7
716	Setto	973	978	977	971	48	13.7
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718	Setto	981	985	986	980	49	13.7
719	Setto	987	988	985	981	49	13.7
720	Setto	989	990	988	987	49	13.7
721	Setto	991	418	990	989	49	13.7
722	Setto	985	993	994	986	49	13.7
723	Setto	988	1000	993	985	49	13.7
724	Setto	1408	82	88	1410	49	13.7
725	Setto	1410	88	94	1411	49	13.7
726	Setto	1411	94	103	1413	49	13.7
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728	Setto	153	105	113	185	48	13.7
729	Setto	185	113	118	193	48	13.7
730	Setto	990	1001	1000	988	49	13.7
731	Setto	992	428	1001	990	49	13.7

732	Setto	993	955	953	994	49	13.7
733	Setto	1000	959	955	993	49	13.7
734	Setto	1001	961	959	1000	49	13.7
735	Setto	1002	443	961	1001	49	13.7
736	Setto	544	1005	1004	548	48	13.7
737	Setto	548	1004	1007	551	48	13.7
738	Setto	551	1007	1009	556	48	13.7
739	Setto	556	1009	1027	561	48	13.7
740	Setto	1005	1029	1028	1004	49	13.7
741	Setto	1004	1028	1030	1007	49	13.7
742	Setto	1007	1030	1031	1009	49	13.7
743	Setto	1009	1031	1032	1027	49	13.7
744	Setto	1029	1034	1033	1028	49	13.7
745	Setto	1028	1033	1035	1030	49	13.7
746	Setto	1030	1035	1036	1031	49	13.7
747	Setto	1031	1036	1037	1032	49	13.7
748	Setto	1034	1039	1038	1033	49	13.7
749	Setto	1033	1038	1041	1035	49	13.7
750	Setto	1035	1041	1042	1036	49	13.7
751	Setto	193	118	123	194	48	13.7
752	Setto	194	123	128	198	48	13.7
753	Setto	1036	1042	1043	1037	49	13.7
754	Setto	198	128	137	200	48	13.7
755	Setto	1047	1046	1044	1049	48	13.7
756	Setto	1052	1051	1046	1047	48	13.7
757	Setto	1056	1055	1051	1052	48	13.7
758	Setto	1059	569	1055	1056	48	13.7
759	Setto	1060	1047	1049	1061	48	13.7
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762	Setto	1067	568	1056	1066	48	13.7
763	Setto	1038	1060	1061	1039	48	13.7
764	Setto	1041	1064	1060	1038	48	13.7
765	Setto	1042	1066	1064	1041	48	13.7
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767	Setto	1072	1071	1069	1074	49	13.7
768	Setto	1077	1076	1071	1072	49	13.7
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770	Setto	1089	571	1079	1082	49	13.7
771	Setto	1091	1072	1074	1092	49	13.7
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773	Setto	1096	1082	1077	1094	49	13.7
774	Setto	1097	570	1082	1096	49	13.7
775	Setto	1046	1091	1092	1044	49	13.7
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778	Setto	1058	1097	1096	1055	49	13.7
779	Setto	1102	1101	1099	1105	48	13.7
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781	Setto	1110	1109	1106	1108	48	13.7
782	Setto	1156	1118	1109	1110	48	13.7
783	Setto	1157	1102	1105	1159	48	13.7
784	Setto	1160	1108	1102	1157	48	13.7
785	Setto	1161	1110	1108	1160	48	13.7
786	Setto	1162	572	1110	1161	48	13.7
787	Setto	1071	1157	1159	1069	48	13.7
788	Setto	1076	1160	1157	1071	48	13.7
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790	Setto	1085	1162	1161	1079	48	13.7
791	Setto	188	183	153	190	48	13.7
792	Setto	190	153	185	215	48	13.7
793	Setto	215	185	193	220	48	13.7
794	Setto	220	193	194	230	48	13.7
795	Setto	230	194	198	201	48	13.7
796	Setto	201	198	200	223	48	13.7
797	Setto	431	368	374	432	48	13.7
798	Setto	435	227	252	436	48	13.7
799	Setto	228	220	230	233	49	13.7
800	Setto	171	1165	1164	1163	49	13.7
801	Setto	1163	1164	1168	1167	49	13.7
802	Setto	1167	1168	1170	73	49	13.7
803	Setto	73	1170	1173	83	49	13.7
804	Setto	1174	1178	1177	1175	49	13.7
805	Setto	1175	1177	1181	1179	49	13.7
806	Setto	1179	1181	1184	1182	49	13.7
807	Setto	1182	1184	1186	1185	49	13.7

808	Setto	1645	1188	1187	1647	49	13.7
809	Setto	1647	1187	1189	1650	49	13.7
810	Setto	1650	1189	1190	1654	49	13.7
811	Setto	567	1172	840		49	13.7
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813	Setto	1187	1193	1196	1189	49	13.7
814	Setto	1189	1196	1197	1190	49	13.7
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817	Setto	1193	1200	1202	1196	48	13.7
818	Setto	1196	1202	1205	1197	48	13.7
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820	Setto	1201	1210	1208	1200	48	13.7
821	Setto	310	228	233	313	49	13.7
822	Setto	313	233	238	318	49	13.7
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824	Setto	438	358	368	431	48	13.7
825	Setto	439	268	288	440	48	13.7
826	Setto	238	201	223	243	49	13.7
827	Setto	375	310	313	376	49	13.7
828	Setto	1200	1208	1211	1202	48	13.7
829	Setto	1202	1211	1213	1205	48	13.7
830	Setto	1205	1213	1214	1207	48	13.7
831	Setto	1337	1216	1215	1345	48	13.7
832	Setto	1345	1215	1219	1364	48	13.7
833	Setto	1364	1219	1221	1367	48	13.7
834	Setto	1367	1221	1222	1375	48	13.7
835	Setto	1224	1229	1227	1226	48	13.7
836	Setto	1226	1227	1232	1231	48	13.7
837	Setto	559	467	466	560	49	13.7
838	Setto	1231	1232	1237	1235	48	13.7
839	Setto	1235	1237	1239	1238	48	13.7
840	Setto	1229	1242	1240	1227	48	13.7
841	Setto	1227	1240	1244	1232	48	13.7
842	Setto	1232	1244	1245	1237	48	13.7
843	Setto	1237	1245	1246	1239	48	13.7
844	Setto	1248	1251	1250	1249	48	13.7
845	Setto	1249	1250	1256	1254	48	13.7
846	Setto	1254	1256	1258	1257	48	13.7
847	Setto	1257	1258	1261	1259	48	13.7
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849	Setto	1251	1263	1262	1250	48	13.7
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851	Setto	1256	1264	1266	1258	48	13.7
852	Setto	1258	1266	1267	1261	48	13.7
853	Setto	1263	1269	1268	1262	48	13.7
854	Setto	1262	1268	1271	1264	48	13.7
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860	Setto	1272	1278	1280	1273	49	13.7
861	Setto	1276	1283	1281	1274	49	13.7
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863	Setto	1277	1284	1285	1278	49	13.7
864	Setto	1278	1285	1286	1280	49	13.7
865	Setto	1283	1288	1287	1281	49	13.7
866	Setto	1281	1287	1290	1284	49	13.7
867	Setto	1284	1290	1291	1285	49	13.7
868	Setto	1285	1291	1293	1286	49	13.7
869	Setto	1296	1295	1294	1297	48	13.7
870	Setto	1299	1298	1295	1296	48	13.7
871	Setto	1302	1301	1298	1299	48	13.7
872	Setto	1305	1303	1301	1302	48	13.7
873	Setto	1306	1296	1297	1308	48	13.7
874	Setto	520	559	560	521	49	13.7
875	Setto	1309	1299	1296	1306	48	13.7
876	Setto	1310	1302	1299	1309	48	13.7
877	Setto	1311	309	1302	1310	48	13.7
878	Setto	1287	1306	1308	1288	48	13.7
879	Setto	1290	1309	1306	1287	48	13.7
880	Setto	1291	1310	1309	1290	48	13.7
881	Setto	1293	1311	1310	1291	48	13.7
882	Setto	1314	1313	1660	1316	48	13.7
883	Setto	563	469	467	559	49	13.7

884	Setto	1318	1317	1313	1314	48	13.7
885	Setto	1321	1320	1317	1318	48	13.7
886	Setto	1324	1323	1320	1321	48	13.7
887	Setto	582	471	469	563	49	13.7
888	Setto	1325	1314	1316	1326	48	13.7
889	Setto	1328	1318	1314	1325	48	13.7
890	Setto	1329	1321	1318	1328	48	13.7
891	Setto	1331	363	1321	1329	48	13.7
892	Setto	1332	1325	1326	1333	48	13.7
893	Setto	1335	1328	1325	1332	48	13.7
894	Setto	527	583	582	525	49	13.7
895	Setto	1336	1329	1328	1335	48	13.7
896	Setto	1338	1331	1329	1336	48	13.7
897	Setto	1339	1332	1333	1340	49	13.7
898	Setto	555	584	583	527	49	13.7
899	Setto	523	563	559	520	49	13.7
900	Setto	376	313	318	377	49	13.7
901	Setto	377	318	343	383	49	13.7
902	Setto	1341	1335	1332	1339	49	13.7
903	Setto	1364	1405	1389	1345	49	13.7
904	Setto	1346	1529	1336	1344	49	13.7
905	Setto	583	472	471	582	49	13.7
906	Setto	1347	1339	1340	1354	49	13.7
907	Setto	584	474	472	583	49	13.7
908	Setto	1355	1341	1339	1347	49	13.7
909	Setto	585	476	474	584	49	13.7
910	Setto	1367	1412	1405	1364	49	13.7
911	Setto	558	585	584	555	49	13.7
912	Setto	1357	1346	1344	1356	49	13.7
913	Setto	1295	1347	1354	1294	49	13.7
914	Setto	1298	1355	1347	1295	49	13.7
915	Setto	1375	1425	1412	1367	49	13.7
916	Setto	1303	749	1356	1301	49	13.7
917	Setto	1627	1361	1362	1626	49	13.7
918	Setto	525	582	563	523	49	13.7
919	Setto	440	288	358	438	48	13.7
920	Setto	1626	1362	1363	1628	49	13.7
921	Setto	1628	1363	1365	1630	49	13.7
922	Setto	1630	1365	1366	1631	49	13.7
923	Setto	1631	1366	1368	1635	49	13.7
924	Setto	1635	1368	1369	1636	49	13.7
925	Setto	1602	1370	1371	1600	48	13.7
926	Setto	1600	1371	1374	1603	48	13.7
927	Setto	1603	1374	1376	1605	48	13.7
928	Setto	1605	1376	1377	1606	48	13.7
929	Setto	1606	1377	1379	1607	48	13.7
930	Setto	1607	1379	1381	1608	48	13.7
931	Setto	1350	1382	1385	1349	49	13.7
932	Setto	1349	1385	1386	1351	49	13.7
933	Setto	1351	1386	1387	1352	49	13.7
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936	Setto	1358	1391	1393	1359	49	13.7
937	Setto	1663	1396	1395	1394	48	13.7
938	Setto	1394	1395	1398	1397	48	13.7
939	Setto	1397	1398	1401	1399	48	13.7
940	Setto	1669	1401	1403	1402	48	13.7
941	Setto	112	1404	1406	105	48	13.7
942	Setto	105	1406	1407	113	48	13.7
943	Setto	113	1407	1408	118	48	13.7
944	Setto	118	1408	1410	123	48	13.7
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948	Setto	622	1415	1416	625	48	13.7
949	Setto	625	1416	1417	626	48	13.7
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953	Setto	601	1422	1423	600	49	13.7
954	Setto	600	1423	1424	605	49	13.7
955	Setto	436	252	268	439	48	13.7
956	Setto	605	1424	1426	607	49	13.7
957	Setto	233	230	201	238	49	13.7
958	Setto	607	1426	1427	608	49	13.7
959	Setto	608	1427	1428	609	49	13.7

960	Setto	609	1428	1429	610	49	13.7
961	Setto	693	1431	1432	691	49	13.7
962	Setto	691	1432	1433	694	49	13.7
963	Setto	694	1433	1434	697	49	13.7
964	Setto	697	1434	1436	699	49	13.7
965	Setto	699	1436	1437	700	49	13.7
966	Setto	700	1437	1438	701	49	13.7
967	Setto	1125	1439	1441	1120	49	13.7
968	Setto	1120	1441	1442	1132	49	13.7
969	Setto	1132	1442	1443	1140	49	13.7
970	Setto	288	375	376	358	49	13.7
971	Setto	358	376	377	368	49	13.7
972	Setto	368	377	383	374	49	13.7
973	Setto	235	395	389	240	48	13.7
974	Setto	240	389	408	244	48	13.7
975	Setto	244	408	417	247	48	13.7
976	Setto	247	417	423	255	48	13.7
977	Setto	255	423	433	260	48	13.7
978	Setto	260	433	442	265	48	13.7
979	Setto	536	463	483	538	48	13.7
980	Setto	532	473	522	534	48	13.7
981	Setto	503	255	260	504	49	13.7
982	Setto	526	498	503	528	49	13.7
983	Setto	528	503	504	530	49	13.7
984	Setto	530	504	505	531	49	13.7
985	Setto	535	511	463	536	48	13.7
986	Setto	534	522	511	535	48	13.7
987	Setto	498	247	255	503	49	13.7
988	Setto	511	526	528	463	49	13.7
989	Setto	463	528	530	483	49	13.7
990	Setto	483	530	531	524	49	13.7
991	Setto	550	544	548	549	48	13.7
992	Setto	549	548	551	553	48	13.7
993	Setto	553	551	556	557	48	13.7
994	Setto	557	556	561	562	48	13.7
995	Setto	562	561	564	576	48	13.7
996	Setto	576	564	577	578	48	13.7
997	Setto	580	550	549	579	48	13.7
998	Setto	579	549	553	581	48	13.7
999	Setto	581	553	557	589	48	13.7
1000	Setto	589	557	562	590	48	13.7
1001	Setto	590	562	576	592	48	13.7
1002	Setto	592	576	578	599	48	13.7
1003	Setto	1422	580	579	1423	48	13.7
1004	Setto	1423	579	581	1424	48	13.7
1005	Setto	1424	581	589	1426	48	13.7
1006	Setto	1426	589	590	1427	48	13.7
1007	Setto	1427	590	592	1428	48	13.7
1008	Setto	1428	592	599	1429	48	13.7
1009	Setto	612	601	600	611	49	13.7
1010	Setto	611	600	605	613	49	13.7
1011	Setto	613	605	607	616	49	13.7
1012	Setto	616	607	608	617	49	13.7
1013	Setto	617	608	609	619	49	13.7
1014	Setto	619	609	610	620	49	13.7
1015	Setto	1414	612	611	1415	49	13.7
1016	Setto	1415	611	613	1416	49	13.7
1017	Setto	1416	613	616	1417	49	13.7
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1021	Setto	631	624	622	630	48	13.7
1022	Setto	630	622	625	632	48	13.7
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1024	Setto	634	626	627	635	48	13.7
1025	Setto	635	627	628	636	48	13.7
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1030	Setto	447	634	635	449	48	13.7
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1032	Setto	451	636	649	452	48	13.7
1033	Setto	1431	651	650	1432	48	13.7
1034	Setto	1432	650	652	1433	48	13.7
1035	Setto	1014	951	952	1053	48	13.7

1036	Setto	1433	652	657	1434	48	13.7
1037	Setto	1434	657	660	1436	48	13.7
1038	Setto	1436	660	662	1437	48	13.7
1039	Setto	1011	965	951	1014	48	13.7
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1041	Setto	1437	662	681	1438	48	13.7
1042	Setto	703	693	691	702	49	13.7
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1045	Setto	702	691	694	705	49	13.7
1046	Setto	705	694	697	707	49	13.7
1047	Setto	900	983	984	893	49	13.7
1048	Setto	1078	998	995	1073	48	13.7
1049	Setto	1073	995	1011	1080	48	13.7
1050	Setto	596	449	447	595	49	13.7
1051	Setto	707	697	699	716	49	13.7
1052	Setto	716	699	700	736	49	13.7
1053	Setto	736	700	701	741	49	13.7
1054	Setto	34	703	702	33	49	13.7
1055	Setto	33	702	705	36	49	13.7
1056	Setto	36	705	707	37	49	13.7
1057	Setto	37	707	716	38	49	13.7
1058	Setto	575	588	587	574	48	13.7
1059	Setto	38	716	736	39	49	13.7
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1062	Setto	1145	1444	1446	1150	49	13.7
1063	Setto	868	861	862	865	48	13.7
1064	Setto	865	862	869	871	48	13.7
1065	Setto	871	869	873	875	48	13.7
1066	Setto	1150	1446	1447	1155	49	13.7
1067	Setto	875	873	753	879	48	13.7
1068	Setto	879	877	881	883	48	13.7
1069	Setto	883	881	889	890	48	13.7
1070	Setto	275	868	865	280	48	13.7
1071	Setto	280	865	871	285	48	13.7
1072	Setto	285	871	875	290	48	13.7
1073	Setto	290	875	879	294	48	13.7
1074	Setto	1210	1337	1345	1208	48	13.7
1075	Setto	1208	1345	1364	1211	48	13.7
1076	Setto	1211	1364	1367	1213	48	13.7
1077	Setto	1213	1367	1375	1214	48	13.7
1078	Setto	1389	1384	1380	1392	49	13.7
1079	Setto	1405	1400	1384	1389	49	13.7
1080	Setto	1412	1409	1400	1405	49	13.7
1081	Setto	1425	1195	1409	1412	49	13.7
1082	Setto	1345	1389	1392	1337	49	13.7
1083	Setto	1445	1430	1435	1440	49	13.7
1084	Setto	1440	1435	1449	1452	49	13.7
1085	Setto	1452	1449	1460	1465	49	13.7
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1096	Setto	928	1525	1514	925	48	13.7
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1098	Setto	930	1534	1530	929	48	13.7
1099	Setto	1460	1545	1557	1469	48	13.7
1100	Setto	1537	1530	1534	1550	48	13.7
1101	Setto	1545	1554	1565	1557	48	13.7
1102	Setto	1554	1537	1550	1565	48	13.7
1103	Setto	792	785	25		48	13.7
1104	Setto	806	824	822		48	13.7
1105	Setto	810	806	822		48	13.7
1106	Setto	784	801	810		48	13.7
1107	Setto	799	801	784		48	13.7
1108	Setto	801	806	810		48	13.7
1109	Setto	659	259	257		49	13.7
1110	Setto	1725	1169	753	1728	48	13.7
1111	Setto	267	1724	781		48	13.7

1112	Setto	674	1646	1644		48	13.7
1113	Setto	823	1649	1648		49	13.7
1114	Setto	667	672	1655		48	13.7
1115	Setto	633	74	70		49	13.7
1116	Setto	312	160	155		48	13.7
1117	Setto	547	120	115		48	13.7
1118	Setto	430	1541	425		48	13.7
1119	Setto	437	1547	434		48	13.7
1120	Setto	450	1548	445		48	13.7
1121	Setto	460	1549	455		48	13.7
1122	Setto	1502	420	412		48	13.7
1123	Setto	195	50	48		48	13.7
1124	Setto	663	1556	1539	1578	48	13.7
1125	Setto	205	1571	820		48	13.7
1126	Setto	365	540	538		48	13.7
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1128	Setto	311	1737	1722		48	13.7
1130	Setto	715	730	728	492	49	13.7
1131	Setto	370	539	512		48	13.7
1132	Setto	139	1702	1703	141	48	13.7
1133	Setto	877	755	566	1169	49	13.7
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1135	Setto	1660	1313	1312		48	13.7
1136	Setto	146	1706	1707	253	48	13.7
1137	Setto	400	835	833		48	13.7
1138	Setto	403	1709	1708	149	48	13.7
1139	Setto	809	1142	1141		48	13.7
1140	Setto	147	149	1708		48	13.7
1141	Setto	1521	1538	1528		48	13.7
1142	Setto	790	1641	1658	789	48	13.7
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1146	Setto	846	6	4		48	13.7
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1149	Setto	844	87	86		48	13.7
1150	Setto	672	5	1655		48	13.7
1151	Setto	403	1710	1709		48	13.7
1152	Setto	1013	1622	1601		48	13.7
1153	Setto	387	161	159		48	13.7
1154	Setto	1728	753	873	1723	48	13.7
1155	Setto	1737	239	237	1722	48	13.7
1156	Setto	373	177	176		49	13.7
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1161	Setto	696	236	234		49	13.7
1162	Setto	774	1738	66	728	48	13.7
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1164	Setto	286	782	1172		48	13.7
1165	Setto	724	1564	1563		48	13.7
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1167	Setto	727	1574	1573		48	13.7
1168	Setto	744	1559	1558		48	13.7
1169	Setto	731	1583	1582		48	13.7
1170	Setto	1735	763	251	117	48	13.7
1171	Setto	1634	1538	1527		48	13.7
1172	Setto	732	1722	96	730	48	13.7
1173	Setto	1670	1399	1669		48	13.7
1174	Setto	10	598	597		48	13.7
1175	Setto	1134	554	529		48	13.7
1176	Setto	11	641	640		48	13.7
1178	Setto	671	704	468		48	13.7
1180	Setto	692	1717	1715		49	13.7
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1182	Setto	737	92	1122	734	49	13.7
1183	Setto	241	80	134	249	49	13.7
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1187	Setto	841	789	567		49	13.7
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1189	Setto	822	567	840		49	13.7
1190	Setto	812	824	801		48	13.7
1191	Setto	814	836	826		48	13.7
1192	Setto	409	845	1541		48	13.7

1193	Setto	425	849	1547		48	13.7
1194	Setto	434	851	1548		48	13.7
1195	Setto	1503	857	856		49	13.7
1196	Setto	542	896	894		49	13.7
1197	Setto	546	910	909		49	13.7
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1199	Setto	519	930	929		48	13.7
1200	Setto	537	895	891		48	13.7
1201	Setto	507	945	942		49	13.7
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1203	Setto	448	964	962		48	13.7
1204	Setto	453	974	973		48	13.7
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1208	Setto	443	963	961		49	13.7
1210	Setto	568	1059	1056		48	13.7
1213	Setto	1118	1111	1109		48	13.7
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1215	Setto	309	1305	1302		48	13.7
1216	Setto	363	1324	1321		48	13.7
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1220	Setto	879	753	1169		48	13.7
1221	Setto	1195	1420	1409		49	13.7
1222	Setto	759	256	254		49	13.7
1223	Setto	1669	759	254		49	13.7
1224	Setto	1402	759	1669		49	13.7
1225	Setto	271	676	1726	269	48	13.7
1226	Setto	781	1728	1723	266	48	13.7
1227	Setto	267	781	266		48	13.7
1228	Setto	552	274	272		49	13.7
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1230	Setto	561	552	556		49	13.7
1231	Setto	783	145	277		48	13.7
1232	Setto	1652	783	277		48	13.7
1233	Setto	1653	783	1652		48	13.7
1234	Setto	785	1653	1652		48	13.7
1235	Setto	25	785	1652		48	13.7
1236	Setto	792	30	785		48	13.7
1237	Setto	565	65	60		49	13.7
1238	Setto	99	565	60		49	13.7
1239	Setto	107	565	99		49	13.7
1240	Setto	776	150	140		48	13.7
1241	Setto	124	776	140		48	13.7
1242	Setto	132	776	124		48	13.7
1243	Setto	775	107	99		48	13.7
1244	Setto	140	775	99		48	13.7
1245	Setto	150	775	140		48	13.7
1246	Setto	816	1543	1542		48	13.7
1247	Setto	789	1658	1595	1172	48	13.7
1248	Setto	1172	1595	1736	782	48	13.7
1249	Setto	999	1566	1629		48	13.7
1250	Setto	1526	999	1629		48	13.7
1251	Setto	1527	999	1526		48	13.7
1252	Setto	253	1707	1711		48	13.7
1254	Setto	146	253	144		48	13.7
1255	Setto	226	157	156		48	13.7
1256	Setto	1476	226	156		48	13.7
1257	Setto	1478	226	1476		48	13.7
1258	Setto	1012	1732	1730	1567	48	13.7
1259	Setto	1732	445	1548	1730	48	13.7
1260	Setto	1568	1012	1567		48	13.7
1261	Setto	225	174	167		49	13.7
1262	Setto	187	225	167		49	13.7
1263	Setto	189	225	187		49	13.7
1264	Setto	818	1561	1560		48	13.7
1265	Setto	1551	818	1560		48	13.7
1266	Setto	1552	818	1551		48	13.7
1267	Setto	224	189	187		49	13.7
1268	Setto	207	224	187		49	13.7
1269	Setto	208	224	207		49	13.7
1270	Setto	218	208	207		48	13.7
1271	Setto	214	218	207		48	13.7
1272	Setto	216	218	214		48	13.7

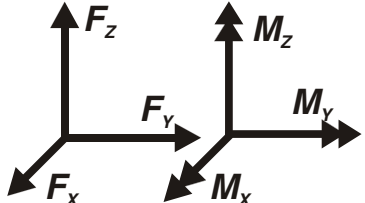
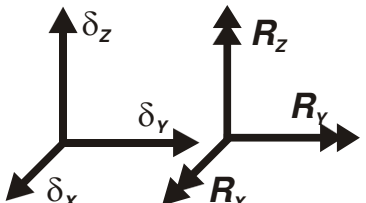
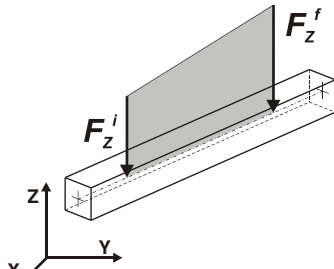
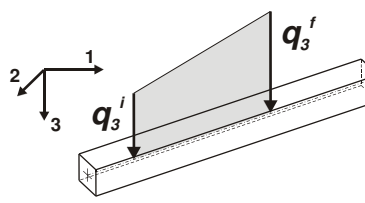
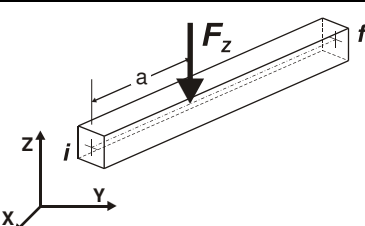
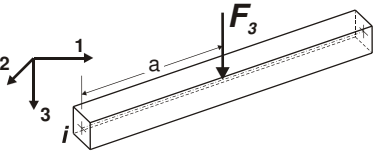
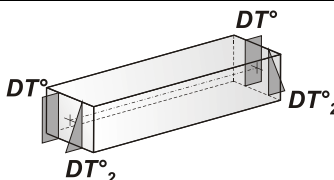
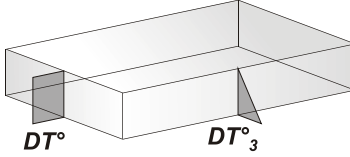
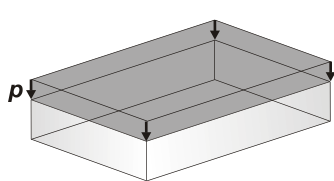
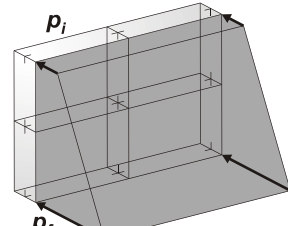
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1274	Setto	231	202	214		48	13.7
1275	Setto	232	202	231		48	13.7
1276	Setto	760	232	231		49	13.7
1277	Setto	242	760	231		49	13.7
1278	Setto	245	760	242		49	13.7
1279	Setto	763	734	251		48	13.7
1280	Setto	96	742	765	1738	48	13.7
1281	Setto	730	96	1738	774	48	13.7
1282	Setto	1010	1576	1575		48	13.7
1283	Setto	1629	1010	1575		48	13.7
1284	Setto	1566	1010	1629		48	13.7
1285	Setto	820	1571	1570		48	13.7
1286	Setto	1560	820	1570		48	13.7
1287	Setto	1561	820	1560		48	13.7
1288	Setto	827	1634	1632		48	13.7
1289	Setto	1579	827	1632		48	13.7
1290	Setto	1581	827	1579		48	13.7
1291	Setto	825	1581	1579		48	13.7
1292	Setto	1570	825	1579		48	13.7
1293	Setto	1571	825	1570		48	13.7
1294	Setto	239	1720	1729	237	48	13.7
1295	Setto	1572	734	763	1735	48	13.7
1296	Setto	730	774	728		48	13.7
1297	Setto	478	704	692		48	13.7
1298	Setto	669	478	692		48	13.7
1299	Setto	468	478	669		48	13.7
1300	Setto	251	874	656	250	49	13.7
1301	Setto	739	828	92	737	49	13.7
1302	Setto	781	1725	1728		48	13.7
1303	Setto	797	786	799		48	13.7
1304	Setto	769	797	799		48	13.7
1305	Setto	770	797	769		48	13.7
1306	Setto	30	792	25		48	13.7
1307	Setto	840	1172	782		49	13.7

MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza Fx, Fy, Fz, momento Mx, My, Mz)
2	spostamento nodale impresso 6 dati (spostamento Tx,Ty,Tz, rotazione Rx,Ry,Rz)
3	carico distribuito globale su elemento tipo trave 7 dati (fx,fy,fz,mx,my,mz,ascissa di inizio carico) 7 dati (fx,fy,fz,mx,my,mz,ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f1,f2,f3,m1,m2,m3,ascissa di inizio carico) 7 dati (f1,f2,f3,m1,m2,m3,ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (Fx,Fy,Fz,Mx,My,Mz,ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F1, F2, F3, M1, M2, M3, ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell' impronta, interasse tra i carichi)

 <p>Carico concentrato nodale</p>	 <p>Spostamento impresso</p>
 <p>Carico distribuito globale</p>	 <p>Carico distribuito locale</p>
 <p>Carico concentrato globale</p>	 <p>Carico concentrato locale</p>
 <p>Carico termico 2D</p>	 <p>Carico termico 3D</p>
 <p>Carico pressione uniforme</p>	 <p>Carico pressione variabile</p>

Tipo	carico di pressione uniforme su piastra
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Id	Tipo	pressione
		daN/ m2
7	QVK PAN ++ vento*0.4	25.60
8	QVK PAN -- vento*0.4	25.60

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Et	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso: *Numero Tipo e Sigla identificativa, Valore di riferimento* del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Qnk	CDC=Qnk (carico da neve)	
5	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=Qnk (carico da neve)
			partecipazione:0.80 per 13 CDC=G1k (permanente scarico porzione atrio)
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
7	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. +)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. -)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. +)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. -)	come precedente CDC sismico
14	Qvk	CDC=Qvk (carico da vento) dir X +	D3 :da 47 a 49 Azione : QVK PAN ++ vento*0.4
			D3 :da 47 a 49 Azione : QVK PAN ++ vento*0.4
			D3 :da 53 a 117 Azione : QVK PAN ++ vento*0.4
			D3 : 120 Azione : QVK PAN ++ vento*0.4
			D3 : 166 Azione : QVK PAN ++ vento*0.4

CDC	Tipo	Sigla Id	Note
			D3 :da 186 a 187 Azione : QVK PAN ++ vento*0.4
			D3 :da 203 a 218 Azione : QVK PAN ++ vento*0.4
			D3 : 223 Azione : QVK PAN ++ vento*0.4
			D3 : 226 Azione : QVK PAN ++ vento*0.4
			D3 :da 230 a 231 Azione : QVK PAN ++ vento*0.4
			D3 :da 392 a 395 Azione : QVK PAN ++ vento*0.4
			D3 :da 420 a 437 Azione : QVK PAN ++ vento*0.4
			D3 :da 441 a 460 Azione : QVK PAN ++ vento*0.4
			D3 :da 473 a 476 Azione : QVK PAN ++ vento*0.4
			D3 :da 473 a 476 Azione : QVK PAN ++ vento*0.4
			D3 :da 487 a 513 Azione : QVK PAN ++ vento*0.4
			D3 :da 487 a 513 Azione : QVK PAN ++ vento*0.4
			D3 :da 515 a 529 Azione : QVK PAN ++ vento*0.4
			D3 :da 515 a 529 Azione : QVK PAN ++ vento*0.4
			D3 : 531 Azione : QVK PAN ++ vento*0.4
			D3 :da 533 a 539 Azione : QVK PAN ++ vento*0.4
			D3 :da 599 a 603 Azione : QVK PAN ++ vento*0.4
			D3 :da 599 a 603 Azione : QVK PAN ++ vento*0.4
			D3 :da 608 a 627 Azione : QVK PAN ++ vento*0.4
			D3 :da 608 a 627 Azione : QVK PAN ++ vento*0.4
			D3 :da 831 a 836 Azione : QVK PAN ++ vento*0.4
			D3 :da 831 a 836 Azione : QVK PAN ++ vento*0.4
			D3 :da 838 a 847 Azione : QVK PAN ++ vento*0.4
			D3 :da 838 a 847 Azione : QVK PAN ++ vento*0.4
			D3 :da 849 a 868 Azione : QVK PAN ++ vento*0.4
			D3 :da 849 a 868 Azione : QVK PAN ++ vento*0.4
			D3 : 917 Azione : QVK PAN ++ vento*0.4
			D3 : 917 Azione : QVK PAN ++ vento*0.4
			D3 :da 920 a 940 Azione : QVK PAN ++ vento*0.4
			D3 :da 920 a 940 Azione : QVK PAN ++ vento*0.4
			D3 :da 961 a 969 Azione : QVK PAN ++ vento*0.4
			D3 :da 961 a 969 Azione : QVK PAN ++ vento*0.4
			D3 :da 973 a 990 Azione : QVK PAN ++ vento*0.4
			D3 :da 973 a 990 Azione : QVK PAN ++ vento*0.4
			D3 :da 1033 a 1034 Azione : QVK PAN ++ vento*0.4
			D3 :da 1033 a 1034 Azione : QVK PAN ++ vento*0.4
			D3 :da 1036 a 1038 Azione : QVK PAN ++ vento*0.4
			D3 :da 1036 a 1038 Azione : QVK PAN ++ vento*0.4
			D3 :da 1041 a 1042 Azione : QVK PAN ++ vento*0.4
			D3 :da 1041 a 1042 Azione : QVK PAN ++ vento*0.4
			D3 :da 1045 a 1046 Azione : QVK PAN ++ vento*0.4
			D3 :da 1045 a 1046 Azione : QVK PAN ++ vento*0.4
			D3 :da 1051 a 1057 Azione : QVK PAN ++ vento*0.4
			D3 :da 1051 a 1057 Azione : QVK PAN ++ vento*0.4
			D3 :da 1059 a 1062 Azione : QVK PAN ++ vento*0.4
			D3 :da 1059 a 1062 Azione : QVK PAN ++ vento*0.4
			D3 : 1066 Azione : QVK PAN ++ vento*0.4
			D3 :da 1091 a 1092 Azione : QVK PAN ++ vento*0.4
			D3 :da 1091 a 1092 Azione : QVK PAN ++ vento*0.4
			D3 :da 1118 a 1122 Azione : QVK PAN ++ vento*0.4
			D3 : 1173 Azione : QVK PAN ++ vento*0.4
			D3 : 1173 Azione : QVK PAN ++ vento*0.4
			D3 : 1219 Azione : QVK PAN ++ vento*0.4
			D3 : 1219 Azione : QVK PAN ++ vento*0.4
15	Qvk	CDC=Qvk (carico da vento) dir X -	D3 :da 47 a 49 Azione : QVK PAN -- vento*0.4
			D3 :da 53 a 117 Azione : QVK PAN -- vento*0.4
			D3 :da 53 a 117 Azione : QVK PAN -- vento*0.4
			D3 : 120 Azione : QVK PAN -- vento*0.4
			D3 : 120 Azione : QVK PAN -- vento*0.4
			D3 : 166 Azione : QVK PAN -- vento*0.4
			D3 : 166 Azione : QVK PAN -- vento*0.4
			D3 :da 186 a 187 Azione : QVK PAN -- vento*0.4
			D3 :da 186 a 187 Azione : QVK PAN -- vento*0.4
			D3 :da 203 a 218 Azione : QVK PAN -- vento*0.4
			D3 :da 203 a 218 Azione : QVK PAN -- vento*0.4
			D3 : 223 Azione : QVK PAN -- vento*0.4
			D3 : 223 Azione : QVK PAN -- vento*0.4
			D3 : 226 Azione : QVK PAN -- vento*0.4

CDC	Tipo	Sigla Id	Note
			D3 : 226 Azione : QVK PAN -- vento*0.4
			D3 :da 230 a 231 Azione : QVK PAN -- vento*0.4
			D3 :da 230 a 231 Azione : QVK PAN -- vento*0.4
			D3 :da 392 a 395 Azione : QVK PAN -- vento*0.4
			D3 :da 392 a 395 Azione : QVK PAN -- vento*0.4
			D3 :da 420 a 437 Azione : QVK PAN -- vento*0.4
			D3 :da 420 a 437 Azione : QVK PAN -- vento*0.4
			D3 :da 441 a 460 Azione : QVK PAN -- vento*0.4
			D3 :da 441 a 460 Azione : QVK PAN -- vento*0.4
			D3 :da 473 a 476 Azione : QVK PAN -- vento*0.4
			D3 :da 487 a 513 Azione : QVK PAN -- vento*0.4
			D3 :da 515 a 529 Azione : QVK PAN -- vento*0.4
			D3 : 531 Azione : QVK PAN -- vento*0.4
			D3 : 531 Azione : QVK PAN -- vento*0.4
			D3 :da 533 a 539 Azione : QVK PAN -- vento*0.4
			D3 :da 533 a 539 Azione : QVK PAN -- vento*0.4
			D3 :da 599 a 603 Azione : QVK PAN -- vento*0.4
			D3 :da 608 a 627 Azione : QVK PAN -- vento*0.4
			D3 :da 831 a 836 Azione : QVK PAN -- vento*0.4
			D3 :da 838 a 847 Azione : QVK PAN -- vento*0.4
			D3 :da 849 a 868 Azione : QVK PAN -- vento*0.4
			D3 : 917 Azione : QVK PAN -- vento*0.4
			D3 :da 920 a 940 Azione : QVK PAN -- vento*0.4
			D3 :da 961 a 969 Azione : QVK PAN -- vento*0.4
			D3 :da 973 a 990 Azione : QVK PAN -- vento*0.4
			D3 :da 1033 a 1034 Azione : QVK PAN -- vento*0.4
			D3 :da 1036 a 1038 Azione : QVK PAN -- vento*0.4
			D3 :da 1041 a 1042 Azione : QVK PAN -- vento*0.4
			D3 :da 1045 a 1046 Azione : QVK PAN -- vento*0.4
			D3 :da 1051 a 1057 Azione : QVK PAN -- vento*0.4
			D3 :da 1059 a 1062 Azione : QVK PAN -- vento*0.4
			D3 : 1066 Azione : QVK PAN -- vento*0.4
			D3 : 1066 Azione : QVK PAN -- vento*0.4
			D3 :da 1091 a 1092 Azione : QVK PAN -- vento*0.4
			D3 :da 1118 a 1122 Azione : QVK PAN -- vento*0.4
			D3 :da 1118 a 1122 Azione : QVK PAN -- vento*0.4
			D3 : 1173 Azione : QVK PAN -- vento*0.4
			D3 : 1219 Azione : QVK PAN -- vento*0.4
16	Qvk	CDC=Qvk (carico da vento) dir Y +	D3 :da 118 a 119 Azione : QVK PAN ++ vento*0.4
			D3 :da 118 a 119 Azione : QVK PAN ++ vento*0.4
			D3 :da 121 a 130 Azione : QVK PAN ++ vento*0.4
			D3 :da 121 a 130 Azione : QVK PAN ++ vento*0.4
			D3 :da 132 a 135 Azione : QVK PAN ++ vento*0.4
			D3 :da 132 a 135 Azione : QVK PAN ++ vento*0.4
			D3 : 137 Azione : QVK PAN ++ vento*0.4
			D3 : 137 Azione : QVK PAN ++ vento*0.4
			D3 :da 139 a 141 Azione : QVK PAN ++ vento*0.4
			D3 :da 139 a 141 Azione : QVK PAN ++ vento*0.4
			D3 :da 143 a 147 Azione : QVK PAN ++ vento*0.4
			D3 :da 143 a 147 Azione : QVK PAN ++ vento*0.4
			D3 :da 149 a 165 Azione : QVK PAN ++ vento*0.4
			D3 :da 149 a 165 Azione : QVK PAN ++ vento*0.4
			D3 :da 168 a 171 Azione : QVK PAN ++ vento*0.4
			D3 :da 168 a 171 Azione : QVK PAN ++ vento*0.4
			D3 : 173 Azione : QVK PAN ++ vento*0.4
			D3 : 173 Azione : QVK PAN ++ vento*0.4
			D3 :da 175 a 177 Azione : QVK PAN ++ vento*0.4
			D3 :da 175 a 177 Azione : QVK PAN ++ vento*0.4
			D3 :da 179 a 183 Azione : QVK PAN ++ vento*0.4
			D3 :da 179 a 183 Azione : QVK PAN ++ vento*0.4
			D3 : 185 Azione : QVK PAN ++ vento*0.4
			D3 : 185 Azione : QVK PAN ++ vento*0.4
			D3 :da 219 a 222 Azione : QVK PAN ++ vento*0.4
			D3 :da 219 a 222 Azione : QVK PAN ++ vento*0.4
			D3 :da 235 a 236 Azione : QVK PAN ++ vento*0.4
			D3 :da 235 a 236 Azione : QVK PAN ++ vento*0.4
			D3 :da 240 a 243 Azione : QVK PAN ++ vento*0.4
			D3 :da 240 a 243 Azione : QVK PAN ++ vento*0.4

CDC	Tipo	Sigla Id	Note
			D3 :da 247 a 251 Azione : QVK PAN ++ vento*0.4
			D3 :da 247 a 251 Azione : QVK PAN ++ vento*0.4
			D3 :da 264 a 265 Azione : QVK PAN ++ vento*0.4
			D3 :da 264 a 265 Azione : QVK PAN ++ vento*0.4
			D3 : 267 Azione : QVK PAN ++ vento*0.4
			D3 : 267 Azione : QVK PAN ++ vento*0.4
			D3 :da 283 a 285 Azione : QVK PAN ++ vento*0.4
			D3 :da 283 a 285 Azione : QVK PAN ++ vento*0.4
			D3 : 288 Azione : QVK PAN ++ vento*0.4
			D3 : 288 Azione : QVK PAN ++ vento*0.4
			D3 :da 290 a 292 Azione : QVK PAN ++ vento*0.4
			D3 :da 290 a 292 Azione : QVK PAN ++ vento*0.4
			D3 :da 294 a 298 Azione : QVK PAN ++ vento*0.4
			D3 :da 294 a 298 Azione : QVK PAN ++ vento*0.4
			D3 :da 300 a 304 Azione : QVK PAN ++ vento*0.4
			D3 :da 300 a 304 Azione : QVK PAN ++ vento*0.4
			D3 : 347 Azione : QVK PAN ++ vento*0.4
			D3 : 347 Azione : QVK PAN ++ vento*0.4
			D3 : 514 Azione : QVK PAN ++ vento*0.4
			D3 : 514 Azione : QVK PAN ++ vento*0.4
			D3 : 530 Azione : QVK PAN ++ vento*0.4
			D3 : 530 Azione : QVK PAN ++ vento*0.4
			D3 : 532 Azione : QVK PAN ++ vento*0.4
			D3 : 532 Azione : QVK PAN ++ vento*0.4
			D3 :da 540 a 562 Azione : QVK PAN ++ vento*0.4
			D3 :da 540 a 562 Azione : QVK PAN ++ vento*0.4
			D3 : 571 Azione : QVK PAN ++ vento*0.4
			D3 : 571 Azione : QVK PAN ++ vento*0.4
			D3 :da 670 a 723 Azione : QVK PAN ++ vento*0.4
			D3 :da 730 a 735 Azione : QVK PAN ++ vento*0.4
			D3 : 837 Azione : QVK PAN ++ vento*0.4
			D3 : 837 Azione : QVK PAN ++ vento*0.4
			D3 : 848 Azione : QVK PAN ++ vento*0.4
			D3 : 848 Azione : QVK PAN ++ vento*0.4
			D3 :da 869 a 899 Azione : QVK PAN ++ vento*0.4
			D3 :da 902 a 916 Azione : QVK PAN ++ vento*0.4
			D3 : 918 Azione : QVK PAN ++ vento*0.4
			D3 : 918 Azione : QVK PAN ++ vento*0.4
			D3 : 1050 Azione : QVK PAN ++ vento*0.4
			D3 : 1050 Azione : QVK PAN ++ vento*0.4
			D3 : 1058 Azione : QVK PAN ++ vento*0.4
			D3 : 1058 Azione : QVK PAN ++ vento*0.4
			D3 :da 1078 a 1082 Azione : QVK PAN ++ vento*0.4
			D3 :da 1095 a 1098 Azione : QVK PAN ++ vento*0.4
			D3 : 1123 Azione : QVK PAN ++ vento*0.4
			D3 : 1123 Azione : QVK PAN ++ vento*0.4
			D3 : 1126 Azione : QVK PAN ++ vento*0.4
			D3 : 1126 Azione : QVK PAN ++ vento*0.4
			D3 : 1131 Azione : QVK PAN ++ vento*0.4
			D3 : 1131 Azione : QVK PAN ++ vento*0.4
			D3 :da 1134 a 1135 Azione : QVK PAN ++ vento*0.4
			D3 :da 1134 a 1135 Azione : QVK PAN ++ vento*0.4
			D3 : 1137 Azione : QVK PAN ++ vento*0.4
			D3 : 1137 Azione : QVK PAN ++ vento*0.4
			D3 : 1139 Azione : QVK PAN ++ vento*0.4
			D3 : 1139 Azione : QVK PAN ++ vento*0.4
			D3 : 1146 Azione : QVK PAN ++ vento*0.4
			D3 : 1146 Azione : QVK PAN ++ vento*0.4
			D3 : 1149 Azione : QVK PAN ++ vento*0.4
			D3 : 1149 Azione : QVK PAN ++ vento*0.4
			D3 : 1158 Azione : QVK PAN ++ vento*0.4
			D3 : 1158 Azione : QVK PAN ++ vento*0.4
			D3 :da 1174 a 1176 Azione : QVK PAN ++ vento*0.4
			D3 :da 1174 a 1176 Azione : QVK PAN ++ vento*0.4
			D3 :da 1196 a 1208 Azione : QVK PAN ++ vento*0.4
			D3 :da 1215 a 1218 Azione : QVK PAN ++ vento*0.4
			D3 : 1221 Azione : QVK PAN ++ vento*0.4
17	Qvk	CDC=Qvk (carico da vento) dir Y -	D3 :da 118 a 119 Azione : QVK PAN -- vento*0.4

CDC	Tipo	Sigla Id	Note
			D3 :da 121 a 130 Azione : QVK PAN -- vento*0.4
			D3 :da 132 a 135 Azione : QVK PAN -- vento*0.4
			D3 : 137 Azione : QVK PAN -- vento*0.4
			D3 :da 139 a 141 Azione : QVK PAN -- vento*0.4
			D3 :da 143 a 147 Azione : QVK PAN -- vento*0.4
			D3 :da 149 a 165 Azione : QVK PAN -- vento*0.4
			D3 :da 168 a 171 Azione : QVK PAN -- vento*0.4
			D3 : 173 Azione : QVK PAN -- vento*0.4
			D3 :da 175 a 177 Azione : QVK PAN -- vento*0.4
			D3 :da 179 a 183 Azione : QVK PAN -- vento*0.4
			D3 : 185 Azione : QVK PAN -- vento*0.4
			D3 :da 219 a 222 Azione : QVK PAN -- vento*0.4
			D3 :da 235 a 236 Azione : QVK PAN -- vento*0.4
			D3 :da 240 a 243 Azione : QVK PAN -- vento*0.4
			D3 :da 247 a 251 Azione : QVK PAN -- vento*0.4
			D3 :da 264 a 265 Azione : QVK PAN -- vento*0.4
			D3 : 267 Azione : QVK PAN -- vento*0.4
			D3 :da 283 a 285 Azione : QVK PAN -- vento*0.4
			D3 : 288 Azione : QVK PAN -- vento*0.4
			D3 :da 290 a 292 Azione : QVK PAN -- vento*0.4
			D3 :da 294 a 298 Azione : QVK PAN -- vento*0.4
			D3 :da 300 a 304 Azione : QVK PAN -- vento*0.4
			D3 : 347 Azione : QVK PAN -- vento*0.4
			D3 : 514 Azione : QVK PAN -- vento*0.4
			D3 : 530 Azione : QVK PAN -- vento*0.4
			D3 : 532 Azione : QVK PAN -- vento*0.4
			D3 :da 540 a 562 Azione : QVK PAN -- vento*0.4
			D3 : 571 Azione : QVK PAN -- vento*0.4
			D3 :da 670 a 723 Azione : QVK PAN -- vento*0.4
			D3 :da 670 a 723 Azione : QVK PAN -- vento*0.4
			D3 :da 730 a 735 Azione : QVK PAN -- vento*0.4
			D3 :da 730 a 735 Azione : QVK PAN -- vento*0.4
			D3 : 837 Azione : QVK PAN -- vento*0.4
			D3 : 848 Azione : QVK PAN -- vento*0.4
			D3 :da 869 a 899 Azione : QVK PAN -- vento*0.4
			D3 :da 869 a 899 Azione : QVK PAN -- vento*0.4
			D3 :da 902 a 916 Azione : QVK PAN -- vento*0.4
			D3 :da 902 a 916 Azione : QVK PAN -- vento*0.4
			D3 : 918 Azione : QVK PAN -- vento*0.4
			D3 : 1050 Azione : QVK PAN -- vento*0.4
			D3 : 1058 Azione : QVK PAN -- vento*0.4
			D3 :da 1078 a 1082 Azione : QVK PAN -- vento*0.4
			D3 :da 1078 a 1082 Azione : QVK PAN -- vento*0.4
			D3 :da 1095 a 1098 Azione : QVK PAN -- vento*0.4
			D3 :da 1095 a 1098 Azione : QVK PAN -- vento*0.4
			D3 : 1123 Azione : QVK PAN -- vento*0.4
			D3 : 1126 Azione : QVK PAN -- vento*0.4
			D3 : 1131 Azione : QVK PAN -- vento*0.4
			D3 :da 1134 a 1135 Azione : QVK PAN -- vento*0.4
			D3 : 1137 Azione : QVK PAN -- vento*0.4
			D3 : 1139 Azione : QVK PAN -- vento*0.4
			D3 : 1146 Azione : QVK PAN -- vento*0.4
			D3 : 1149 Azione : QVK PAN -- vento*0.4
			D3 : 1158 Azione : QVK PAN -- vento*0.4
			D3 :da 1174 a 1176 Azione : QVK PAN -- vento*0.4
			D3 :da 1196 a 1208 Azione : QVK PAN -- vento*0.4
			D3 :da 1196 a 1208 Azione : QVK PAN -- vento*0.4
			D3 :da 1215 a 1218 Azione : QVK PAN -- vento*0.4
			D3 :da 1215 a 1218 Azione : QVK PAN -- vento*0.4
			D3 : 1221 Azione : QVK PAN -- vento*0.4
			D3 : 1221 Azione : QVK PAN -- vento*0.4

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente.

Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: *Numero, Tipo, Sigla identificativa*. Una seconda tabella riporta il *peso nella combinazione* assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G_1 \cdot G_1 + \gamma G_2 \cdot G_2 + \gamma P \cdot P + \gamma Q_1 \cdot Q_{k1} + \gamma Q_2 \cdot \psi_{02} \cdot Q_{k2} + \gamma Q_3 \cdot \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2008 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli ≤ 30 kN)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli > 30 kN)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2008 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11	
12	SLU	Comb. SLU A1 12	
13	SLU	Comb. SLU A1 13	
14	SLU	Comb. SLU A1 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLU	Comb. SLU A1 (SLV sism.) 41	
42	SLU	Comb. SLU A1 (SLV sism.) 42	
43	SLU	Comb. SLU A1 (SLV sism.) 43	
44	SLU	Comb. SLU A1 (SLV sism.) 44	
45	SLU	Comb. SLU A1 (SLV sism.) 45	
46	SLU	Comb. SLU A1 (SLV sism.) 46	
47	SLD(sis)	Comb. SLE (SLO Operativo sism.) 47	
48	SLD(sis)	Comb. SLE (SLO Operativo sism.) 48	
49	SLD(sis)	Comb. SLE (SLO Operativo sism.) 49	
50	SLD(sis)	Comb. SLE (SLO Operativo sism.) 50	
51	SLD(sis)	Comb. SLE (SLO Operativo sism.) 51	
52	SLD(sis)	Comb. SLE (SLO Operativo sism.) 52	
53	SLD(sis)	Comb. SLE (SLO Operativo sism.) 53	
54	SLD(sis)	Comb. SLE (SLO Operativo sism.) 54	
55	SLD(sis)	Comb. SLE (SLO Operativo sism.) 55	
56	SLD(sis)	Comb. SLE (SLO Operativo sism.) 56	
57	SLD(sis)	Comb. SLE (SLO Operativo sism.) 57	
58	SLD(sis)	Comb. SLE (SLO Operativo sism.) 58	
59	SLD(sis)	Comb. SLE (SLO Operativo sism.) 59	
60	SLD(sis)	Comb. SLE (SLO Operativo sism.) 60	
61	SLD(sis)	Comb. SLE (SLO Operativo sism.) 61	
62	SLD(sis)	Comb. SLE (SLO Operativo sism.) 62	
63	SLD(sis)	Comb. SLE (SLO Operativo sism.) 63	
64	SLD(sis)	Comb. SLE (SLO Operativo sism.) 64	

Cmb	Tipo	Sigla Id	effetto P-delta
65	SLD(sis)	Comb. SLE (SLO Operativo sism.) 65	
66	SLD(sis)	Comb. SLE (SLO Operativo sism.) 66	
67	SLD(sis)	Comb. SLE (SLO Operativo sism.) 67	
68	SLD(sis)	Comb. SLE (SLO Operativo sism.) 68	
69	SLD(sis)	Comb. SLE (SLO Operativo sism.) 69	
70	SLD(sis)	Comb. SLE (SLO Operativo sism.) 70	
71	SLD(sis)	Comb. SLE (SLO Operativo sism.) 71	
72	SLD(sis)	Comb. SLE (SLO Operativo sism.) 72	
73	SLD(sis)	Comb. SLE (SLO Operativo sism.) 73	
74	SLD(sis)	Comb. SLE (SLO Operativo sism.) 74	
75	SLD(sis)	Comb. SLE (SLO Operativo sism.) 75	
76	SLD(sis)	Comb. SLE (SLO Operativo sism.) 76	
77	SLD(sis)	Comb. SLE (SLO Operativo sism.) 77	
78	SLD(sis)	Comb. SLE (SLO Operativo sism.) 78	
79	SLU(acc.)	Comb. SLU (Accid.) 79	
80	SLE(r)	Comb. SLE(rara) 80	
81	SLE(r)	Comb. SLE(rara) 81	
82	SLE(r)	Comb. SLE(rara) 82	
83	SLE(r)	Comb. SLE(rara) 83	
84	SLE(r)	Comb. SLE(rara) 84	
85	SLE(r)	Comb. SLE(rara) 85	
86	SLE(r)	Comb. SLE(rara) 86	
87	SLE(f)	Comb. SLE(freq.) 87	
88	SLE(f)	Comb. SLE(freq.) 88	
89	SLE(f)	Comb. SLE(freq.) 89	
90	SLE(p)	Comb. SLE(perm.) 90	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
2	1.00	1.00	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
3	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.50	0.0
	0.0	0.0	0.0											
4	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.50	0.0
	0.0	0.0	0.0											
5	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	1.50
	0.0	0.0	0.0											
6	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	1.50
	0.0	0.0	0.0											
7	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
8	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
9	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	1.50	0.0	0.0											
10	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	1.50	0.0	0.0											
11	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	1.50	0.0											
12	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	1.50	0.0											
13	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	1.50											
14	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	1.50											
15	1.00	1.00	1.00	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
16	1.00	1.00	1.00	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
17	1.00	1.00	1.00	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
18	1.00	1.00	1.00	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
19	1.00	1.00	1.00	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0											
20	1.00	1.00	1.00	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
21	1.00	1.00	1.00	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
22	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
23	1.00	1.00	1.00	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
24	1.00	1.00	1.00	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
25	1.00	1.00	1.00	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
26	1.00	1.00	1.00	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
27	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
28	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
29	1.00	1.00	1.00	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
30	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
31	1.00	1.00	1.00	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
32	1.00	1.00	1.00	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
33	1.00	1.00	1.00	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
34	1.00	1.00	1.00	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
35	1.00	1.00	1.00	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
36	1.00	1.00	1.00	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
37	1.00	1.00	1.00	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
38	1.00	1.00	1.00	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
39	1.00	1.00	1.00	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
40	1.00	1.00	1.00	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
41	1.00	1.00	1.00	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
42	1.00	1.00	1.00	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
43	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
44	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
45	1.00	1.00	1.00	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
46	1.00	1.00	1.00	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
47	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
48	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
49	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
50	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
51	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
52	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
53	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
54	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											
55	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
56	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
57	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
58	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
59	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
60	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											
61	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
62	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											
63	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
64	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
65	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
66	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
67	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
68	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
69	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
70	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
71	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
72	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
73	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
74	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
75	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
76	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
77	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
78	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
79	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											
80	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	0.0	0.0	0.0											
81	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0
	0.0	0.0	0.0											
82	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	1.00
	0.0	0.0	0.0											
83	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	0.0	0.0	0.0											
84	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	1.00	0.0	0.0											
85	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	0.0	1.00	0.0											
86	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	1.00											
87	1.00	1.00	1.00	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											
88	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.50	0.0
	0.0	0.0	0.0											
89	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											
90	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											

AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

ag: accelerazione orizzontale massima del terreno;

Fo: valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T*c: periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	50.0	1.5	75.0	C	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche

mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.5)

Fo è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

Fv è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno ag su sito di riferimento rigido orizzontale

Tb è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

Tc è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

Td è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	11.363	44.575	
16508	11.316	44.565	3.873
16509	11.386	44.566	2.072
16287	11.384	44.616	4.837
16286	11.314	44.615	5.883

SL	Pver	Tr	ag	Fo	T*c
		Anni	g		sec
SLO	81.0	45.0	0.059	2.500	0.270
SLD	63.0	75.0	0.074	2.480	0.280
SLV	10.0	712.0	0.194	2.470	0.290
SLC	5.0	1462.0	0.251	2.440	0.290

SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.059	1.500	2.500	0.821	0.146	0.437	1.837
SLD	0.074	1.500	2.480	0.910	0.149	0.447	1.896
SLV	0.194	1.413	2.470	1.467	0.153	0.458	2.374
SLC	0.251	1.332	2.440	1.652	0.153	0.458	2.606

RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

- | | |
|----------------|--|
| 9. Esk | caso di carico sismico con analisi statica equivalente |
| 10. Edk | caso di carico sismico con analisi dinamica |

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore di struttura q	Fattore dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

- a) **analisi sismica statica equivalente:**
 - quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - azione sismica complessiva
- b) **analisi sismica dinamica con spettro di risposta:**
 - quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
 - massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione η_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \eta_T / h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione η_T , η_P e η_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \eta_T / h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo l' allegato 10.A dell'Ordinanza 3274 e smi. In particolare la tabella, per ogni combinazione SLU (SLC per il DM 14-01-2008) sismica riporta il codice di verifica e i valori utilizzati per la verifica: spostamento dE, area ridotta e dimensione A2, azione verticale, deformazioni di taglio dell' elastomero e tensioni nell' acciaio.

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva, NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta Ar (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio

Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig s} < f_{yk}$
- 3) $\text{Gam t} < 5$
- 4) $\text{Gam s} < \text{Gam}^*$ (caratteristica dell' elastomero)
- 5) $\text{Gam s} < 2$
- 6) $V < 0.5 V_{cr}$

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
23	DM 2008: SPETTRO
29	SISMICA 1000/H, SOMMA V, EFFETTO P-δ
30	ANALISI DI UN EDIFICIO CON ISOLATORI SISMICI
70	MASSE SISMICHE
75	PROGETTO DI ISOLATORI ELASTOMERICI
76	VERIFICA DI ISOLATORI ELASTOMERICI
77	VERIFICA DI ISOLATORI FRICTION PENDULUM

CDC	Tipo	Sigla Id	Note
5	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.120 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 4.817
			classe di duttilità CD: B
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	0.0	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	0.0	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.35	42.83	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	0.0	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	0.0	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	0.0	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	0.0	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	0.0	-0.42	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	0.0	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	0.0	0.0	10.35	9.50	0.082	1.084	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
2.72	40.72	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	0.0	-0.58	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	0.0	-0.42	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	0.0	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	0.0	-0.80	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	0.0	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	0.0	-0.42	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	0.0	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	0.0	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	0.0	-0.52	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.80	17.25	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.841	0.543	0.285	5.37e-04	0.0	2.566e+04	18.1	1.64	1.16e-03	0.0	0.0
2	2.085	0.480	0.323	41.65	2.93e-02	1.043e+04	7.3	0.37	2.64e-04	0.0	0.0
3	2.220	0.450	0.338	3.27	2.30e-03	6778.43	4.8	0.20	1.39e-04	0.0	0.0
4	2.367	0.423	0.338	3.15	2.22e-03	2.097e+04	14.8	1.20	8.43e-04	0.0	0.0
5	3.545	0.282	0.338	3515.72	2.5	11.37	8.00e-03	0.15	1.04e-04	0.0	0.0
6	4.042	0.247	0.338	25.18	1.77e-02	3.276e+04	23.1	28.67	2.02e-02	0.0	0.0
7	4.720	0.212	0.338	5.888e+04	41.4	50.72	3.57e-02	131.42	9.25e-02	0.0	0.0
8	5.183	0.193	0.338	399.12	0.3	439.06	0.3	7956.35	5.6	0.0	0.0
9	6.244	0.160	0.338	368.10	0.3	703.37	0.5	2.310e+04	16.3	0.0	0.0
10	8.334	0.120	0.324	7.169e+04	50.5	62.83	4.42e-02	49.18	3.46e-02	0.0	0.0
11	9.191	0.109	0.319	83.23	5.86e-02	3.100e+04	21.8	30.14	2.12e-02	0.0	0.0
12	12.568	0.080	0.307	0.61	4.28e-04	20.14	1.42e-02	9.760e+04	68.7	0.0	0.0
Risulta				1.350e+05		1.289e+05		1.289e+05			
In percentuale				95.03		90.72		90.73			

CDC	Tipo	Sigla Id	Note
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.120 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 4.825
			classe di duttilità CD: B
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	0.0	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.75	419.65	24.03	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	0.0	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	0.0	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	0.0	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	0.0	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	0.0	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	0.0	0.42	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	0.0	0.16	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	0.0	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.00	34.54	39.50	13.61	0.0	0.22	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	0.0	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	0.0	0.58	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	0.0	0.42	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	0.0	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	0.0	0.80	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	0.0	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	0.0	0.42	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	0.0	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.91	734.19	15.09	9.50	0.0	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	0.0	0.52	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.841	0.543	0.285	5.52e-04	0.0	2.566e+04	18.1	1.64	1.16e-03	0.0	0.0
2	2.085	0.480	0.323	46.29	3.26e-02	1.043e+04	7.3	0.38	2.65e-04	0.0	0.0
3	2.220	0.450	0.338	3.21	2.26e-03	6781.00	4.8	0.20	1.39e-04	0.0	0.0
4	2.367	0.423	0.338	3.43	2.41e-03	2.096e+04	14.8	1.20	8.43e-04	0.0	0.0
5	3.604	0.278	0.338	3931.89	2.8	16.21	1.14e-02	0.21	1.51e-04	0.0	0.0
6	4.042	0.247	0.338	30.19	2.12e-02	3.277e+04	23.1	28.70	2.02e-02	0.0	0.0
7	4.788	0.209	0.338	6.233e+04	43.9	66.96	4.71e-02	206.34	0.1	0.0	0.0
8	5.188	0.193	0.338	924.22	0.7	421.52	0.3	7961.75	5.6	0.0	0.0
9	6.249	0.160	0.338	257.78	0.2	705.37	0.5	2.306e+04	16.2	0.0	0.0
10	8.351	0.120	0.324	6.648e+04	46.8	95.46	6.72e-02	31.34	2.21e-02	0.0	0.0
11	9.194	0.109	0.319	140.24	9.87e-02	3.095e+04	21.8	29.19	2.05e-02	0.0	0.0
12	12.571	0.080	0.307	0.39	2.72e-04	20.90	1.47e-02	9.760e+04	68.7	0.0	0.0
Risulta				1.341e+05		1.289e+05		1.289e+05			
In percentuale				94.42		90.72		90.74			

CDC	Tipo	Sigla Id	Note
7	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.269 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 2.704
			classe di duttilità CD: B
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	1.98	0.0	19.75	9.50	0.042	0.074	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	1.63	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	1.98	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	1.98	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	1.63	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	1.98	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	1.93	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	1.98	0.0	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.20	388.37	19.68	2.48	1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	1.98	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	1.80	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	1.83	0.0	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	1.98	0.0	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	1.98	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	1.98	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	1.86	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	1.98	0.0	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	1.98	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	1.86	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	1.98	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.065	0.484	0.320	0.01	7.53e-06	2.104e+04	14.8	2.23	1.57e-03	0.0	0.0
2	2.154	0.464	0.333	0.64	4.53e-04	609.90	0.4	0.85	6.02e-04	0.0	0.0
3	2.202	0.454	0.338	51.52	3.63e-02	7200.96	5.1	0.21	1.47e-04	0.0	0.0
4	2.289	0.437	0.338	7.39	5.20e-03	2.997e+04	21.1	0.53	3.74e-04	0.0	0.0
5	3.568	0.280	0.338	3287.09	2.3	2580.17	1.8	1.39	9.78e-04	0.0	0.0
6	3.721	0.269	0.338	484.54	0.3	3.087e+04	21.7	39.46	2.78e-02	0.0	0.0
7	4.749	0.211	0.338	5.894e+04	41.5	240.93	0.2	214.89	0.2	0.0	0.0
8	5.065	0.197	0.338	1486.32	1.0	3436.30	2.4	4487.70	3.2	0.0	0.0
9	6.020	0.166	0.338	160.00	0.1	2736.86	1.9	2.467e+04	17.4	0.0	0.0
10	8.357	0.120	0.324	6.863e+04	48.3	796.86	0.6	16.98	1.19e-02	0.0	0.0
11	8.694	0.115	0.322	1744.74	1.2	2.779e+04	19.6	1471.50	1.0	0.0	0.0
12	12.445	0.080	0.307	1.72	1.21e-03	106.16	7.47e-02	9.716e+04	68.4	0.0	0.0
Risulta				1.348e+05		1.274e+05		1.281e+05			
In percentuale				94.88		89.66		90.15			

CDC	Tipo	Sigla Id	Note
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.596 sec.

CDC	Tipo	Sigla Id	Note
			fattore di struttura q: 2.000
			fattore per spost. mu d: 2.000
			classe di duttilità CD: B
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	-1.98	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	-1.63	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	-1.98	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	-1.98	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	-1.63	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	-1.98	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	-1.93	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	-1.55	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.40	7.580e+04	18.35	12.78	-1.98	0.0	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	-1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	-1.98	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	-0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	-1.80	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	-1.83	0.0	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	-1.98	0.0	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	-1.98	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	-0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	-1.98	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	-1.86	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
1.70	1829.48	18.25	13.81	-1.98	0.0	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	-1.98	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	-1.86	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	-1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	-1.98	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.677	0.596	0.259	6.96e-04	0.0	3.071e+04	21.6	1.31	9.20e-04	0.0	0.0
2	1.987	0.503	0.307	38.25	2.69e-02	1.249e+04	8.8	0.30	2.13e-04	0.0	0.0
3	2.250	0.444	0.338	3.66	2.58e-03	1.275e+04	9.0	0.04	2.93e-05	0.0	0.0
4	2.521	0.397	0.338	2.04	1.44e-03	1.306e+04	9.2	1.73	1.22e-03	0.0	0.0
5	3.560	0.281	0.338	3581.74	2.5	70.20	4.94e-02	0.56	3.93e-04	0.0	0.0
6	4.183	0.239	0.338	26.90	1.89e-02	2.519e+04	17.7	2.34	1.64e-03	0.0	0.0
7	4.747	0.211	0.338	6.004e+04	42.3	0.15	1.04e-04	106.28	7.48e-02	0.0	0.0
8	5.340	0.187	0.338	174.20	0.1	1206.92	0.8	1.337e+04	9.4	0.0	0.0
9	6.578	0.152	0.337	791.61	0.6	3220.47	2.3	1.796e+04	12.6	0.0	0.0
10	8.327	0.120	0.324	6.516e+04	45.9	2323.85	1.6	29.18	2.05e-02	0.0	0.0
11	8.774	0.114	0.321	4860.66	3.4	2.519e+04	17.7	6331.56	4.5	0.0	0.0
12	13.093	0.076	0.306	46.61	3.28e-02	1242.76	0.9	9.325e+04	65.6	0.0	0.0
Risulta				1.347e+05		1.275e+05		1.311e+05			
In percentuale				94.83		89.72		92.24			

CDC	Tipo	Sigla Id	Note
9	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.120 sec.
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	0.0	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	0.0	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	0.0	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	0.0	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	0.0	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	0.0	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.45	69.89	20.92	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	0.0	-0.42	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	0.0	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	0.0	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	0.0	-0.58	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	0.0	-0.42	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	0.0	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	0.0	-0.80	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	0.0	0.0	12.82	9.50	0.071	0.244	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	0.0	-0.42	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	0.0	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	0.0	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	0.0	-0.52	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.841	0.543	0.179	5.37e-04	0.0	2.566e+04	18.1	1.64	1.16e-03	0.0	0.0
2	2.085	0.480	0.202	41.65	2.93e-02	1.043e+04	7.3	0.37	2.64e-04	0.0	0.0
3	2.220	0.450	0.215	3.27	2.30e-03	6778.43	4.8	0.20	1.39e-04	0.0	0.0
4	2.367	0.423	0.222	3.15	2.22e-03	2.097e+04	14.8	1.20	8.43e-04	0.0	0.0
5	3.545	0.282	0.222	3515.72	2.5	11.37	8.00e-03	0.15	1.04e-04	0.0	0.0
6	4.042	0.247	0.222	25.18	1.77e-02	3.276e+04	23.1	28.67	2.02e-02	0.0	0.0
7	4.720	0.212	0.222	5.888e+04	41.4	50.72	3.57e-02	131.42	9.25e-02	0.0	0.0
8	5.183	0.193	0.222	399.12	0.3	439.06	0.3	7956.35	5.6	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
9	6.244	0.160	0.222	368.10	0.3	703.37	0.5	2.310e+04	16.3	0.0	0.0
10	8.334	0.120	0.198	7.169e+04	50.5	62.83	4.42e-02	49.18	3.46e-02	0.0	0.0
11	9.191	0.109	0.188	83.23	5.86e-02	3.100e+04	21.8	30.14	2.12e-02	0.0	0.0
12	12.568	0.080	0.161	0.61	4.28e-04	20.14	1.42e-02	9.760e+04	68.7	0.0	0.0
Risulta				1.350e+05		1.289e+05		1.289e+05			
In percentuale				95.03		90.72		90.73			

CDC	Tipo	Sigla Id	Note
10	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.120 sec.
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	0.0	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	0.0	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	0.0	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	0.0	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	0.0	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.64	755.59	17.36	9.50	0.0	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	0.0	0.42	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	0.0	0.16	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	0.0	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	0.22	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	0.0	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	0.0	0.58	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	0.0	0.42	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	0.0	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	0.0	0.80	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
2.15	78.81	2.11	18.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	0.0	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	0.0	0.42	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	0.0	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	0.0	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	0.0	0.52	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	0.0	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
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Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.841	0.543	0.179	5.52e-04	0.0	2.566e+04	18.1	1.64	1.16e-03	0.0	0.0
2	2.085	0.480	0.202	46.29	3.26e-02	1.043e+04	7.3	0.38	2.65e-04	0.0	0.0
3	2.220	0.450	0.215	3.21	2.26e-03	6781.00	4.8	0.20	1.39e-04	0.0	0.0
4	2.367	0.423	0.222	3.43	2.41e-03	2.096e+04	14.8	1.20	8.43e-04	0.0	0.0
5	3.604	0.278	0.222	3931.89	2.8	16.21	1.14e-02	0.21	1.51e-04	0.0	0.0
6	4.042	0.247	0.222	30.19	2.12e-02	3.277e+04	23.1	28.70	2.02e-02	0.0	0.0
7	4.788	0.209	0.222	6.233e+04	43.9	66.96	4.71e-02	206.34	0.1	0.0	0.0
8	5.188	0.193	0.222	924.22	0.7	421.52	0.3	7961.75	5.6	0.0	0.0
9	6.249	0.160	0.222	257.78	0.2	705.37	0.5	2.306e+04	16.2	0.0	0.0
10	8.351	0.120	0.198	6.648e+04	46.8	95.46	6.72e-02	31.34	2.21e-02	0.0	0.0
11	9.194	0.109	0.188	140.24	9.87e-02	3.095e+04	21.8	29.19	2.05e-02	0.0	0.0
12	12.571	0.080	0.161	0.39	2.72e-04	20.90	1.47e-02	9.760e+04	68.7	0.0	0.0
Risulta				1.341e+05		1.289e+05		1.289e+05			
In percentuale				94.42		90.72		90.74			

CDC	Tipo	Sigla Id	Note
11	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.269 sec.
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	1.98	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	1.63	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	1.98	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	1.98	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	58.55	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	1.63	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.95	184.05	19.92	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	1.98	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	1.93	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	1.98	0.0	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	1.98	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	1.80	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
2.60	828.14	21.28	9.42	1.83	0.0	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	1.98	0.0	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
2.46	147.90	15.84	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	1.98	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	1.98	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	1.86	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	1.98	0.0	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	1.98	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	1.86	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	1.40	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.73	128.98	21.21	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.64	94.63	18.33	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	1.98	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.065	0.484	0.200	0.01	7.53e-06	2.104e+04	14.8	2.23	1.57e-03	0.0	0.0
2	2.154	0.464	0.209	0.64	4.53e-04	609.90	0.4	0.85	6.02e-04	0.0	0.0
3	2.202	0.454	0.214	51.52	3.63e-02	7200.96	5.1	0.21	1.47e-04	0.0	0.0
4	2.289	0.437	0.222	7.39	5.20e-03	2.997e+04	21.1	0.53	3.74e-04	0.0	0.0
5	3.568	0.280	0.222	3287.09	2.3	2580.17	1.8	1.39	9.78e-04	0.0	0.0
6	3.721	0.269	0.222	484.54	0.3	3.087e+04	21.7	39.46	2.78e-02	0.0	0.0
7	4.749	0.211	0.222	5.894e+04	41.5	240.93	0.2	214.89	0.2	0.0	0.0
8	5.065	0.197	0.222	1486.32	1.0	3436.30	2.4	4487.70	3.2	0.0	0.0
9	6.020	0.166	0.222	160.00	0.1	2736.86	1.9	2.467e+04	17.4	0.0	0.0
10	8.357	0.120	0.198	6.863e+04	48.3	796.86	0.6	16.98	1.19e-02	0.0	0.0
11	8.694	0.115	0.194	1744.74	1.2	2.779e+04	19.6	1471.50	1.0	0.0	0.0
12	12.445	0.080	0.162	1.72	1.21e-03	106.16	7.47e-02	9.716e+04	68.4	0.0	0.0
Risulta				1.348e+05		1.274e+05		1.281e+05			
In percentuale				94.88		89.66		90.15			

CDC	Tipo	Sigla Id	Note
12	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.596 sec.
			numero di modi considerati: 12
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.320e+04	18.91	9.50	-1.98	0.0	19.75	9.50	0.042	0.074	0.0
5.33	15.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	354.31	18.42	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.22	76.66	27.33	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.20	53.10	12.55	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
5.16	6.60	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	305.03	19.25	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	91.12	16.88	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.92	365.38	18.36	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.82	75.09	27.33	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.76	44.41	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	419.65	24.03	9.50	-1.63	0.0	0.0	0.0	0.0	0.0	0.0
4.74	319.72	19.04	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	88.53	16.84	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	303.68	18.28	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.55	1236.87	17.24	9.50	-1.98	0.0	16.32	9.50	0.047	0.091	0.0
4.46	73.62	27.33	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.44	34.58	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.40	228.08	19.76	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.37	270.71	18.60	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	27.31	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.35	42.83	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.33	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.799e+04	19.15	3.20	-1.98	0.0	20.46	3.20	0.032	0.167	0.0
4.25	176.82	20.09	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.22	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	105.63	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.11	58.55	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.10	211.44	19.34	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.08	58.45	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	470.46	23.90	9.50	-1.63	0.0	23.85	9.50	0.055	0.004	0.0
4.01	39.69	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.01	170.39	19.67	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.97	19.74	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	184.05	19.92	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	175.58	19.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	56.51	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.80	22.73	36.52	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	160.61	19.28	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.72	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.65	6074.14	19.71	0.0	-1.98	0.0	20.22	0.0	0.066	0.039	0.0
3.64	148.26	19.56	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.64	755.59	17.36	9.50	-1.93	0.0	17.22	9.50	0.047	0.014	0.0
3.64	11.28	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	29.65	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	248.41	19.80	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.53	24.38	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	233.32	19.78	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.49	92.50	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.48	42.78	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.89	20.92	-1.04	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.44	127.20	20.58	-1.12	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.43	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.42	138.31	20.25	-1.22	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	50.54	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.40	148.42	19.92	-1.31	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.580e+04	18.35	12.78	-1.98	0.0	19.79	12.52	0.811	0.095	0.027
3.40	174.42	19.99	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.39	157.83	19.58	-1.39	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.38	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.60	19.25	-1.48	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	177.90	18.92	-1.57	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.34	145.18	19.67	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.33	111.52	18.58	-1.66	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.28	205.78	19.17	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.21	35.63	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	15.26	11.23	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	388.37	19.68	2.48	-1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.19	146.48	19.34	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.18	46.66	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.18	17.61	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.16	179.96	20.13	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.12	7.28	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.06	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.05	7.91	23.64	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	420.86	20.31	0.0	-1.98	0.0	20.74	0.0	0.107	0.033	0.0
3.04	152.64	19.84	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.00	34.54	39.50	13.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.98	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.92	143.13	19.96	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.91	8.47	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	36.47	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.84	296.98	19.95	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.80	90.57	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	45.01	2.13	18.00	-0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.74	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.73	682.67	19.47	9.50	-1.80	0.0	10.35	9.50	0.082	1.084	0.0
2.72	40.72	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.67	126.76	19.45	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.67	30.77	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.66	13.96	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.64	215.27	19.34	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
2.60	828.14	21.28	9.42	-1.83	0.0	22.22	9.50	0.026	0.362	0.264
2.58	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.55	129.86	19.10	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.55	1708.00	17.65	13.86	-1.98	0.0	9.02	14.65	0.408	1.147	0.166
2.55	107.67	15.33	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.54	34.04	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.53	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.46	147.90	15.84	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.43	512.62	20.10	0.0	-1.98	0.0	20.22	0.0	0.066	0.009	0.0
2.37	161.81	21.49	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.35	225.59	14.37	7.88	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.29	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.29	34.97	8.50	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	123.10	22.56	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.19	128.98	21.21	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.15	78.81	2.11	18.00	-0.08	0.0	0.0	0.0	0.0	0.0	0.0
2.13	283.58	21.18	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.10	92.50	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.06	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.01	76.81	18.33	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.92	94.63	18.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.90	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.82	504.94	20.12	0.0	-1.98	0.0	20.22	0.0	0.066	0.007	0.0
1.82	716.98	14.98	9.50	-1.86	0.0	12.82	9.50	0.071	0.244	0.0
1.78	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.77	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	20.93	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.76	219.94	19.55	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.74	14.91	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
1.70	1829.48	18.25	13.81	-1.98	0.0	10.58	14.76	0.535	0.817	0.151
1.70	107.67	15.33	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.69	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.64	148.47	15.81	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.61	18.80	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.59	18.52	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.58	162.33	21.51	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.53	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	123.10	22.56	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.49	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.46	128.98	21.21	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.45	12.70	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	322.85	19.64	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.40	94.43	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.37	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.36	36.23	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.34	76.81	18.33	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.28	94.63	18.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.27	53.94	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.22	508.69	20.13	0.0	-1.98	0.0	20.22	0.0	0.066	0.006	0.0
0.95	44.08	36.52	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.91	734.19	15.09	9.50	-1.86	0.0	12.82	9.50	0.071	0.256	0.0
0.89	31.30	36.52	8.82	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.89	19.51	8.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	21.76	15.00	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	218.36	19.36	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.87	14.96	27.50	8.22	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	36.75	20.22	8.14	-1.40	0.0	0.0	0.0	0.0	0.0	0.0
0.85	2055.31	17.06	13.73	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.20	18.33	7.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	147.90	15.84	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	17.25	27.50	6.12	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.79	16.80	8.50	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.79	161.81	21.49	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	57.02	18.33	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	123.10	22.56	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.74	36.75	27.50	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.73	128.98	21.21	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.73	10.20	8.50	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	318.55	19.79	3.20	-1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.70	92.50	19.88	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.69	50.73	18.33	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.68	30.99	21.17	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.67	76.81	18.33	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	94.63	18.33	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.64	42.69	21.17	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.61	504.94	20.12	0.0	-1.98	0.0	20.22	0.0	0.066	0.007	0.0
Risulta	1.421e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.677	0.596	0.163	6.96e-04	0.0	3.071e+04	21.6	1.31	9.20e-04	0.0	0.0
2	1.987	0.503	0.193	38.25	2.69e-02	1.249e+04	8.8	0.30	2.13e-04	0.0	0.0
3	2.250	0.444	0.218	3.66	2.58e-03	1.275e+04	9.0	0.04	2.93e-05	0.0	0.0
4	2.521	0.397	0.222	2.04	1.44e-03	1.306e+04	9.2	1.73	1.22e-03	0.0	0.0
5	3.560	0.281	0.222	3581.74	2.5	70.20	4.94e-02	0.56	3.93e-04	0.0	0.0
6	4.183	0.239	0.222	26.90	1.89e-02	2.519e+04	17.7	2.34	1.64e-03	0.0	0.0
7	4.747	0.211	0.222	6.004e+04	42.3	0.15	1.04e-04	106.28	7.48e-02	0.0	0.0
8	5.340	0.187	0.222	174.20	0.1	1206.92	0.8	1.337e+04	9.4	0.0	0.0
9	6.578	0.152	0.222	791.61	0.6	3220.47	2.3	1.796e+04	12.6	0.0	0.0
10	8.327	0.120	0.198	6.516e+04	45.9	2323.85	1.6	29.18	2.05e-02	0.0	0.0
11	8.774	0.114	0.193	4860.66	3.4	2.519e+04	17.7	6331.56	4.5	0.0	0.0
12	13.093	0.076	0.158	46.61	3.28e-02	1242.76	0.9	9.325e+04	65.6	0.0	0.0
Risulta				1.347e+05		1.275e+05		1.311e+05			
In percentuale				94.83		89.72		92.24			

Cmb	Pilas. 1000 etaT/h	etaT	inter. h	Pilas. 1000 etaT/h	etaT	inter. h	Pilas. 1000 etaT/h	etaT	inter. h
		cm	cm		cm	cm		cm	cm
47	9	0.81	340.0	43	0.43	340.0	56	0.54	340.0
	57	0.66	340.0	59	0.18	340.0	119	0.67	340.0
	134	0.59	340.0	138	0.58	340.0	140	0.09	340.0
...									
78	178	0.78	340.0	526	4.10	340.0	527	4.10	340.0
Cmb	1000 etaT/h								
	4.11								

RISULTATI NODALI

LEGENDA RISULTATI NODALI

Il controllo dei risultati delle analisi condotte, per quanto concerne i nodi strutturali, è possibile in relazione alle tabelle sottoportate.

Una prima tabella riporta infatti per ogni nodo e per ogni combinazione (o caso di carico) gli spostamenti nodali.

Una seconda tabella riporta per ogni nodo a cui sia associato un vincolo rigido e/o elastico o una fondazione speciale e per ogni combinazione (o caso di carico) i valori delle azioni esercitate dalla struttura sui vincoli (reazioni vincolari cambiate di segno).

Una terza tabella, infine riassume per ogni nodo le sei combinazioni in cui si attingono i valori minimi e massimi della reazione Fz, della reazione Mx e della reazione My.

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
		cm	cm	cm			
1	1	0.02	-1.02e-03	-0.35	-1.45e-05	0.0	-5.08e-04
1	5	0.03	1.32e-03	-0.31	-2.22e-05	0.0	-3.69e-04
1	14	9.90e-03	-0.02	-0.22	3.30e-05	0.0	3.43e-05
...							
1738	90	3.53e-03	0.03	-0.28	-5.80e-05	0.0	2.84e-05
Nodo		Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
		-3.01	-4.13	-4.82	-0.01	-9.37e-03	-0.02
		2.44	3.80	0.47	0.03	9.42e-03	0.02

RISULTATI OPERE DI FONDAZIONE

LEGENDA RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sotto riportate.

La prima tabella è riferita alle fondazioni tipo palo e plinto su pali.

Per questo tipo di fondazione vengono riportate le sei componenti di sollecitazione (esprese nel riferimento globale della struttura) per ogni palo componente l'opera.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	codice corrispondente al nome assegnato al tipo di plinto di fondazione: 3) palo singolo (<i>PALO</i>) 4) plinto su palo 5) plinto su due pali (<i>PL.2P</i>) 6) plinto su tre pali (<i>PL.3P</i>) 7) plinto su quattro pali (<i>PL.4P</i>) 8) plinto rettangolare su cinque pali (<i>PL.5P.R</i>) 9) plinto pentagonale su cinque pali (<i>PL.5P</i>) 10) plinto su sei pali (<i>PL.6P</i>)
Palo	numero del palo
Comb.	combinazione di carico in cui si verificano le sei componenti di sollecitazione.
Quota	quota assoluta della sezione del palo per cui si riportano le sei componenti di sollecitazione.

L'azione F_z (corrispondente allo sforzo normale nel palo) è costante poiché il peso del palo stesso non è considerato nella modellazione.

La seconda tabella è riferita alle fondazioni tipo plinto su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni nei quattro vertici dell'impronta sul terreno.

In particolare viene riportato:

Nodo		numero del nodo a cui è applicato il plinto
Tipo		Codice identificativo del nome assegnato al plinto
area		area dell'impronta del plinto
Wink O	Wink V	coefficienti di Winkler (orizzontale e verticale) adottati
Comb		Combinazione di carico in cui si verificano i valori riportati
Pt (P1 P2 P3 P4)		valori di pressione nei vertici

La terza tabella è riferita alle fondazioni tipo platea su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni in ogni vertice (nodo) degli elementi costituenti la platea.

La quarta tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
105	PLINTO SUPERFICIALE
106	PLINTO SUPERFICIALE
107	PLINTO SUPERFICIALE
108	PLINTO SUPERFICIALE
109	PLINTO SUPERFICIALE
110	PLINTO SUPERFICIALE
111	PLINTO SUPERFICIALE
112	PLINTO SUPERFICIALE
113	PLINTO SUPERFICIALE
114	PLINTO SUPERFICIALE
115	PLINTO SUPERFICIALE
116	PLINTO SUPERFICIALE
117	PLINTO SUPERFICIALE
118	PLINTO SUPERFICIALE
119	PLINTO SUPERFICIALE
120	PLINTO SUPERFICIALE
121	PLINTO SUPERFICIALE
122	PLINTO SUPERFICIALE
123	PLINTO SUPERFICIALE
124	FONDAZIONE NASTRIFORME
125	CALCOLO DEI K DI WINKLER

Elem.	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2
27	1	-0.38	-0.38	-0.38	39	-0.24	-0.23	-0.24	71	-0.23	-0.22	-0.23
	79	-0.21	-0.21	-0.21	80	-0.28	-0.28	-0.28	87	-0.22	-0.22	-0.22
	90	-0.21	-0.21	-0.21								
...												
563	90	-0.27	-0.20	-0.27	80	-0.33	-0.24	-0.33	87	-0.28	-0.21	-0.28
Elem.		Pt ini	Pt fin	Pt max		Pt ini	Pt fin	Pt max		Pt ini	Pt fin	Pt max
		-0.66										
		-0.16										

RISULTATI ELEMENTI TIPO TRAVE

LEGENDA RISULTATI ELEMENTI TIPO TRAVE

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo trave, è possibile in relazione alle tabelle sotto riportate.

Gli elementi vengono suddivisi in relazione alle proprietà in elementi:

- tipo **pilastro**
- tipo **trave in elevazione**
- tipo **trave in fondazione**

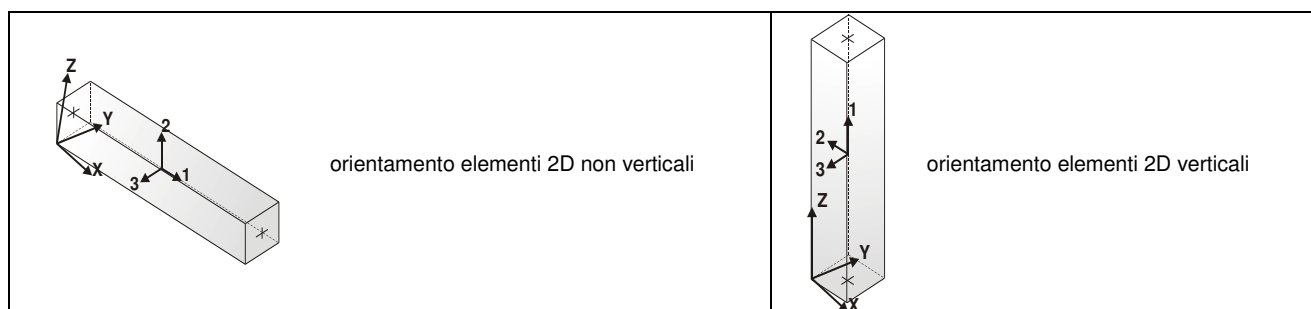
Per ogni elemento e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.

Per gli elementi tipo *pilastro* sono riportati in tabella i seguenti valori:

Pilas.	numero dell'elemento pilastro
Cmb	combinazione in cui si verificano i valori riportati
M3 mx/mn	momento flettente in campata M3 max (prima riga) / min (seconda riga)
M2 mx/mn	momento flettente in campata M2 max (prima riga) / min (seconda riga)
D2/D3	freccia massima in direzione 2 (prima riga) / direzione 3 (seconda riga)
Q2/Q3	carico totale in direzione 2 (prima riga) / direzione 3 (seconda riga)
Pos.	ascissa del punto iniziale e finale dell'elemento
N, V2, ecc..	sei componenti di sollecitazione al piede ed in sommità dell'elemento

Per gli elementi tipo *trave in elevazione* sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri.

Per gli elementi tipo *trave in fondazione* (trave f.) sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri e la massima pressione sul terreno.



Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN	cm	kN	kN	kN	kN m	kN m	kN m
9	1	0.0	0.0	2.09e-04	0.0	0.0	-25.60	0.0	0.0	3.57e-03	0.0	0.0
		0.0	0.0	-6.91e-04	0.0	20.0	-25.55	0.0	0.0	3.57e-03	0.0	0.0
						85.0	-25.40	0.0	0.0	3.57e-03	0.0	0.0
...												
527	90	0.0	0.0	-3.35e-04	0.0	340.0	-43.20	0.0	0.0	-2.03e-04	0.0	0.0
Pilas.		M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3		N	V 2	V 3	T		
		0.0	0.0	-0.02	0.0		-127.70	0.0	0.0	-0.40		
		0.0	0.0	0.02	0.0		-1.46	0.0	0.0	0.45		
Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN	cm	kN	kN	kN	kN m	kN m	kN m
1	1	17.12	0.0	0.02	-21.36	0.0	-1.77	10.68	0.0	-0.37	0.0	0.0
		0.0	0.0	3.02e-04	0.0	80.2	-1.26	8.01	0.0	-0.37	0.0	7.49
						160.3	-0.75	5.34	0.0	-0.37	0.0	12.84
...												
568	90	11.29	6.65e-03	-7.43e-06	0.0	54.0	-0.02	-3.66	-3.01e-03	0.0	6.65e-03	11.29
Trave		M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3		N	V 2	V 3	T		
		-68.65	-26.01	-0.03	-21.36		-59.19	-64.64	-19.47	-6.52		
		143.29	25.12	0.04	0.0		59.23	64.53	17.91	7.57		
Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN/ m2	cm	kN	kN	kN	kN m	kN m	kN m
27	1	5.02	0.38	-1.41e-05	-38.34	0.0	10.04	-5.65	-0.33	2.39	0.38	5.02
		3.76	0.18	2.45e-06		7.5	10.04	-4.70	-0.33	2.38	0.36	4.63
						15.0	10.04	-3.75	-0.33	2.38	0.33	4.31
...												
563	90	-1.41	-0.33	-8.30e-06	-26.53	275.0	0.06	0.03	0.22	-0.35	0.28	-1.41
Trave f.		M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt		N	V 2	V 3	T		
		-73.92	-41.08	-2.68e-03	-65.64		-53.51	-60.92	-25.28	-12.97		
		81.49	39.65	2.18e-03	-9.96		51.91	66.77	24.38	17.16		

VERIFICHE DI RESISTENZA AL FUOCO

Legenda tabella verifiche resistenza al fuoco per elementi in cemento armato

Le verifiche di resistenza al fuoco sono condotte in ottemperanza alla UNI EN 1992-1-2:2005 come previsto dal DM Infrastrutture 14 gennaio 2008.

Si precisa che:

- con riferimento alla figura 1. di UNI EN 1992-1-2:2005 "Procedure di progettazione" si è seguito il ramo "progettazione" > "regole prescrittive" > "analisi delle membrature" > calcolo delle azioni" > "modelli di calcolo semplificati" e "modelli di calcolo avanzati";
- l' incendio di progetto, assieme alle regole per l' analisi della temperatura, è previsto come nella sezione 3 di UNI EN-1991-1-2:2005
- i materiali sono definiti come nella sezione 3 di UNI EN 1992-1-2:2005 per quanto concerne proprietà meccaniche e fisiche in funzione della temperatura;
- parametri di riduzione della resistenza per i modelli di calcolo semplificati sono tratti dalla sezione 4 di UNI EN 1992-1-2:2005.

La verifica dello stato limite per sollecitazioni N,M2,M3 è condotta sia per i modelli semplificati che per i modelli avanzati con le usuali ipotesi di conservazione delle sezioni piane ed aderenza acciaio-cla. La verifica dello stato limite per la sollecitazione di taglio V si esplica nel controllo della minor sicurezza lato acciaio (taglio portato dall' armatura trasversale) e lato cla (verifica della biella compressa).

I modelli semplificati adottano:

- diagrammi tensioni deformazioni utilizzati a freddo opportunamente ridotti:

1. UNI EN 1992-1-1:2005 per il calcestruzzo prevede al punto 3.1.7. il diagramma parabola rettangolo o bilineare
2. UNI EN 1992-1-1:2005 per l' acciaio prevede al punto 3.2.7 e 3.3.6 diagrammi di tipo elastico perfettamente plastico senza limiti di deformazione o elastico incrudito con limite di deformazione.

- fattori di riduzione funzione della temperatura per i calcestruzzi silicei o calcarei;

- fattori di riduzione per gli acciai funzione del tipo e del comportamento limite della sezione (acciaio compresso e teso con deformazione inferiore al 2% e acciaio teso con deformazione superiore al 2%).

La modalità di verifica secondo il modello semplificato richiede pertanto gli usuali parametri e algoritmi in uso nelle verifiche a freddo.

I modelli avanzati utilizzano diagrammi tensioni deformazioni come da sezione 3 di UNI EN-1991-1-2:2005:

1. per il calcestruzzo si adotta un diagramma definito dai tre parametri funzione della temperatura resistenza massima, deformazione corrispondente alla resistenza massima, deformazione corrispondente alla tensione nulla (esiste pertanto un ramo discendente);
2. per l' acciaio si adotta un diagramma definito dai seguenti parametri tutti funzione della temperatura:
 - $E(t)$ modulo elastico
 - $f_p(t)$ tensione al limite proporzionale
 - $f_y(t)$ tensione massima
 - $\epsilon_p(t)$ deformazione per f_p
 - $\epsilon_y(t)$ deformazione iniziale per f_y (inizio tratto orizzontale)
 - $\epsilon_t(t)$ deformazione finale per f_y (fine tratto orizzontale)
 - $\epsilon_u(t)$ deformazione per tensione nulla (esiste pertanto un ramo discendente);

La modalità di verifica con il modello avanzato necessita di alcune precisazioni:

- il calcestruzzo al crescere della temperatura diminuisce la resistenza
- il calcestruzzo al crescere della temperatura diventa più duttile ossia aumenta la deformazione per cui attinge la massima resistenza e la deformazione in cui si annulla la resistenza
- si ammette pertanto che alcune fibre siano deformate in modo da cadere nel ramo discendente
- l' acciaio al crescere della temperatura diminuisce il modulo elastico, presenta una fascia non lineare (tra la proporzionale e la plastica) crescente, e in particolare nel precompresso varia $\epsilon_t(t)$ e $\epsilon_u(t)$.

La resistenza limite della sezione si ottiene pertanto iterando sulla curvatura ossia variando la deformazione massima del calcestruzzo e limitando quella dell' acciaio alla $\epsilon_t(t)$.

La modalità di analisi termica della sezione è identica nei due modelli. Per determinare la mappa termica si è effettuata una analisi del transitorio con elementi finiti bidimensionali utilizzando il codice "FIRES-T3: A Computer Program for the Fire Response of Structure-Thermal (Three-Dimensional Version)" di Iding, R.; Bresler, B.; Nizamuddin, Z. disponibile presso il "Building and Fire Research Laboratory National Institute of Standards and Technology Gaithersburg, MD 20899". Il software, opportunamente adattato per operare in ambiente grafico-interattivo assicura risultati coerenti con le mappe termiche delle norme UNI EN 1992-1-2:2005. Poiché l' analisi termica della sezione è effettuata indipendentemente dalla disposizione delle armature può essere adottata per tutte le verifiche allo stato limite ultimo.

Le tabelle sottoriportate, relative ad elementi trave e pilastro, guscio e setto riportano le verifiche condotte ed in particolare:

Trave / Pilas	Numero dell' elemento
Stato	Codice di verifica dell' elemento ok: verificato NV: non verificato
Note	Indice della sezione dell' elemento e valore del tempo di esposizione (in minuti)
%Res C	Indicatore della capacità residua per compressione (in percentuale).

Legenda tabella verifiche resistenza al fuoco per elementi in acciaio

Le verifiche per elementi monodimensionali in acciaio sono condotte in ottemperanza alla norma tecnica UNI EN 1993-1-2:2005 "Eurocodice 3 - Progettazione delle strutture in acciaio - Parte 1-2: Regole generali – Progettazione strutturale contro l'incendio".

In particolare con riferimento al capitolo

4 Structural fire design

si considerano i seguenti paragrafi :

4.2 Simple calculation models

4.2.1 General

Le verifiche saranno riportate in conformità alla formula (4.1) " $E_{f,d} < R_{f,d,t}$ " normalizzata a 1 ossia " $E_{f,d}/R_{f,d,t} < 1$ " ; valori maggiori di 1 indicheranno la non verifica.

Il programma segue il paragrafo (4.2) e pertanto determina le resistenze $R_{f,d,t}$ in conformità alla UNI EN 1993-1-1 nell' ipotesi di temperatura uniforme della sezione e modificando le proprietà meccaniche dell'acciaio per alte temperature. Viene lasciata all'utente la possibilità di considerare una distribuzione di temperatura non uniforme nella sezione per mezzo del fattore di adattamento k_1 . Non è considerata la variazione di temperatura nello sviluppo dell'elemento in quanto questo può essere modellato suddividendo lo stesso.

4.2.2 Classification of cross-sections

4.2.3 Resistance

Per effettuare le verifiche di resistenza e di stabilità flessionale e torsionale deve considerarsi sia la riduzione in funzione della temperatura sia della resistenza che del modulo elastico come da "Table 3.1: Reduction factors for stress-strain relationship of carbon steel at elevated temperatures".

Si considera un fattore di imperfezione α specifico e snellezze adimensionali corrette dalla radice del rapporto tra riduzione di resistenza e riduzione di modulo come da formula (4.7) e (4.15); nella formula (4.15) si considera a favore di sicurezza η .

4.2.5 Steel temperature development

L'analisi termica della sezione è condotta con riferimento al paragrafo 4.2.5; per i profili senza protezione si opera come da par. "4.2.5.1 Unprotected internal steelwork"; laddove previsto il programma consente di considerare l' effetto di rivestimenti di protezione e pertanto verrà applicato il par. "4.2.5.2 Internal steelwork insulated by fire protection material".

Le verifiche sono riassunte in tabella con la seguente modalità:

Elem.	Numero dell' elemento
Stato	Codice di verifica dell' elemento ok: verificato NV: non verificato
Note	Sezione e materiale
Min.	Tempo di esposizione per il quale si sono condotte le verifiche (minuti)
Prot.	Indicatore della protezione (si/no)
Temp.	Temperatura raggiunta al tempo di esposizione
Rid. fy	Fattore di riduzione della tensione di snervamento f_y come da Table 3.1: Reduction factors for stress-strain relationship of carbon steel at elevated temperatures
Rid. E	Fattore di riduzione del modulo elastico E come da Table 3.1: Reduction factors for stress-strain relationship of carbon steel at elevated temperatures
Cl.	Classe massima adottata nelle verifiche di interesse
V V/T	verifica di resistenza come da par. 4.2.3 per azioni taglio-torsione
V N/M	verifica di resistenza come da par. 4.2.3 per azioni composte con riduzione per taglio ove richiesto
V stab	verifica come da par. 4.2.3.5 (membrature inflesse e compresse senza/con presenza di instabilità flessione-torsionale)
V flst	verifica di stabilità flessotorsionale come da par. 4.2.3.3
Rif. cmb	combinazioni in cui si sono rispettivamente attinti i valori di verifica più elevati

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
103	VERIFICA AL FUOCO DI STRUTTURE IN LEGNO SECONDO EC5
104	ANALISI DI RESISTENZA AL FUOCO

VERIFICHE ELEMENTI TRAVE C.A.

LEGENDA TABELLA VERIFICHE ELEMENTI TRAVE C.A.

In tabella vengono riportati per ogni elemento il numero dello stesso ed il codice di verifica.

Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite vengono riportati il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L1 (paralleli alla base della sezione) e lungo i lati L2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

In particolare i simboli utilizzati con il metodo delle tensioni ammissibili assumono il seguente significato:

M P X Y	Numero della pilastrata e posizione in pianta
M T Z P P	Numero della travata, quota media pilastrata iniziale e finale (nodo in assenza di pilastrata)
Pilas. o Trave	numero identificativo dell'elemento
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m); nella terza riga viene riportato il valore delle snellezze in direzione 2-2 e 3-3
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Quota	Ascissa del punto di verifica
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
Armat. long.	Numero e diametro dei ferri di armatura longitudinale: ferri di vertice + ferri di lato (vedi seguente figura)
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup	Area di armatura longitudinale posta all'estradosso della trave
Sc max	Massima tensione di compressione del calcestruzzo
Sc med	Massima tensione media di compressione del calcestruzzo
Sf max	Tensione massima nell'acciaio
staffe	Vengono riportati i dati del tratto di staffatura in cui cade la sezione di verifica; in particolare: numero dei bracci, diametro, passo, lunghezza tratto
Tau max	Tensione massima tangenziale nel cls
Rif. comb	Combinazioni in cui si generano i seguenti valori di tensione: Sc max, Sc med, Sf max, Tau max
AfV	area dell'armatura atta ad assorbire le azioni di taglio
AfT	area dell'armatura atta ad assorbire le azioni di torsione
Scorr. P	Scorrimento dei piegati
Af long.	Area del ferro longitudinale aggiuntivo per assorbire la torsione

Progettazione delle fondazioni

Il D.M.14/02/2008 - par: 7.2.5 prevede:

"Per le strutture progettate sia per CD "A" sia per CD "B" il dimensionamento delle strutture di fondazione e la verifica di sicurezza del complesso fondazione-terreno devono essere eseguiti assumendo come azioni in fondazione le resistenze degli elementi strutturali soprastanti [...] si richiede tuttavia che tali azioni risultino non maggiori di quelle trasferite dagli elementi soprastanti, amplificate con un γ_{Rd} pari a 1,1 in CD "B" e 1,3 in CD "A" e comunque non maggiori di quelle derivanti da una analisi elastica della struttura in elevazione eseguita con un fattore di struttura q pari a 1...."

Nel contesto visualizzazione risultati e nella stampa della relazione sulle fondazioni PRO_SAP mostra le sollecitazioni che derivano dall'analisi non incrementate sia in termini di pressioni sul terreno che in termini di sollecitazioni.

La progettazione degli elementi strutturali con proprietà fondazione è effettuata da PRO_SAP (per travi e platee) o da PRO_CAD Plinti (per plinti e pali di fondazione) incrementando le sollecitazioni delle combinazioni con sisma del fattore: $\gamma_{rd} = 1.1$ in CDB $\gamma_{rd} = 1.3$ in CDA per pali, plinti, travi e platee.

Per i bicchieri dei plinti di fondazione prefabbricati l'incremento delle sollecitazioni ha un fattore: $\gamma_{rd} = 1.2$ in CDB $\gamma_{rd} = 1.35$ in CDA.

N.B.: se il fattore di struttura q è ≥ 1 la progettazione viene effettuata senza nessun incremento.

Le verifiche geotecniche vengono effettuate dal modulo geotecnico incrementando automaticamente le sollecitazioni del fattore: $\gamma_{rd} = 1.1$ in CDB $\gamma_{rd} = 1.3$ in CDA per pali, plinti, travi e platee.

N.B.: se il fattore di struttura q è ≥ 1 le verifiche geotecniche vengono effettuate senza nessun incremento.

Mentre i simboli utilizzati con il metodo degli stati limite assumono il seguente significato:

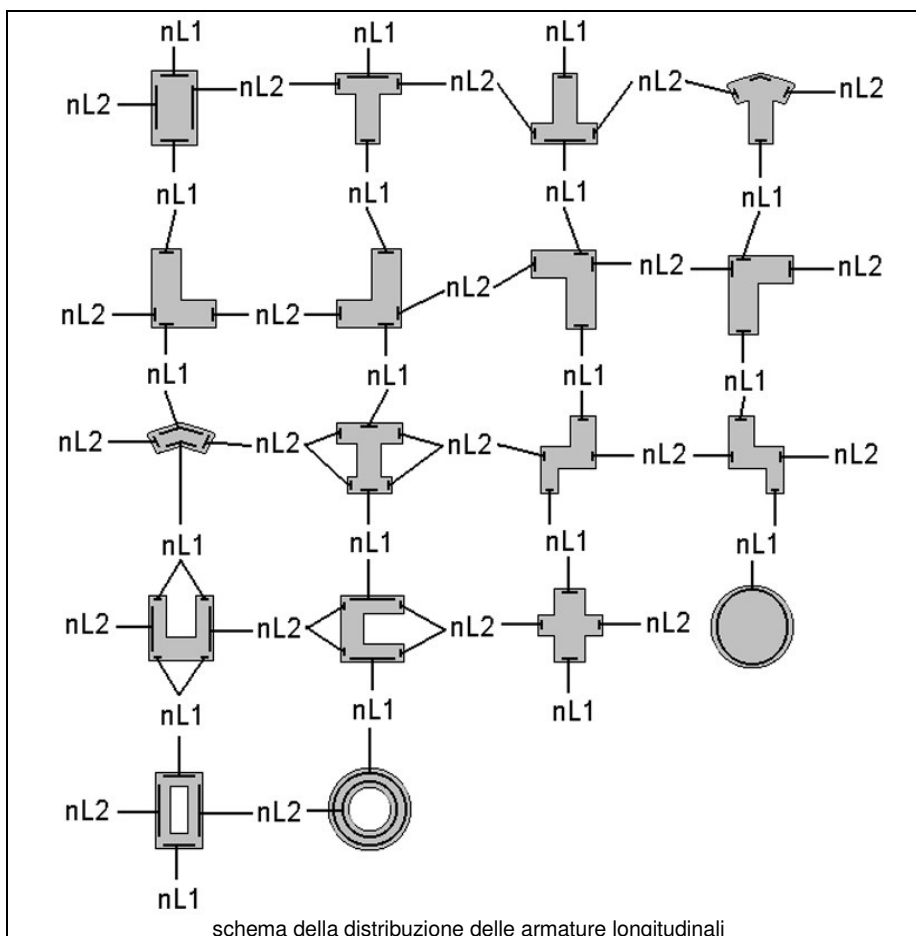
Mentre i simboli utilizzati con il metodo degli stati limite assumono il seguente significato:	
r. snell.	Rapporto λ su λ^* : valore superiore a 1 per elementi snelli, caso in cui viene effettuata la verifica con il metodo diretto dello stato di equilibrio
Verifica(verif.)	rapporto S_d/S_u con sollecitazioni ultime proporzionali o a sforzo normale costante: valore minore o uguale a 1 per verifica positiva
ver.sis	rapporto N_d/N_u con N_u calcolato come al punto 7.4.4.2.2.1; valore minore o uguale a 1 per verifica positiva
ver.V/T	rapporto S_d/S_u con sollecitazioni taglianti e torcenti proporzionali valore minore o uguale a 1 per verifica positiva
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)

Per gli elementi progettati secondo il criterio della gerarchia delle resistenze (pilastri e travi) si riporta una ulteriore tabella di seguito descritta:

M negativo i	Valore del momento resistente negativo (positivo) all' estremità iniziale i (finale f) della trave
V M-i M+f	Taglio generato dai momenti resistenti negativo i e positivo f (positivo i e negativo f)
V totale	Massimo valore assoluto ottenuto per combinazione del taglio isostatico e dei tagli concomitanti (p.to 7.4.4.1.1.)
Verif. V	Rapporto tra il taglio massimo e V_{r1} (p.to 7.4.4.1.2.2);
Sovr. 2-2 i	Sovraresistenza del pilastro (come da formula 7.4.4). Rapporto tra i momenti resistenti delle travi e dei pilastri. Il valore del fattore rispettivamente per il momento 2-2 (3-3) alla base i ed alla sommità f del pilastro deve essere maggiore del γ_{Rd} adottato
M 2-2 i	Valore del momento resistente rispettivamente per 2-2 (3-3) alla base i ed alla sommità f del pilastro (massimo momento in presenza dello sforzo normale di calcolo)
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M2-2	Valore del taglio generato dai momenti resistenti 2-2 (3-3)

Per i nodi trave-pilastro viene riportata la seguente tabella relativa al calcolo delle armature di confinamento e alla verifica di resistenza del nodo (richiesta solo per strutture in classe di duttilità alta); le caselle vuote indicano parametri non riportati in quanto non necessari.

Stato	Esito della verifica (come da formula 7.4.8) per resistenza a compressione del nodo (solo CDA)
I 7.4.29	Passo delle staffe di confinamento come richiesto dalla formula 7.4.29
Bj2(3)	Dimensione del nodo per il taglio in direzione 2 (3)
Hjc2(2)	Distanza tra le giaciture di armatura del pilastro per il taglio in direzione 2 (3)
V. 7.4.8	Rapporto tra il taglio V_{jbd} e il taglio resistente come da formula 7.4.8 (solo CDA)
I 7.4.10	Passo delle staffe valutato in funzione della formula 7.4.10 (solo CDA)



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Test N°	Titolo
24	TENSIONI E ROTAZIONI RISPETTO ALLA CORDA DI ELEMENTI TRAVE
27	FRECCIA DI ELEMENTI TRAVE
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE TA DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
68	VALUTAZIONE EFFETTO P-δ SU PILASTRATA
69	VALUTAZIONE EFFETTO P-δ SU TELAIO 3D
120	PROGETTO E VERIFICA DI TRAVI PREM

Trave	Note	Pos. cm	%Af	Af inf.	Af. sup	Af long.	M_T= 26 x/d	Z=0.0 V N/M	P=1 V V/T cls	P=4 V V/T acc	Staffe L=cm	Rif. cmb
123	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.15	0.04	2d8/10 L=95	43,5,42
		11.9	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.03	2d8/10 L=95	43,5,42
		23.8	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.03	2d8/10 L=95	43,5,42
		35.6	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.03	2d8/10 L=95	46,5,42
		47.5	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=95	46,5,42
		59.4	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=95	46,5,42
		71.3	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=95	46,5,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.03	2d8/10 L=95	46,5,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.04	2d8/10 L=95	46,5,43
86	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.02	2d8/10 L=95	46,5,46
		11.9	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01	2d8/10 L=95	42,5,46
		23.8	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01	2d8/10 L=95	42,5,46
		35.6	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01	2d8/10 L=95	42,5,39
		47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.02	2d8/10 L=95	42,5,39
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=95	42,5,39
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.02	2d8/10 L=95	39,5,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.02	2d8/10 L=95	39,5,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.03	2d8/10 L=95	1,5,39
69	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.13	2.13e-03	2d8/10 L=53	1,5,22
		6.6	0.38	7.7	7.7	0.0	0.13	0.02	0.13	3.97e-03	2d8/10 L=53	1,5,1
		13.3	0.38	7.7	7.7	0.0	0.13	0.02	0.13	6.62e-03	2d8/10 L=53	1,5,1
		19.9	0.38	7.7	7.7	0.0	0.13	0.02	0.13	9.26e-03	2d8/10 L=53	1,5,1
		26.5	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.01	2d8/10 L=53	1,5,1
		33.1	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.01	2d8/10 L=53	1,5,1
		39.8	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02	2d8/10 L=53	1,5,1
		46.4	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02	2d8/10 L=53	1,5,1
		53.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02	2d8/10 L=53	1,5,1
50	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	1.43e-03	2d8/10 L=42	1,5,1
		5.3	0.38	7.7	7.7	0.0	0.13	0.04	0.13	3.54e-03	2d8/10 L=42	1,5,1
		10.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	5.65e-03	2d8/10 L=42	1,5,1
		15.8	0.38	7.7	7.7	0.0	0.13	0.04	0.14	7.76e-03	2d8/10 L=42	1,5,1
		21.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	9.87e-03	2d8/10 L=42	1,5,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=42	1,5,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=42	1,5,1
		36.8	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=42	1,5,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=42	1,5,1
78	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	5.00e-03	2d8/10 L=35	1,5,1
		4.4	0.38	7.7	7.7	0.0	0.13	0.05	0.13	3.24e-03	2d8/10 L=35	1,5,1
		8.8	0.38	7.7	7.7	0.0	0.13	0.05	0.13	2.09e-03	2d8/10 L=35	1,5,42

		13.1	0.38	7.7	7.7	0.0	0.13	0.05	0.13	1.10e-03	2d8/10 L=35	1,5,42
		17.5	0.38	7.7	7.7	0.0	0.13	0.05	0.13	2.04e-03	2d8/10 L=35	1,5,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.05	0.13	3.80e-03	2d8/10 L=35	1,5,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.13	5.57e-03	2d8/10 L=35	1,5,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.05	0.13	7.33e-03	2d8/10 L=35	1,5,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	9.09e-03	2d8/10 L=35	1,5,1
27	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=60	1,5,1
	s=7,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.01	2d8/10 L=60	1,5,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01	2d8/10 L=60	1,5,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	8.93e-03	2d8/10 L=60	1,5,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	5.91e-03	2d8/10 L=60	1,5,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	2.90e-03	2d8/10 L=60	1,5,1
		45.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	8.89e-04	2d8/10 L=60	1,5,19
		52.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	3.12e-03	2d8/10 L=60	1,5,1
		60.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	6.12e-03	2d8/10 L=60	1,5,1
102	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.03	2d8/10 L=95	1,5,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=95	1,5,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=95	1,5,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.01	2d8/10 L=95	1,5,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.10	8.90e-03	2d8/10 L=95	1,5,1
		59.4	0.38	7.7	7.7	0.0	0.13	9.19e-03	0.10	4.19e-03	2d8/10 L=95	1,5,1
		71.3	0.38	7.7	7.7	0.0	0.13	8.62e-03	0.10	2.10e-03	2d8/10 L=95	19,5,19
		83.1	0.38	7.7	7.7	0.0	0.13	9.57e-03	0.10	5.20e-03	2d8/10 L=95	1,5,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.10	9.88e-03	2d8/10 L=95	1,5,1
87	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=18	1,5,1
	s=7,m=3	2.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=18	1,5,1
		4.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=18	1,5,1
		6.8	0.38	7.7	7.7	0.0	0.13	0.01	0.07	9.57e-03	2d8/10 L=18	1,5,1
		9.0	0.38	7.7	7.7	0.0	0.13	9.36e-03	0.07	8.69e-03	2d8/10 L=18	1,5,1
		11.3	0.38	7.7	7.7	0.0	0.13	8.78e-03	0.07	7.81e-03	2d8/10 L=18	1,5,1
		13.5	0.38	7.7	7.7	0.0	0.13	8.40e-03	0.06	6.92e-03	2d8/10 L=18	19,5,1
		15.8	0.38	7.7	7.7	0.0	0.13	8.20e-03	0.06	6.04e-03	2d8/10 L=18	19,5,1
		18.0	0.38	7.7	7.7	0.0	0.13	8.04e-03	0.06	5.16e-03	2d8/10 L=18	19,5,1
70	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	8.01e-03	0.06	0.02	2d8/10 L=77	19,5,1
	s=7,m=3	9.6	0.38	7.7	7.7	0.0	0.13	5.46e-03	0.06	0.02	2d8/10 L=77	19,5,1
		19.3	0.38	7.7	7.7	0.0	0.13	4.55e-03	0.06	0.01	2d8/10 L=77	22,5,1
		28.9	0.38	7.7	7.7	0.0	0.13	6.91e-03	0.06	0.01	2d8/10 L=77	1,5,1
		38.5	0.38	7.7	7.7	0.0	0.13	9.41e-03	0.05	6.43e-03	2d8/10 L=77	1,5,1
		48.1	0.38	7.7	7.7	0.0	0.13	0.01	0.05	2.69e-03	2d8/10 L=77	1,5,1
		57.8	0.38	7.7	7.7	0.0	0.13	0.01	0.05	2.25e-03	2d8/10 L=77	1,5,39
		67.4	0.38	7.7	7.7	0.0	0.13	0.01	0.05	4.76e-03	2d8/10 L=77	1,5,1
		77.0	0.38	7.7	7.7	0.0	0.13	8.17e-03	0.06	8.47e-03	2d8/10 L=77	1,5,1
121	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	8.15e-03	0.05	0.02	2d8/10 L=95	1,9,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.01	0.05	0.01	2d8/10 L=95	1,9,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.05	8.59e-03	2d8/10 L=95	1,9,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.05	4.04e-03	2d8/10 L=95	1,9,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.04	1.10e-03	2d8/10 L=95	1,9,39
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.05	5.04e-03	2d8/10 L=95	1,9,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.05	9.56e-03	2d8/10 L=95	1,9,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.05	0.01	2d8/10 L=95	1,9,1
		95.0	0.38	7.7	7.7	0.0	0.13	6.72e-03	0.05	0.02	2d8/10 L=95	1,9,1
107	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	6.72e-03	0.08	7.91e-03	2d8/10 L=78	1,9,1
	s=7,m=3	9.8	0.38	7.7	7.7	0.0	0.13	8.56e-03	0.07	4.21e-03	2d8/10 L=78	1,9,1
		19.5	0.38	7.7	7.7	0.0	0.13	9.28e-03	0.07	9.51e-04	2d8/10 L=78	1,6,42
		29.3	0.38	7.7	7.7	0.0	0.13	8.88e-03	0.07	3.17e-03	2d8/10 L=78	1,9,1
		39.0	0.38	7.7	7.7	0.0	0.13	7.36e-03	0.08	6.85e-03	2d8/10 L=78	1,9,1
		48.8	0.38	7.7	7.7	0.0	0.13	4.71e-03	0.08	0.01	2d8/10 L=78	1,9,1
		58.5	0.38	7.7	7.7	0.0	0.13	4.61e-03	0.08	0.01	2d8/10 L=78	27,9,1
		68.3	0.38	7.7	7.7	0.0	0.13	7.07e-03	0.08	0.02	2d8/10 L=78	5,9,1
		78.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.02	2d8/10 L=78	5,9,1
93	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	4.69e-03	2d8/10 L=17	5,6,19
	s=7,m=3	2.1	0.38	7.7	7.7	0.0	0.13	0.01	0.10	5.20e-03	2d8/10 L=17	5,6,19
		4.3	0.38	7.7	7.7	0.0	0.13	0.01	0.10	5.71e-03	2d8/10 L=17	5,6,19
		6.4	0.38	7.7	7.7	0.0	0.13	0.01	0.10	6.21e-03	2d8/10 L=17	5,6,19
		8.5	0.38	7.7	7.7	0.0	0.13	0.01	0.10	6.72e-03	2d8/10 L=17	5,6,19
		10.6	0.38	7.7	7.7	0.0	0.13	0.01	0.10	7.23e-03	2d8/10 L=17	5,6,19
		12.8	0.38	7.7	7.7	0.0	0.13	0.01	0.10	7.73e-03	2d8/10 L=17	5,6,19
		14.9	0.38	7.7	7.7	0.0	0.13	0.01	0.10	8.39e-03	2d8/10 L=17	5,6,1
		17.0	0.38	7.7	7.7	0.0	0.13	0.01	0.10	9.19e-03	2d8/10 L=17	5,6,1
155	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.15	0.01	2d8/10 L=95	5,6,42
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.01	0.15	0.01	2d8/10 L=95	19,6,42
		23.8	0.38	7.7	7.7	0.0	0.13	0.01	0.14	8.41e-03	2d8/10 L=95	19,6,22
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.14	8.28e-03	2d8/10 L=95	19,6,19
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.01	2d8/10 L=95	19,6,19
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.01	2d8/10 L=95	19,6,19
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=95	19,6,19

		83.1	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=95	19,6,19
		95.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=95	19,6,1
143	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.03	2d8/10 L=95	19,6,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=95	19,6,5
		23.8	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=95	19,6,5
		35.6	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=95	19,6,5
		47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.01	2d8/10 L=95	19,6,5
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.01	2d8/10 L=95	22,6,22
		71.3	0.38	7.7	7.7	0.0	0.13	0.04	0.17	9.70e-03	2d8/10 L=95	22,6,22
		83.1	0.38	7.7	7.7	0.0	0.13	0.04	0.17	8.80e-03	2d8/10 L=95	22,6,19
		95.0	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.01	2d8/10 L=95	22,6,19
122	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.17	0.05	0.03	2d8/10 L=17	39,27,1
	s=7,m=3	2.1	0.38	7.7	7.7	0.0	0.13	0.17	0.05	0.03	2d8/10 L=17	39,27,1
		4.3	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=17	39,27,1
		6.4	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=17	39,27,1
		8.5	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=17	39,27,1
		10.6	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=17	39,27,1
		12.8	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=17	39,27,1
		14.9	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=17	39,27,1
		17.0	0.38	7.7	7.7	0.0	0.13	0.15	0.05	0.03	2d8/10 L=17	39,27,1
110	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.06	0.05	2d8/10 L=169	39,30,42
	s=7,m=3	21.1	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.04	2d8/10 L=169	39,30,42
		42.3	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.04	2d8/10 L=169	39,30,42
		63.4	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.03	2d8/10 L=169	42,27,42
		84.5	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.03	2d8/10 L=169	42,27,42
		105.6	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=169	42,27,42
		126.8	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.02	2d8/10 L=169	42,27,39
		147.9	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=169	42,27,39
		169.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=169	42,27,39
144	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=146	42,27,42
	s=7,m=3	18.3	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=146	46,27,42
		36.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=146	30,27,39
		54.8	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=146	26,27,39
		73.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=146	26,27,39
		91.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.03	2d8/10 L=146	27,27,39
		109.5	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=146	27,27,1
		127.8	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.04	2d8/10 L=146	43,27,1
		146.0	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.05	2d8/10 L=146	43,27,1
127	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.04	2d8/10 L=151	43,28,42
	s=7,m=3	18.9	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.03	2d8/10 L=151	43,28,42
		37.8	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.03	2d8/10 L=151	43,28,42
		56.6	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.03	2d8/10 L=151	43,28,42
		75.5	0.38	7.7	7.7	0.0	0.13	0.08	0.04	0.02	2d8/10 L=151	39,27,42
		94.4	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.02	2d8/10 L=151	42,27,42
		113.3	0.38	7.7	7.7	0.0	0.13	0.10	0.04	0.02	2d8/10 L=151	42,27,39
		132.1	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.02	2d8/10 L=151	42,27,39
		151.0	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.02	2d8/10 L=151	39,27,39
52	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.04	3.23e-03	2d8/10 L=53	39,27,43
	s=7,m=3	6.7	0.38	7.7	7.7	0.0	0.13	0.05	0.04	4.57e-03	2d8/10 L=53	39,27,43
		13.3	0.38	7.7	7.7	0.0	0.13	0.05	0.04	5.92e-03	2d8/10 L=53	39,27,43
		20.0	0.38	7.7	7.7	0.0	0.13	0.05	0.04	7.37e-03	2d8/10 L=53	39,27,1
		26.7	0.38	7.7	7.7	0.0	0.13	0.05	0.04	9.56e-03	2d8/10 L=53	39,27,1
		33.3	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.01	2d8/10 L=53	39,27,1
		40.0	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.01	2d8/10 L=53	39,27,1
		46.7	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=53	39,27,1
		53.3	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=53	39,27,1
79	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=39	39,19,42
	s=7,m=3	4.8	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=39	39,19,42
		9.7	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.01	2d8/10 L=39	39,19,42
		14.5	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=39	39,19,39
		19.3	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.02	2d8/10 L=39	39,19,39
		24.2	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.02	2d8/10 L=39	39,19,39
		29.0	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.02	2d8/10 L=39	39,19,39
		33.8	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=39	39,19,39
		38.7	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=39	39,19,39
95	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.03	0.02	2d8/10 L=68	39,24,42
	s=7,m=3	8.5	0.38	7.7	7.7	0.0	0.13	0.04	0.03	0.02	2d8/10 L=68	39,24,42
		17.0	0.38	7.7	7.7	0.0	0.13	0.04	0.03	0.01	2d8/10 L=68	43,19,42
		25.5	0.38	7.7	7.7	0.0	0.13	0.04	0.03	0.01	2d8/10 L=68	43,19,42
		34.0	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.01	2d8/10 L=68	43,19,42
		42.5	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.01	2d8/10 L=68	43,19,39
		51.0	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.01	2d8/10 L=68	43,19,39
		59.5	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.01	2d8/10 L=68	43,19,39
		68.0	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.02	2d8/10 L=68	43,19,39
111	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.03	8.75e-03	2d8/10 L=69	43,5,1
	s=7,m=3	8.6	0.38	7.7	7.7	0.0	0.13	0.02	0.03	6.25e-03	2d8/10 L=69	43,5,42

		17.3	0.38	7.7	7.7	0.0	0.13	0.02	0.03	4.76e-03	2d8/10 L=69	43,5,42
		25.9	0.38	7.7	7.7	0.0	0.13	0.02	0.03	3.33e-03	2d8/10 L=69	43,5,46
		34.5	0.38	7.7	7.7	0.0	0.13	0.02	0.03	4.17e-03	2d8/10 L=69	43,27,43
		43.1	0.38	7.7	7.7	0.0	0.13	0.02	0.03	5.93e-03	2d8/10 L=69	43,27,43
		51.8	0.38	7.7	7.7	0.0	0.13	0.02	0.03	7.71e-03	2d8/10 L=69	43,27,27
		60.4	0.38	7.7	7.7	0.0	0.13	0.03	0.04	9.75e-03	2d8/10 L=69	43,27,27
		69.0	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.01	2d8/10 L=69	43,27,1
131	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.01	2d8/10 L=69	43,5,43
	s=7,m=3	8.6	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.02	2d8/10 L=69	43,5,43
		17.3	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.02	2d8/10 L=69	43,5,43
		25.9	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=69	39,5,43
		34.5	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=69	43,5,43
		43.1	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=69	43,5,43
		51.8	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.02	2d8/10 L=69	43,5,43
		60.4	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.03	2d8/10 L=69	43,5,43
		69.0	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.03	2d8/10 L=69	43,5,43
148	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.03	2d8/10 L=69	43,5,43
	s=7,m=3	8.6	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.03	2d8/10 L=69	43,5,43
		17.3	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.04	2d8/10 L=69	43,5,43
		25.9	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.04	2d8/10 L=69	43,5,43
		34.5	0.38	7.7	7.7	0.0	0.13	0.11	0.06	0.04	2d8/10 L=69	43,5,43
		43.1	0.38	7.7	7.7	0.0	0.13	0.12	0.06	0.04	2d8/10 L=69	43,5,43
		51.8	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.04	2d8/10 L=69	43,5,43
		60.4	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.04	2d8/10 L=69	43,5,43
		69.0	0.38	7.7	7.7	0.0	0.13	0.15	0.06	0.04	2d8/10 L=69	43,5,43
M_T= 39 Z=0.0 N=405 N=1663												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
325	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.20	0.03	2d8/10 L=236	6,39,5
	s=7,m=3	29.5	0.38	7.7	7.7	0.0	0.13	0.10	0.20	0.02	2d8/10 L=236	9,39,5
		59.0	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.02	2d8/10 L=236	9,39,6
		88.5	0.38	7.7	7.7	0.0	0.13	0.08	0.21	0.02	2d8/10 L=236	9,39,19
		118.0	0.38	7.7	7.7	0.0	0.13	0.06	0.21	0.03	2d8/10 L=236	9,39,19
		147.5	0.38	7.7	7.7	0.0	0.13	0.03	0.22	0.04	2d8/10 L=236	30,39,9
		177.0	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.05	2d8/10 L=236	5,39,1
		206.5	0.38	7.7	7.7	0.0	0.13	0.09	0.23	0.06	2d8/10 L=236	15,39,1
		236.0	0.38	7.7	7.7	0.0	0.13	0.14	0.23	0.07	2d8/10 L=236	1,39,1
518	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.01	2d8/10 L=104	1,39,5
	s=7,m=3	13.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	6.66e-03	2d8/10 L=104	1,39,5
		26.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	5.21e-03	2d8/10 L=104	1,39,43
		39.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.01	2d8/10 L=104	1,39,9
		52.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=104	1,39,1
		65.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.02	2d8/10 L=104	1,39,1
		78.0	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.03	2d8/10 L=104	1,39,1
		91.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.03	2d8/10 L=104	1,39,1
		104.0	0.38	7.7	7.7	0.0	0.13	0.10	0.15	0.04	2d8/10 L=104	1,39,1
512	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.04	2d8/10 L=72	1,43,1
	s=7,m=3	9.0	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.03	2d8/10 L=72	1,43,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.08	0.16	0.03	2d8/10 L=72	1,43,1
		27.0	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=72	1,43,1
		36.0	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=72	1,43,1
		45.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.01	2d8/10 L=72	1,39,1
		54.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.01	2d8/10 L=72	1,39,42
		63.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	7.87e-03	2d8/10 L=72	1,39,42
		72.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	5.93e-03	2d8/10 L=72	1,39,39
76	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.01	2d8/10 L=31	19,42,39
	s=7,m=3	3.9	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.01	2d8/10 L=31	19,42,39
		7.8	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.01	2d8/10 L=31	19,42,19
		11.6	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.01	2d8/10 L=31	19,42,19
		15.5	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.02	2d8/10 L=31	19,42,19
		19.4	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.02	2d8/10 L=31	19,42,19
		23.3	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.02	2d8/10 L=31	19,42,19
		27.1	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.02	2d8/10 L=31	19,42,19
		31.0	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.02	2d8/10 L=31	19,42,19
500	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=67	19,42,1
	s=7,m=3	8.4	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.01	2d8/10 L=67	19,42,1
		16.8	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=67	19,42,22
		25.1	0.38	7.7	7.7	0.0	0.13	0.03	0.16	8.89e-03	2d8/10 L=67	19,42,22
		33.5	0.38	7.7	7.7	0.0	0.13	0.03	0.16	6.94e-03	2d8/10 L=67	1,42,22
		41.9	0.38	7.7	7.7	0.0	0.13	0.03	0.16	9.27e-03	2d8/10 L=67	1,42,19
		50.3	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=67	1,42,19
		58.6	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.01	2d8/10 L=67	1,42,19
		67.0	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=67	1,42,19
484	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.02	2d8/10 L=85	1,1,1
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=85	1,1,1
		21.3	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.01	2d8/10 L=85	1,1,1
		31.9	0.38	7.7	7.7	0.0	0.13	0.03	0.08	5.72e-03	2d8/10 L=85	1,34,1

		42.5	0.38	7.7	7.7	0.0	0.13	0.02	0.07	1.61e-03	2d8/10 L=85	1,34,22
		53.1	0.38	7.7	7.7	0.0	0.13	0.03	0.07	5.13e-03	2d8/10 L=85	1,34,1
		63.8	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.01	2d8/10 L=85	1,1,1
		74.4	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=85	1,1,1
		85.0	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.02	2d8/10 L=85	1,1,1
462	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=35	1,42,1
	s=7,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=35	1,42,1
		8.8	0.38	7.7	7.7	0.0	0.13	0.04	0.14	9.44e-03	2d8/10 L=35	1,42,1
		13.1	0.38	7.7	7.7	0.0	0.13	0.03	0.14	7.20e-03	2d8/10 L=35	1,42,1
		17.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	4.95e-03	2d8/10 L=35	1,42,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.03	0.13	2.70e-03	2d8/10 L=35	1,42,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.03	0.13	1.20e-03	2d8/10 L=35	1,42,19
		30.6	0.38	7.7	7.7	0.0	0.13	0.03	0.13	2.49e-03	2d8/10 L=35	1,42,19
		35.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	4.04e-03	2d8/10 L=35	1,42,1
493	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=50	1,42,1
	s=7,m=3	6.3	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=50	1,42,1
		12.5	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=50	1,42,1
		18.8	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=50	1,42,1
		25.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	8.20e-03	2d8/10 L=50	1,42,1
		31.3	0.38	7.7	7.7	0.0	0.13	0.02	0.16	4.99e-03	2d8/10 L=50	1,42,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.02	0.16	1.83e-03	2d8/10 L=50	1,42,22
		43.8	0.38	7.7	7.7	0.0	0.13	0.02	0.16	3.28e-03	2d8/10 L=50	1,42,19
		50.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	5.20e-03	2d8/10 L=50	1,42,19
439	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.22	0.03	2d8/10 L=85	1,42,1
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.01	0.21	0.02	2d8/10 L=85	1,42,1
		21.3	0.38	7.7	7.7	0.0	0.13	5.64e-03	0.21	0.02	2d8/10 L=85	27,42,1
		31.9	0.38	7.7	7.7	0.0	0.13	4.67e-03	0.21	0.01	2d8/10 L=85	27,42,1
		42.5	0.38	7.7	7.7	0.0	0.13	4.92e-03	0.21	6.89e-03	2d8/10 L=85	27,42,30
		53.1	0.38	7.7	7.7	0.0	0.13	6.51e-03	0.21	5.92e-03	2d8/10 L=85	30,42,23
		63.8	0.38	7.7	7.7	0.0	0.13	8.83e-03	0.21	9.18e-03	2d8/10 L=85	27,42,23
		74.4	0.38	7.7	7.7	0.0	0.13	0.01	0.21	0.01	2d8/10 L=85	27,42,23
		85.0	0.38	7.7	7.7	0.0	0.13	0.02	0.21	0.02	2d8/10 L=85	27,42,1
531	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.02	2d8/10 L=35	27,42,30
	s=7,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.02	2d8/10 L=35	27,42,30
		8.8	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.02	2d8/10 L=35	27,42,30
		13.1	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.01	2d8/10 L=35	27,42,30
		17.5	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.01	2d8/10 L=35	27,42,30
		21.9	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.01	2d8/10 L=35	27,42,26
		26.3	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.01	2d8/10 L=35	27,42,23
		30.6	0.38	7.7	7.7	0.0	0.13	0.03	0.24	0.01	2d8/10 L=35	27,42,23
		35.0	0.38	7.7	7.7	0.0	0.13	0.03	0.24	0.01	2d8/10 L=35	27,42,23
532	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.25	0.03	2d8/10 L=50	27,42,30
	s=7,m=3	6.3	0.38	7.7	7.7	0.0	0.13	0.03	0.25	0.03	2d8/10 L=50	27,42,30
		12.5	0.38	7.7	7.7	0.0	0.13	0.03	0.25	0.02	2d8/10 L=50	30,42,30
		18.8	0.38	7.7	7.7	0.0	0.13	0.04	0.25	0.02	2d8/10 L=50	30,42,30
		25.0	0.38	7.7	7.7	0.0	0.13	0.04	0.25	0.02	2d8/10 L=50	30,42,30
		31.3	0.38	7.7	7.7	0.0	0.13	0.04	0.25	0.02	2d8/10 L=50	30,42,26
		37.5	0.38	7.7	7.7	0.0	0.13	0.05	0.25	0.02	2d8/10 L=50	30,42,26
		43.8	0.38	7.7	7.7	0.0	0.13	0.05	0.25	0.02	2d8/10 L=50	30,42,23
		50.0	0.38	7.7	7.7	0.0	0.13	0.05	0.24	0.02	2d8/10 L=50	30,42,23
449	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.02	2d8/10 L=103	30,42,30
	s=7,m=3	12.9	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=103	30,42,30
		25.8	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=103	30,39,27
		38.6	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.02	2d8/10 L=103	30,39,27
		51.5	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=103	26,39,27
		64.4	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.03	2d8/10 L=103	26,39,27
		77.3	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.03	2d8/10 L=103	26,39,1
		90.1	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.04	2d8/10 L=103	26,39,1
		103.0	0.38	7.7	7.7	0.0	0.13	0.01	0.17	0.04	2d8/10 L=103	27,39,1
504	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.12	0.01	2d8/10 L=104	27,42,1
	s=7,m=3	13.0	0.38	7.7	7.7	0.0	0.13	8.59e-03	0.11	6.28e-03	2d8/10 L=104	23,42,1
		26.0	0.38	7.7	7.7	0.0	0.13	7.22e-03	0.11	1.85e-03	2d8/10 L=104	23,39,26
		39.0	0.38	7.7	7.7	0.0	0.13	7.09e-03	0.11	7.33e-03	2d8/10 L=104	23,39,1
		52.0	0.38	7.7	7.7	0.0	0.13	8.21e-03	0.12	0.01	2d8/10 L=104	27,39,1
		65.0	0.38	7.7	7.7	0.0	0.13	0.01	0.12	0.02	2d8/10 L=104	1,39,1
		78.0	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.03	2d8/10 L=104	1,39,1
		91.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.03	2d8/10 L=104	1,39,1
		104.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.04	2d8/10 L=104	1,39,1
533	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.07	8.49e-03	2d8/10 L=66	1,42,22
	s=7,m=3	8.3	0.38	7.7	7.7	0.0	0.13	0.05	0.07	6.02e-03	2d8/10 L=66	1,39,22
		16.5	0.38	7.7	7.7	0.0	0.13	0.05	0.07	7.20e-03	2d8/10 L=66	1,39,19
		24.8	0.38	7.7	7.7	0.0	0.13	0.05	0.07	9.31e-03	2d8/10 L=66	1,39,19
		33.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.01	2d8/10 L=66	1,39,1
		41.3	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=66	1,39,1
		49.5	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.02	2d8/10 L=66	1,39,1
		57.8	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.03	2d8/10 L=66	1,39,1

534	ok,ok s=7,m=3	66.0	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.03	2d8/10 L=66	1,39,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=27	1,18,18
		3.4	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,18,18
		6.8	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,18,18
		10.1	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,18,18
		13.5	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,15,18
		16.9	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,15,15
		20.3	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,15,15
		23.6	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,15,15
		27.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.01	2d8/10 L=27	1,15,15
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.05	2d8/10 L=95	1,30,1
		11.9	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.04	2d8/10 L=95	1,30,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.03	2d8/10 L=95	1,30,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.03	2d8/10 L=95	1,30,1
520	ok,ok s=7,m=3	47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=95	15,30,1
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=95	15,27,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.05	9.35e-03	2d8/10 L=95	15,27,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.02	0.04	3.13e-03	2d8/10 L=95	15,27,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.05	3.85e-03	2d8/10 L=95	15,27,15
		0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.12	0.07	2d8/10 L=210	15,46,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.06	2d8/10 L=210	18,46,18
522	ok,ok s=7,m=3	52.5	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.05	2d8/10 L=210	18,46,18
		78.8	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.04	2d8/10 L=210	1,46,18
		105.0	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.04	2d8/10 L=210	1,46,18
		131.3	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.03	2d8/10 L=210	1,39,15
		157.5	0.38	7.7	7.7	0.0	0.13	0.10	0.11	0.04	2d8/10 L=210	18,39,15
		183.8	0.38	7.7	7.7	0.0	0.13	0.12	0.11	0.05	2d8/10 L=210	18,39,15
		210.0	0.38	7.7	7.7	0.0	0.13	0.13	0.12	0.06	2d8/10 L=210	18,39,15
490	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.04	2d8/10 L=45	18,43,15
		5.6	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.04	2d8/10 L=45	18,43,15
		11.3	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.04	2d8/10 L=45	18,43,15
		16.9	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.04	2d8/10 L=45	18,43,15
		22.5	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.05	2d8/10 L=45	18,43,15
		28.1	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.05	2d8/10 L=45	18,43,15
		33.8	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.05	2d8/10 L=45	18,43,15
		39.4	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.05	2d8/10 L=45	15,43,15
		45.0	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.05	2d8/10 L=45	15,43,15
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.05	2d8/10 L=50	15,46,18
		6.3	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.05	2d8/10 L=50	15,46,18
		12.5	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.05	2d8/10 L=50	15,43,18
		18.8	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.05	2d8/10 L=50	15,43,15
		25.0	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.05	2d8/10 L=50	15,43,15
537	ok,ok s=7,m=3	31.3	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.05	2d8/10 L=50	15,43,15
		37.5	0.38	7.7	7.7	0.0	0.13	0.13	0.14	0.05	2d8/10 L=50	15,43,15
		43.8	0.38	7.7	7.7	0.0	0.13	0.14	0.14	0.06	2d8/10 L=50	15,43,15
		50.0	0.38	7.7	7.7	0.0	0.13	0.15	0.14	0.06	2d8/10 L=50	15,43,15
		0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.03	2d8/10 L=85	39,42,18
		10.6	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.03	2d8/10 L=85	39,42,18
		21.3	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=85	39,42,18
513	ok,ok s=7,m=3	31.9	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=85	39,42,18
		42.5	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.02	2d8/10 L=85	39,42,18
		53.1	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.02	2d8/10 L=85	39,42,18
		63.8	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.02	2d8/10 L=85	19,42,15
		74.4	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.02	2d8/10 L=85	19,42,15
		85.0	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.02	2d8/10 L=85	19,39,15
		0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.03	2d8/10 L=43	19,42,1
508	ok,ok s=7,m=3	5.4	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=43	19,42,1
		10.8	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=43	19,42,22
		16.1	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.02	2d8/10 L=43	19,42,22
		21.5	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=43	19,42,22
		26.9	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=43	19,42,22
		32.3	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=43	19,42,22
		37.6	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=43	22,42,22
		43.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=43	22,42,22
		0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.11	0.05	2d8/10 L=210	22,22,22
		26.3	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.04	2d8/10 L=210	22,22,22
		52.5	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=210	22,22,22
		78.8	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.03	2d8/10 L=210	22,22,19
		105.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.04	2d8/10 L=210	1,19,19
		131.3	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.04	2d8/10 L=210	22,19,19
479	ok,ok s=7,m=3	157.5	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.05	2d8/10 L=210	19,19,1
		183.8	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.07	2d8/10 L=210	19,19,1
		210.0	0.38	7.7	7.7	0.0	0.13	0.14	0.11	0.08	2d8/10 L=210	1,19,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.02	2d8/10 L=87	1,19,15
		10.9	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.02	2d8/10 L=87	1,19,15
		21.8	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03	2d8/10 L=87	1,19,19

		32.6	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.03	2d8/10 L=87	1,19,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.03	2d8/10 L=87	1,19,1
		54.4	0.38	7.7	7.7	0.0	0.13	0.13	0.08	0.04	2d8/10 L=87	1,19,1
		65.3	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.05	2d8/10 L=87	1,19,1
		76.1	0.38	7.7	7.7	0.0	0.13	0.16	0.08	0.05	2d8/10 L=87	1,19,1
		87.0	0.38	7.7	7.7	0.0	0.13	0.18	0.09	0.06	2d8/10 L=87	1,19,1
356	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.09	0.09	2d8/10 L=26	1,30,1
	s=7,m=3	3.3	0.38	7.7	7.7	0.0	0.13	0.17	0.09	0.08	2d8/10 L=26	1,30,1
		6.5	0.38	7.7	7.7	0.0	0.13	0.16	0.09	0.08	2d8/10 L=26	1,30,1
		9.8	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.08	2d8/10 L=26	1,30,1
		13.0	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.08	2d8/10 L=26	1,30,1
		16.3	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.08	2d8/10 L=26	1,30,1
		19.5	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.07	2d8/10 L=26	1,30,1
		22.8	0.38	7.7	7.7	0.0	0.13	0.12	0.09	0.07	2d8/10 L=26	1,30,1
		26.0	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.07	2d8/10 L=26	1,30,1
535	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.12	0.10	2d8/10 L=363	19,30,1
	s=7,m=3	45.4	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.08	2d8/10 L=363	15,30,1
		90.7	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.06	2d8/10 L=363	18,30,1
		136.1	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.04	2d8/10 L=363	1,30,18
		181.5	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.02	2d8/10 L=363	1,30,18
		226.9	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.03	2d8/10 L=363	1,27,15
		272.2	0.38	7.7	7.7	0.0	0.13	0.13	0.10	0.04	2d8/10 L=363	26,27,15
		317.6	0.38	7.7	7.7	0.0	0.13	0.13	0.10	0.06	2d8/10 L=363	26,27,1
		363.0	0.38	7.7	7.7	0.0	0.13	0.16	0.11	0.08	2d8/10 L=363	23,27,1
536	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.12	0.08	2d8/10 L=36	23,27,1
	s=7,m=3	4.5	0.38	7.7	7.7	0.0	0.13	0.17	0.12	0.08	2d8/10 L=36	23,27,1
		9.0	0.38	7.7	7.7	0.0	0.13	0.18	0.12	0.09	2d8/10 L=36	23,27,1
		13.5	0.38	7.7	7.7	0.0	0.13	0.18	0.12	0.09	2d8/10 L=36	23,27,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.19	0.12	0.09	2d8/10 L=36	23,27,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.20	0.12	0.09	2d8/10 L=36	23,27,1
		27.0	0.38	7.7	7.7	0.0	0.13	0.21	0.12	0.09	2d8/10 L=36	23,27,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.22	0.12	0.10	2d8/10 L=36	23,27,1
		36.0	0.38	7.7	7.7	0.0	0.13	0.23	0.12	0.10	2d8/10 L=36	23,27,1
386	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.02	2d8/10 L=100	15,31,18
	s=7,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.02	2d8/10 L=100	1,31,15
		25.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.03	2d8/10 L=100	1,31,15
		37.5	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.03	2d8/10 L=100	1,31,15
		50.0	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.03	2d8/10 L=100	1,31,15
		62.5	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.04	2d8/10 L=100	1,31,15
		75.0	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.04	2d8/10 L=100	1,31,1
		87.5	0.38	7.7	7.7	0.0	0.13	0.16	0.09	0.05	2d8/10 L=100	1,31,1
		100.0	0.38	7.7	7.7	0.0	0.13	0.18	0.10	0.05	2d8/10 L=100	1,31,1
368	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.09	0.09	2d8/10 L=29	1,1,1
	s=7,m=3	3.6	0.38	7.7	7.7	0.0	0.13	0.17	0.09	0.09	2d8/10 L=29	1,1,1
		7.3	0.38	7.7	7.7	0.0	0.13	0.16	0.08	0.08	2d8/10 L=29	1,1,1
		10.9	0.38	7.7	7.7	0.0	0.13	0.15	0.08	0.08	2d8/10 L=29	1,1,1
		14.5	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.08	2d8/10 L=29	1,1,1
		18.1	0.38	7.7	7.7	0.0	0.13	0.13	0.08	0.08	2d8/10 L=29	1,1,1
		21.8	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.08	2d8/10 L=29	1,1,1
		25.4	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.07	2d8/10 L=29	1,1,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.07	2d8/10 L=29	1,1,1
401	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.10	0.11	2d8/10 L=444	1,1,1
	s=7,m=3	55.5	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.08	2d8/10 L=444	15,1,1
		111.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.05	2d8/10 L=444	18,1,1
		166.5	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=444	1,23,18
		222.0	0.38	7.7	7.7	0.0	0.13	0.18	0.06	0.01	2d8/10 L=444	1,23,15
		277.5	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.03	2d8/10 L=444	1,23,15
		333.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.06	2d8/10 L=444	18,23,1
		388.5	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.08	2d8/10 L=444	15,23,1
		444.0	0.38	7.7	7.7	0.0	0.13	0.21	0.11	0.11	2d8/10 L=444	1,1,1
433	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.09	2d8/10 L=27	1,23,1
	s=7,m=3	3.4	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.10	2d8/10 L=27	1,1,1
		6.8	0.38	7.7	7.7	0.0	0.13	0.16	0.09	0.10	2d8/10 L=27	1,1,1
		10.1	0.38	7.7	7.7	0.0	0.13	0.17	0.10	0.10	2d8/10 L=27	1,1,1
		13.5	0.38	7.7	7.7	0.0	0.13	0.18	0.10	0.10	2d8/10 L=27	1,1,1
		16.9	0.38	7.7	7.7	0.0	0.13	0.19	0.10	0.10	2d8/10 L=27	1,1,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.20	0.10	0.10	2d8/10 L=27	1,1,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.21	0.10	0.11	2d8/10 L=27	1,1,1
		27.0	0.38	7.7	7.7	0.0	0.13	0.22	0.10	0.11	2d8/10 L=27	1,1,1
457	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.22	0.09	0.04	2d8/10 L=100	1,23,19
	s=7,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.23	0.09	0.04	2d8/10 L=100	1,23,19
		25.0	0.38	7.7	7.7	0.0	0.13	0.24	0.09	0.04	2d8/10 L=100	1,23,19
		37.5	0.38	7.7	7.7	0.0	0.13	0.25	0.09	0.05	2d8/10 L=100	1,23,19
		50.0	0.38	7.7	7.7	0.0	0.13	0.26	0.10	0.05	2d8/10 L=100	1,23,19
		62.5	0.38	7.7	7.7	0.0	0.13	0.28	0.10	0.05	2d8/10 L=100	1,23,19
		75.0	0.38	7.7	7.7	0.0	0.13	0.29	0.10	0.06	2d8/10 L=100	1,23,19

		87.5	0.38	7.7	7.7	0.0	0.13	0.32	0.10	0.06	2d8/10 L=100	1,23,19
		100.0	0.38	7.7	7.7	0.0	0.13	0.34	0.11	0.07	2d8/10 L=100	1,23,19
326	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.39	0.12	0.13	2d8/10 L=552	1,38,1
	s=7,m=3	69.1	0.38	7.7	7.7	0.0	0.13	0.14	0.10	0.10	2d8/10 L=552	1,38,1
		138.1	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.06	2d8/10 L=552	22,38,1
		207.2	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.03	2d8/10 L=552	1,38,1
		276.3	0.38	7.7	7.7	0.0	0.13	0.18	0.07	9.16e-03	2d8/10 L=552	1,38,18
		345.3	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.02	2d8/10 L=552	1,38,1
		414.4	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.05	2d8/10 L=552	1,38,1
		483.4	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.07	2d8/10 L=552	31,38,1
		552.5	0.38	7.7	7.7	0.0	0.13	0.21	0.09	0.10	2d8/10 L=552	1,35,1
327	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.23	0.21	0.08	2d8/10 L=297	1,34,1
	s=7,m=3	37.2	0.38	7.7	7.7	0.0	0.13	0.15	0.20	0.07	2d8/10 L=297	1,34,1
		74.4	0.38	7.7	7.7	0.0	0.13	0.09	0.19	0.05	2d8/10 L=297	9,34,1
		111.6	0.38	7.7	7.7	0.0	0.13	0.06	0.19	0.04	2d8/10 L=297	9,34,1
		148.8	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.03	2d8/10 L=297	10,34,5
		185.9	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.02	2d8/10 L=297	5,34,5
		223.1	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.01	2d8/10 L=297	5,34,10
		260.3	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.02	2d8/10 L=297	5,34,9
		297.5	0.38	7.7	7.7	0.0	0.13	0.11	0.17	0.03	2d8/10 L=297	10,36,9
M_T= 52 Z=0.0 N=8 N=26												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
364	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=85	27,1,27
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=85	27,1,27
		21.3	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=85	27,1,19
		31.9	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=85	27,1,19
		42.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=85	27,1,19
		53.1	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.04	2d8/10 L=85	23,1,19
		63.8	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.04	2d8/10 L=85	23,1,19
		74.4	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.04	2d8/10 L=85	23,1,19
		85.0	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.04	2d8/10 L=85	23,1,19
444	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.02	2d8/10 L=85	23,1,30
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.02	2d8/10 L=85	23,1,30
		21.3	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.02	2d8/10 L=85	23,1,30
		31.9	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.02	2d8/10 L=85	15,1,30
		42.5	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.01	2d8/10 L=85	15,1,30
		53.1	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.01	2d8/10 L=85	15,1,30
		63.8	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.01	2d8/10 L=85	15,1,30
		74.4	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.01	2d8/10 L=85	15,1,27
		85.0	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.01	2d8/10 L=85	15,1,27
476	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.13	0.07	2d8/10 L=382	15,1,1
	s=7,m=3	47.8	0.38	7.7	7.7	0.0	0.13	0.11	0.12	0.05	2d8/10 L=382	15,1,1
		95.6	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.04	2d8/10 L=382	22,1,1
		143.4	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.03	2d8/10 L=382	1,1,18
		191.3	0.38	7.7	7.7	0.0	0.13	0.12	0.10	0.03	2d8/10 L=382	1,1,18
		239.1	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.02	2d8/10 L=382	1,1,18
		286.9	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.02	2d8/10 L=382	1,1,15
		334.7	0.38	7.7	7.7	0.0	0.13	0.14	0.10	0.03	2d8/10 L=382	18,1,23
		382.5	0.38	7.7	7.7	0.0	0.13	0.15	0.11	0.03	2d8/10 L=382	18,1,23
209	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.09	2d8/10 L=27	18,1,1
	s=7,m=3	3.4	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.09	2d8/10 L=27	18,1,1
		6.9	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.09	2d8/10 L=27	18,1,1
		10.3	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.09	2d8/10 L=27	18,1,1
		13.8	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.09	2d8/10 L=27	18,1,1
		17.2	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.09	2d8/10 L=27	18,1,1
		20.6	0.38	7.7	7.7	0.0	0.13	0.15	0.20	0.09	2d8/10 L=27	18,1,1
		24.1	0.38	7.7	7.7	0.0	0.13	0.15	0.20	0.09	2d8/10 L=27	18,1,1
		27.5	0.38	7.7	7.7	0.0	0.13	0.15	0.20	0.09	2d8/10 L=27	18,1,1
419	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.01	2d8/10 L=100	18,1,1
	s=7,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.02	2d8/10 L=100	18,1,1
		25.0	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.02	2d8/10 L=100	18,1,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.02	2d8/10 L=100	18,1,1
		50.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.03	2d8/10 L=100	18,1,1
		62.5	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.03	2d8/10 L=100	15,1,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.03	2d8/10 L=100	15,1,1
		87.5	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.04	2d8/10 L=100	15,1,1
		100.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=100	23,1,1
397	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.02	2d8/10 L=85	23,1,26
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.02	2d8/10 L=85	23,1,18
		21.3	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.02	2d8/10 L=85	9,1,18
		31.9	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=85	9,1,18
		42.5	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=85	9,1,18
		53.1	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=85	9,1,18
		63.8	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=85	9,1,15
		74.4	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=85	9,1,15
		85.0	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=85	9,1,15

431	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=85	9,1,5
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=85	9,1,5
		21.3	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.01	2d8/10 L=85	9,1,5
		31.9	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.01	2d8/10 L=85	9,1,10
		42.5	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.01	2d8/10 L=85	9,9,10
		53.1	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.02	2d8/10 L=85	9,9,9
		63.8	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.02	2d8/10 L=85	9,9,9
		74.4	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.02	2d8/10 L=85	9,9,9
		85.0	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.02	2d8/10 L=85	9,9,9
M_T= 92 Z=0.0 N=148 N=533												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
320	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.19	0.02	2d8/10 L=85	5,43,22
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.02	2d8/10 L=85	5,43,19
		21.3	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.02	2d8/10 L=85	5,43,19
		31.9	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.02	2d8/10 L=85	5,43,19
		42.5	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.03	2d8/10 L=85	5,43,19
		53.1	0.38	7.7	7.7	0.0	0.13	0.08	0.20	0.03	2d8/10 L=85	5,43,19
		63.8	0.38	7.7	7.7	0.0	0.13	0.08	0.20	0.03	2d8/10 L=85	5,43,19
		74.4	0.38	7.7	7.7	0.0	0.13	0.08	0.20	0.03	2d8/10 L=85	5,43,19
		85.0	0.38	7.7	7.7	0.0	0.13	0.09	0.20	0.03	2d8/10 L=85	5,43,19
375	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.03	2d8/10 L=85	5,41,5
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.03	2d8/10 L=85	5,41,5
		21.3	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.02	2d8/10 L=85	5,41,5
		31.9	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.02	2d8/10 L=85	19,41,5
		42.5	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.02	2d8/10 L=85	19,41,5
		53.1	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.02	2d8/10 L=85	19,41,5
		63.8	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.01	2d8/10 L=85	19,43,5
		74.4	0.38	7.7	7.7	0.0	0.13	0.07	0.12	9.41e-03	2d8/10 L=85	19,43,5
		85.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	7.40e-03	2d8/10 L=85	19,43,19
423	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.08	0.07	2d8/10 L=410	19,42,1
	s=7,m=3	51.3	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.05	2d8/10 L=410	22,42,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.03	2d8/10 L=410	30,42,22
		153.8	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.03	2d8/10 L=410	1,46,22
		205.0	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.02	2d8/10 L=410	1,43,19
		256.3	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.03	2d8/10 L=410	1,43,27
		307.5	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.03	2d8/10 L=410	22,43,27
		358.8	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.05	2d8/10 L=410	22,43,1
		410.0	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.07	2d8/10 L=410	19,43,1
468	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	6.92e-03	2d8/10 L=100	19,39,30
	s=7,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	4.76e-03	2d8/10 L=100	19,39,30
		25.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	5.53e-03	2d8/10 L=100	19,39,19
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	7.24e-03	2d8/10 L=100	19,39,19
		50.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.01	2d8/10 L=100	27,39,1
		62.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=100	27,39,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=100	27,39,1
		87.5	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=100	27,39,1
		100.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.03	2d8/10 L=100	1,39,1
451	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.03	2d8/10 L=85	1,42,1
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.06	0.20	0.03	2d8/10 L=85	27,42,30
		21.3	0.38	7.7	7.7	0.0	0.13	0.06	0.20	0.03	2d8/10 L=85	27,42,30
		31.9	0.38	7.7	7.7	0.0	0.13	0.05	0.20	0.02	2d8/10 L=85	27,42,30
		42.5	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=85	27,42,30
		53.1	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=85	27,42,30
		63.8	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=85	27,39,30
		74.4	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=85	27,39,30
		85.0	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=85	27,39,27
480	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.25	0.03	2d8/10 L=85	27,42,30
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.04	0.25	0.03	2d8/10 L=85	27,42,30
		21.3	0.38	7.7	7.7	0.0	0.13	0.04	0.25	0.02	2d8/10 L=85	27,42,30
		31.9	0.38	7.7	7.7	0.0	0.13	0.05	0.25	0.02	2d8/10 L=85	27,42,30
		42.5	0.38	7.7	7.7	0.0	0.13	0.05	0.25	0.02	2d8/10 L=85	27,42,30
		53.1	0.38	7.7	7.7	0.0	0.13	0.06	0.25	0.02	2d8/10 L=85	27,39,30
		63.8	0.38	7.7	7.7	0.0	0.13	0.06	0.25	0.02	2d8/10 L=85	27,39,27
		74.4	0.38	7.7	7.7	0.0	0.13	0.07	0.25	0.02	2d8/10 L=85	27,39,27
		85.0	0.38	7.7	7.7	0.0	0.13	0.08	0.26	0.03	2d8/10 L=85	27,39,27
M_T= 93 Z=0.0 N=8 N=905												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
321	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	6.56e-03	2d8/10 L=95	1,9,26
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.06	0.15	6.44e-03	2d8/10 L=95	1,9,23
		23.8	0.38	7.7	7.7	0.0	0.13	0.06	0.15	7.56e-03	2d8/10 L=95	1,9,23
		35.6	0.38	7.7	7.7	0.0	0.13	0.05	0.15	9.38e-03	2d8/10 L=95	1,9,9
		47.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.01	2d8/10 L=95	1,9,9
		59.4	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=95	1,9,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=95	1,9,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.02	2d8/10 L=95	1,9,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.03	2d8/10 L=95	1,9,1

460	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.14	5.51e-03	2d8/10 L=95	1,9,26
		11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.14	4.07e-03	2d8/10 L=95	1,9,23
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.14	5.34e-03	2d8/10 L=95	1,9,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.15	9.21e-03	2d8/10 L=95	1,9,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.15	0.01	2d8/10 L=95	1,9,1
		59.4	0.38	7.7	7.7	0.0	0.13	8.95e-03	0.15	0.02	2d8/10 L=95	5,9,1
		71.3	0.38	7.7	7.7	0.0	0.13	4.07e-03	0.15	0.02	2d8/10 L=95	26,9,1
		83.1	0.38	7.7	7.7	0.0	0.13	8.68e-03	0.15	0.02	2d8/10 L=95	9,9,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.03	2d8/10 L=95	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.14	4.19e-03	2d8/10 L=53	1,9,1
437	ok,ok s=7,m=3	6.6	0.38	7.7	7.7	0.0	0.13	0.02	0.14	6.39e-03	2d8/10 L=53	1,9,1
		13.3	0.38	7.7	7.7	0.0	0.13	0.02	0.14	8.59e-03	2d8/10 L=53	1,9,1
		19.9	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.01	2d8/10 L=53	1,9,1
		26.5	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.01	2d8/10 L=53	1,9,1
		33.1	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=53	1,9,1
		39.8	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=53	1,9,1
		46.4	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=53	1,9,1
		53.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=53	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	2.54e-03	2d8/10 L=42	1,9,1
		5.3	0.38	7.7	7.7	0.0	0.13	0.04	0.14	4.30e-03	2d8/10 L=42	1,9,1
471	ok,ok s=7,m=3	10.5	0.38	7.7	7.7	0.0	0.13	0.04	0.15	6.06e-03	2d8/10 L=42	1,9,1
		15.8	0.38	7.7	7.7	0.0	0.13	0.04	0.15	7.83e-03	2d8/10 L=42	1,9,1
		21.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	9.60e-03	2d8/10 L=42	1,9,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=42	1,9,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.01	2d8/10 L=42	1,9,1
		36.8	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.01	2d8/10 L=42	1,9,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=42	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	4.09e-03	2d8/10 L=35	1,9,1
		4.4	0.38	7.7	7.7	0.0	0.13	0.05	0.14	2.61e-03	2d8/10 L=35	1,9,1
		8.8	0.38	7.7	7.7	0.0	0.13	0.05	0.14	1.30e-03	2d8/10 L=35	1,9,9
406	ok,ok s=7,m=3	13.1	0.38	7.7	7.7	0.0	0.13	0.05	0.14	3.64e-04	2d8/10 L=35	1,9,34
		17.5	0.38	7.7	7.7	0.0	0.13	0.05	0.14	1.83e-03	2d8/10 L=35	1,9,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.05	0.14	3.31e-03	2d8/10 L=35	1,9,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.14	4.79e-03	2d8/10 L=35	1,9,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.05	0.14	6.27e-03	2d8/10 L=35	1,9,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	7.75e-03	2d8/10 L=35	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=60	1,9,1
		7.5	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.01	2d8/10 L=60	1,9,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.01	2d8/10 L=60	1,9,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	8.27e-03	2d8/10 L=60	1,9,1
376	ok,ok s=7,m=3	30.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	5.74e-03	2d8/10 L=60	1,9,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	3.20e-03	2d8/10 L=60	1,9,1
		45.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	8.02e-04	2d8/10 L=60	1,9,27
		52.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	2.18e-03	2d8/10 L=60	1,9,19
		60.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	4.39e-03	2d8/10 L=60	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.02	2d8/10 L=95	1,9,1
		11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.02	2d8/10 L=95	1,9,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.02	2d8/10 L=95	1,9,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.01	2d8/10 L=95	1,9,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.11	8.76e-03	2d8/10 L=95	1,9,1
503	ok,ok s=7,m=3	59.4	0.38	7.7	7.7	0.0	0.13	0.01	0.11	4.80e-03	2d8/10 L=95	1,9,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.11	1.56e-03	2d8/10 L=95	1,9,27
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.11	3.69e-03	2d8/10 L=95	1,9,27
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	7.02e-03	2d8/10 L=95	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=18	1,9,1
		2.3	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=18	1,9,1
		4.5	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=18	1,9,1
		6.8	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=18	1,9,1
		9.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	9.36e-03	2d8/10 L=18	1,9,1
		11.3	0.38	7.7	7.7	0.0	0.13	0.01	0.08	8.62e-03	2d8/10 L=18	1,9,1
488	ok,ok s=7,m=3	13.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	7.88e-03	2d8/10 L=18	1,9,1
		15.8	0.38	7.7	7.7	0.0	0.13	0.01	0.07	7.14e-03	2d8/10 L=18	1,9,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	6.40e-03	2d8/10 L=18	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.02	2d8/10 L=77	1,9,1
		9.6	0.38	7.7	7.7	0.0	0.13	6.45e-03	0.07	0.02	2d8/10 L=77	2,9,1
		19.3	0.38	7.7	7.7	0.0	0.13	4.24e-03	0.07	0.01	2d8/10 L=77	10,9,1
		28.9	0.38	7.7	7.7	0.0	0.13	2.90e-03	0.07	9.80e-03	2d8/10 L=77	26,9,1
		38.5	0.38	7.7	7.7	0.0	0.13	4.75e-03	0.06	6.66e-03	2d8/10 L=77	1,9,1
		48.1	0.38	7.7	7.7	0.0	0.13	6.29e-03	0.06	3.53e-03	2d8/10 L=77	1,9,1
		57.8	0.38	7.7	7.7	0.0	0.13	6.88e-03	0.06	1.06e-03	2d8/10 L=77	1,9,27
506	ok,ok s=7,m=3	67.4	0.38	7.7	7.7	0.0	0.13	6.54e-03	0.06	2.75e-03	2d8/10 L=77	1,9,5
		77.0	0.38	7.7	7.7	0.0	0.13	5.25e-03	0.06	5.81e-03	2d8/10 L=77	1,9,1
		0.0	0.38	7.7	7.7	0.0	0.13	5.23e-03	0.05	0.02	2d8/10 L=95	1,5,1
		11.9	0.38	7.7	7.7	0.0	0.13	0.01	0.04	0.01	2d8/10 L=95	1,5,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.01	0.04	8.90e-03	2d8/10 L=95	1,15,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.04	5.10e-03	2d8/10 L=95	1,15,1

		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.04	1.31e-03	2d8/10 L=95	1,15,1
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.04	2.47e-03	2d8/10 L=95	1,15,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.04	6.24e-03	2d8/10 L=95	1,15,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.04	1.00e-02	2d8/10 L=95	1,15,1
		95.0	0.38	7.7	7.7	0.0	0.13	9.21e-03	0.05	0.01	2d8/10 L=95	1,15,1
446	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	9.19e-03	0.08	9.11e-03	2d8/10 L=78	1,10,1
	s=7,m=3	9.8	0.38	7.7	7.7	0.0	0.13	0.01	0.08	6.04e-03	2d8/10 L=78	1,10,1
		19.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	2.97e-03	2d8/10 L=78	1,10,1
		29.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	5.26e-04	2d8/10 L=78	1,10,38
		39.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	3.15e-03	2d8/10 L=78	1,10,1
		48.8	0.38	7.7	7.7	0.0	0.13	0.01	0.08	6.20e-03	2d8/10 L=78	1,10,1
		58.5	0.38	7.7	7.7	0.0	0.13	9.03e-03	0.08	9.25e-03	2d8/10 L=78	1,10,1
		68.3	0.38	7.7	7.7	0.0	0.13	5.75e-03	0.08	0.01	2d8/10 L=78	1,10,1
		78.0	0.38	7.7	7.7	0.0	0.13	3.93e-03	0.08	0.02	2d8/10 L=78	10,10,1
477	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	3.94e-03	0.10	1.51e-03	2d8/10 L=17 10,10,35	
	s=7,m=3	2.1	0.38	7.7	7.7	0.0	0.13	3.92e-03	0.10	1.92e-03	2d8/10 L=17 10,10,13	
		4.3	0.38	7.7	7.7	0.0	0.13	3.93e-03	0.10	2.47e-03	2d8/10 L=17 10,10,13	
		6.4	0.38	7.7	7.7	0.0	0.13	3.96e-03	0.10	3.05e-03	2d8/10 L=17 10,10,1	
		8.5	0.38	7.7	7.7	0.0	0.13	4.00e-03	0.10	3.71e-03	2d8/10 L=17 10,10,1	
		10.6	0.38	7.7	7.7	0.0	0.13	4.06e-03	0.10	4.37e-03	2d8/10 L=17 10,10,1	
		12.8	0.38	7.7	7.7	0.0	0.13	4.14e-03	0.10	5.03e-03	2d8/10 L=17 10,10,1	
		14.9	0.38	7.7	7.7	0.0	0.13	4.23e-03	0.10	5.70e-03	2d8/10 L=17 10,10,1	
		17.0	0.38	7.7	7.7	0.0	0.13	4.38e-03	0.10	6.36e-03	2d8/10 L=17 31,10,1	
424	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	4.39e-03	0.15	4.40e-03	2d8/10 L=54 31,10,38	
	s=7,m=3	6.8	0.38	7.7	7.7	0.0	0.13	4.24e-03	0.15	3.30e-03	2d8/10 L=54 35,10,38	
		13.6	0.38	7.7	7.7	0.0	0.13	4.39e-03	0.15	2.21e-03	2d8/10 L=54 35,10,38	
		20.4	0.38	7.7	7.7	0.0	0.13	4.81e-03	0.15	3.24e-03	2d8/10 L=54 35,10,35	
		27.3	0.38	7.7	7.7	0.0	0.13	5.49e-03	0.15	4.67e-03	2d8/10 L=54 35,10,1	
		34.1	0.38	7.7	7.7	0.0	0.13	6.42e-03	0.15	6.78e-03	2d8/10 L=54 35,10,1	
		40.9	0.38	7.7	7.7	0.0	0.13	7.58e-03	0.15	8.89e-03	2d8/10 L=54 35,10,1	
		47.7	0.38	7.7	7.7	0.0	0.13	8.99e-03	0.15	0.01	2d8/10 L=54 35,10,1	
		54.5	0.38	7.7	7.7	0.0	0.13	0.01	0.16	0.01	2d8/10 L=54 35,10,1	
452	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.19	8.12e-03	2d8/10 L=40 35,10,34	
	s=7,m=3	5.1	0.38	7.7	7.7	0.0	0.13	0.01	0.19	7.32e-03	2d8/10 L=40 35,10,34	
		10.1	0.38	7.7	7.7	0.0	0.13	0.01	0.19	6.52e-03	2d8/10 L=40 31,10,34	
		15.2	0.38	7.7	7.7	0.0	0.13	0.01	0.19	5.72e-03	2d8/10 L=40 31,10,34	
		20.3	0.38	7.7	7.7	0.0	0.13	0.01	0.19	6.02e-03	2d8/10 L=40 31,10,31	
		25.3	0.38	7.7	7.7	0.0	0.13	0.01	0.19	6.86e-03	2d8/10 L=40 31,10,31	
		30.4	0.38	7.7	7.7	0.0	0.13	0.02	0.19	7.69e-03	2d8/10 L=40 31,10,31	
		35.4	0.38	7.7	7.7	0.0	0.13	0.02	0.19	8.53e-03	2d8/10 L=40 31,10,31	
		40.5	0.38	7.7	7.7	0.0	0.13	0.02	0.19	9.37e-03	2d8/10 L=40 31,10,31	
353	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.23	0.02	2d8/10 L=95 31,10,34	
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.23	0.01	2d8/10 L=95 31,10,34	
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.23	0.01	2d8/10 L=95 31,10,34	
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.23	0.01	2d8/10 L=95 31,10,34	
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.23	8.77e-03	2d8/10 L=95 31,10,31	
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=95 31,10,31	
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=95 31,10,31	
		83.1	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.01	2d8/10 L=95 31,10,31	
		95.0	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.02	2d8/10 L=95 31,10,31	
340	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=17 1,23,35	
	s=7,m=3	2.1	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=17 1,23,35	
		4.3	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=17 1,23,35	
		6.4	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=17 1,23,35	
		8.5	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=17 1,23,35	
		10.6	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=17 1,23,35	
		12.8	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=17 1,23,35	
		14.9	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=17 1,23,35	
		17.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=17 1,23,35	
365	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.01	2d8/10 L=47 1,23,35	
	s=7,m=3	5.9	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=47 1,23,35	
		11.9	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=47 1,23,35	
		17.8	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=47 1,23,35	
		23.8	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=47 1,23,35	
		29.7	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=47 1,23,35	
		35.6	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=47 1,23,35	
		41.6	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=47 1,23,35	
		47.5	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=47 1,23,35	
420	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,26,38	
	s=7,m=3	1.3	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	
		2.6	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	
		3.9	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	
		5.3	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	
		6.6	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	
		7.9	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	
		9.2	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10 1,23,38	

398	ok,ok s=7,m=3	10.5	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=10	1,23,38
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.04	2d8/10 L=58	1,9,1
		7.3	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.04	2d8/10 L=58	1,9,1
		14.5	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.03	2d8/10 L=58	35,9,1
		21.8	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=58	35,9,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=58	35,9,1
		36.3	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=58	35,23,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.03	2d8/10 L=58	35,23,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.02	2d8/10 L=58	35,23,1
		58.0	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.02	2d8/10 L=58	35,23,1
432	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.06	0.06	2d8/10 L=442	35,9,1
		55.3	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.04	2d8/10 L=442	38,9,1
		110.5	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.03	2d8/10 L=442	38,9,1
		165.8	0.38	7.7	7.7	0.0	0.13	0.10	0.03	0.01	2d8/10 L=442	26,9,34
		221.0	0.38	7.7	7.7	0.0	0.13	0.11	0.03	7.06e-03	2d8/10 L=442	1,31,38
		276.3	0.38	7.7	7.7	0.0	0.13	0.09	0.03	0.02	2d8/10 L=442	1,31,35
		331.5	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=442	1,31,1
		386.8	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.04	2d8/10 L=442	38,31,1
		442.0	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.06	2d8/10 L=442	35,35,1
M_T= 94 Z=0.0 P=7 P=11												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
322	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.12	0.09	2d8/10 L=58	23,30,26
		7.3	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.08	2d8/10 L=58	23,30,26
		14.6	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.09	2d8/10 L=58	15,30,23
		21.9	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.09	2d8/10 L=58	19,30,23
		29.3	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.09	2d8/10 L=58	19,30,23
		36.6	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.09	2d8/10 L=58	19,30,23
		43.9	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.09	2d8/10 L=58	27,30,23
		51.2	0.38	7.7	7.7	0.0	0.13	0.11	0.11	0.09	2d8/10 L=58	27,30,23
		58.5	0.38	7.7	7.7	0.0	0.13	0.13	0.11	0.10	2d8/10 L=58	27,30,23
		0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.10	0.05	2d8/10 L=58	27,22,26
499	ok,ok s=7,m=3	7.3	0.38	7.7	7.7	0.0	0.13	0.13	0.10	0.05	2d8/10 L=58	27,22,26
		14.6	0.38	7.7	7.7	0.0	0.13	0.13	0.10	0.04	2d8/10 L=58	27,22,26
		21.9	0.38	7.7	7.7	0.0	0.13	0.13	0.10	0.04	2d8/10 L=58	27,22,26
		29.3	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.04	2d8/10 L=58	27,22,26
		36.6	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.04	2d8/10 L=58	27,22,26
		43.9	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.04	2d8/10 L=58	27,22,26
		51.2	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.04	2d8/10 L=58	27,22,26
		58.5	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.03	2d8/10 L=58	27,22,26
		0.0	0.38	7.7	7.7	0.0	0.13	0.30	0.11	0.06	2d8/10 L=123	27,22,30
		15.4	0.38	7.7	7.7	0.0	0.13	0.27	0.11	0.06	2d8/10 L=123	27,22,30
483	ok,ok s=7,m=3	30.8	0.38	7.7	7.7	0.0	0.13	0.25	0.11	0.06	2d8/10 L=123	27,22,30
		46.1	0.38	7.7	7.7	0.0	0.13	0.22	0.10	0.05	2d8/10 L=123	30,22,30
		61.5	0.38	7.7	7.7	0.0	0.13	0.22	0.10	0.05	2d8/10 L=123	30,22,30
		76.9	0.38	7.7	7.7	0.0	0.13	0.22	0.10	0.04	2d8/10 L=123	30,22,30
		92.3	0.38	7.7	7.7	0.0	0.13	0.21	0.10	0.04	2d8/10 L=123	30,22,30
		107.6	0.38	7.7	7.7	0.0	0.13	0.20	0.09	0.04	2d8/10 L=123	30,22,30
		123.0	0.38	7.7	7.7	0.0	0.13	0.19	0.09	0.03	2d8/10 L=123	30,22,30
		0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.09	0.03	2d8/10 L=160	30,22,30
		20.0	0.38	7.7	7.7	0.0	0.13	0.18	0.09	0.03	2d8/10 L=160	30,22,30
		40.0	0.38	7.7	7.7	0.0	0.13	0.17	0.09	0.03	2d8/10 L=160	26,22,27
461	ok,ok s=7,m=3	60.0	0.38	7.7	7.7	0.0	0.13	0.15	0.08	0.03	2d8/10 L=160	26,22,27
		80.0	0.38	7.7	7.7	0.0	0.13	0.13	0.08	0.03	2d8/10 L=160	26,22,27
		100.0	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.04	2d8/10 L=160	26,22,27
		120.0	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.04	2d8/10 L=160	26,22,27
		140.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.04	2d8/10 L=160	26,22,27
		160.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=160	23,22,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.05	2d8/10 L=150	23,22,1
		18.8	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.04	2d8/10 L=150	26,22,26
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.04	2d8/10 L=150	26,22,26
		56.3	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.04	2d8/10 L=150	18,22,26
492	ok,ok s=7,m=3	75.0	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.04	2d8/10 L=150	22,22,26
		93.8	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=150	22,22,26
		112.5	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.03	2d8/10 L=150	30,22,26
		131.3	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.03	2d8/10 L=150	30,22,26
		150.0	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.03	2d8/10 L=150	30,22,23
		0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.03	2d8/10 L=150	30,22,23
		18.8	0.38	7.7	7.7	0.0	0.13	0.12	0.09	0.03	2d8/10 L=150	30,22,23
		37.5	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.04	2d8/10 L=150	30,22,23
		56.3	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.04	2d8/10 L=150	30,22,23
		75.0	0.38	7.7	7.7	0.0	0.13	0.16	0.09	0.05	2d8/10 L=150	30,22,23
509	ok,ok s=7,m=3	93.8	0.38	7.7	7.7	0.0	0.13	0.17	0.08	0.05	2d8/10 L=150	30,22,23
		112.5	0.38	7.7	7.7	0.0	0.13	0.18	0.08	0.06	2d8/10 L=150	30,22,23
		131.3	0.38	7.7	7.7	0.0	0.13	0.20	0.08	0.06	2d8/10 L=150	23,22,23
		150.0	0.38	7.7	7.7	0.0	0.13	0.24	0.08	0.07	2d8/10 L=150	23,22,23
		0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.18	0.04	2d8/10 L=125	27,42,18
515		ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.18	0.04	2d8/10 L=125

438	ok,ok s=7,m=3	s=7,m=3	15.6	0.38	7.7	7.7	0.0	0.13	0.12	0.18	0.04	2d8/10 L=125 27,42,18
		31.3	0.38	7.7	7.7	0.0	0.13	0.13	0.18	0.04	2d8/10 L=125 27,42,26	
		46.9	0.38	7.7	7.7	0.0	0.13	0.14	0.17	0.03	2d8/10 L=125 27,42,26	
		62.5	0.38	7.7	7.7	0.0	0.13	0.15	0.17	0.03	2d8/10 L=125 23,39,23	
		78.1	0.38	7.7	7.7	0.0	0.13	0.16	0.17	0.04	2d8/10 L=125 23,39,23	
		93.8	0.38	7.7	7.7	0.0	0.13	0.18	0.18	0.04	2d8/10 L=125 23,39,23	
		109.4	0.38	7.7	7.7	0.0	0.13	0.20	0.18	0.05	2d8/10 L=125 23,39,23	
		125.0	0.38	7.7	7.7	0.0	0.13	0.22	0.18	0.05	2d8/10 L=125 23,39,23	
		0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.02	2d8/10 L=98 23,42,30	
		12.3	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.02	2d8/10 L=98 23,42,30	
472	ok,ok s=7,m=3	24.6	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.01	2d8/10 L=98 23,42,30	
		36.9	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.01	2d8/10 L=98 23,42,30	
		49.2	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=98 23,42,27	
		61.5	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=98 23,42,27	
		73.7	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=98 23,42,23	
		86.0	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=98 23,42,23	
		98.3	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=98 23,42,1	
		0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=98 23,42,30	
		12.3	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=98 23,42,26	
		24.6	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.03	2d8/10 L=98 23,42,26	
494	ok,ok s=7,m=3	36.9	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.03	2d8/10 L=98 23,42,26	
		49.2	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.02	2d8/10 L=98 23,42,26	
		61.5	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=98 23,42,26	
		73.8	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=98 23,42,23	
		86.0	0.38	7.7	7.7	0.0	0.13	0.01	0.12	0.02	2d8/10 L=98 27,42,23	
		98.3	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.03	2d8/10 L=98 27,42,23	
		0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=98 27,22,1	
		12.3	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=98 27,22,1	
		24.6	0.38	7.7	7.7	0.0	0.13	0.02	0.09	8.40e-03	2d8/10 L=98 27,22,1	
		36.9	0.38	7.7	7.7	0.0	0.13	0.01	0.09	4.59e-03	2d8/10 L=98 27,22,1	
407	ok,ok s=7,m=3	49.2	0.38	7.7	7.7	0.0	0.13	0.01	0.09	2.22e-03	2d8/10 L=98 27,22,26	
		61.5	0.38	7.7	7.7	0.0	0.13	0.02	0.09	3.39e-03	2d8/10 L=98 27,22,23	
		73.7	0.38	7.7	7.7	0.0	0.13	0.02	0.09	6.79e-03	2d8/10 L=98 27,22,1	
		86.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=98 27,22,1	
		98.3	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=98 27,22,1	
		0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=98 27,22,1	
		12.3	0.38	7.7	7.7	0.0	0.13	0.02	0.09	9.97e-03	2d8/10 L=98 27,22,1	
		24.6	0.38	7.7	7.7	0.0	0.13	0.02	0.09	6.23e-03	2d8/10 L=98 27,22,1	
		36.9	0.38	7.7	7.7	0.0	0.13	0.02	0.09	2.49e-03	2d8/10 L=98 27,22,1	
		49.2	0.38	7.7	7.7	0.0	0.13	0.02	0.09	1.42e-03	2d8/10 L=98 27,22,23	
448	ok,ok s=7,m=3	61.5	0.38	7.7	7.7	0.0	0.13	0.02	0.09	4.95e-03	2d8/10 L=98 27,22,1	
		73.8	0.38	7.7	7.7	0.0	0.13	0.02	0.09	8.65e-03	2d8/10 L=98 27,22,1	
		86.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=98 27,22,1	
		98.3	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.02	2d8/10 L=98 27,22,1	
		0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.02	2d8/10 L=98 27,22,26	
		12.3	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=98 23,22,26	
		24.6	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=98 23,22,26	
		36.9	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=98 23,22,26	
		49.2	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=98 23,22,23	
		61.5	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.02	2d8/10 L=98 23,22,23	
478	ok,ok s=7,m=3	73.7	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=98 23,22,23	
		86.0	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=98 23,22,23	
		98.3	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.03	2d8/10 L=98 23,22,23	
		0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.02	2d8/10 L=98 23,42,1	
		12.3	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=98 23,42,1	
		24.6	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=98 23,42,1	
		36.9	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.01	2d8/10 L=98 26,42,22	
		49.2	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=98 26,42,22	
		61.5	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.01	2d8/10 L=98 26,42,22	
		73.8	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.01	2d8/10 L=98 26,42,30	
496	ok,ok s=7,m=3	86.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.01	2d8/10 L=98 26,42,27	
		98.3	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.01	2d8/10 L=98 26,42,27	
		0.0	0.38	7.7	7.7	0.0	0.13	0.23	0.18	0.05	2d8/10 L=114 26,42,26	
		14.3	0.38	7.7	7.7	0.0	0.13	0.22	0.18	0.05	2d8/10 L=114 26,42,26	
		28.5	0.38	7.7	7.7	0.0	0.13	0.22	0.18	0.04	2d8/10 L=114 26,42,26	
		42.8	0.38	7.7	7.7	0.0	0.13	0.21	0.18	0.04	2d8/10 L=114 26,42,18	
		57.0	0.38	7.7	7.7	0.0	0.13	0.21	0.18	0.04	2d8/10 L=114 26,42,18	
		71.3	0.38	7.7	7.7	0.0	0.13	0.20	0.18	0.04	2d8/10 L=114 26,42,18	
		85.5	0.38	7.7	7.7	0.0	0.13	0.20	0.17	0.03	2d8/10 L=114 30,42,18	
		99.8	0.38	7.7	7.7	0.0	0.13	0.20	0.17	0.03	2d8/10 L=114 30,42,18	
510	ok,ok s=7,m=3	114.0	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=114 30,42,15	
		0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15	
		2.6	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15	
		5.3	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15	
		7.9	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15	
			10.5	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15

519	ok,ok s=7,m=3	13.1	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15
		15.8	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15
		18.4	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15
		21.0	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.03	2d8/10 L=21 30,42,15
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=119 30,18,27
		14.9	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.02	2d8/10 L=119 30,18,27
		29.8	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=119 30,18,27
		44.6	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=119 30,18,27
		59.5	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=119 30,18,27
		74.4	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.03	2d8/10 L=119 27,18,1
516	ok,ok s=7,m=3	89.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.03	2d8/10 L=119 27,18,1
		104.1	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.04	2d8/10 L=119 1,18,1
		119.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=119 1,18,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=150 1,18,1
		18.8	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.04	2d8/10 L=150 1,18,1
		37.5	0.38	7.7	7.7	0.0	0.13	9.47e-03	0.07	0.04	2d8/10 L=150 1,18,1
		56.3	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.03	2d8/10 L=150 22,18,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=150 22,18,1
		93.8	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=150 1,18,1
		112.5	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.01	2d8/10 L=150 1,18,1
521	ok,ok s=7,m=3	131.3	0.38	7.7	7.7	0.0	0.13	0.05	0.06	8.26e-03	2d8/10 L=150 1,18,26
		150.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	4.50e-03	2d8/10 L=150 1,18,26
		0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	4.51e-03	2d8/10 L=160 1,22,26
		20.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	4.74e-03	2d8/10 L=160 26,22,23
		40.0	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.01	2d8/10 L=160 26,22,1
		60.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=160 26,22,1
		80.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=160 26,22,1
		100.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=160 26,22,1
		120.0	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.04	2d8/10 L=160 26,22,1
		140.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.04	2d8/10 L=160 23,22,1
523	ok,ok s=7,m=3	160.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.05	2d8/10 L=160 1,22,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=149 1,18,1
		18.7	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=149 23,18,1
		37.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.03	2d8/10 L=149 23,18,1
		56.0	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=149 26,18,1
		74.7	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.01	2d8/10 L=149 26,18,1
		93.4	0.38	7.7	7.7	0.0	0.13	0.04	0.05	7.67e-03	2d8/10 L=149 26,18,1
		112.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	3.88e-03	2d8/10 L=149 26,22,30
		130.7	0.38	7.7	7.7	0.0	0.13	0.04	0.05	7.57e-03	2d8/10 L=149 26,22,27
		149.4	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=149 26,18,27
524	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=122 26,18,27
		15.2	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=122 26,18,1
		30.4	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=122 23,18,1
		45.6	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=122 23,18,1
		60.8	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=122 23,18,1
		76.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.04	2d8/10 L=122 23,18,1
		91.2	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.04	2d8/10 L=122 23,18,1
		106.4	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.05	2d8/10 L=122 23,1,1
		121.6	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.06	2d8/10 L=122 1,1,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.03	2d8/10 L=19 23,1,23
497	ok,ok s=7,m=3	2.4	0.38	7.7	7.7	0.0	0.13	0.10	0.15	0.03	2d8/10 L=19 23,1,23
		4.8	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.03	2d8/10 L=19 23,1,23
		7.1	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.03	2d8/10 L=19 23,1,23
		9.5	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.04	2d8/10 L=19 23,1,23
		11.9	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.04	2d8/10 L=19 23,1,23
		14.3	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=19 23,1,23
		16.6	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=19 23,1,23
		19.0	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=19 23,1,23
		0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.17	0.04	2d8/10 L=115 23,1,26
		14.4	0.38	7.7	7.7	0.0	0.13	0.11	0.17	0.04	2d8/10 L=115 23,1,26
339	ok,ok s=7,m=3	28.8	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=115 23,1,26
		43.1	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=115 27,1,26
		57.5	0.38	7.7	7.7	0.0	0.13	0.12	0.15	0.04	2d8/10 L=115 27,1,26
		71.9	0.38	7.7	7.7	0.0	0.13	0.13	0.15	0.03	2d8/10 L=115 27,1,26
		86.3	0.38	7.7	7.7	0.0	0.13	0.14	0.15	0.03	2d8/10 L=115 23,1,26
		100.6	0.38	7.7	7.7	0.0	0.13	0.15	0.14	0.03	2d8/10 L=115 23,1,23
		115.0	0.38	7.7	7.7	0.0	0.13	0.16	0.14	0.03	2d8/10 L=115 23,35,23
		0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.01	2d8/10 L=74 27,1,1
		9.3	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.01	2d8/10 L=74 27,1,1
		18.6	0.38	7.7	7.7	0.0	0.13	0.06	0.14	7.88e-03	2d8/10 L=74 23,1,1
377	ok,ok s=7,m=3	27.9	0.38	7.7	7.7	0.0	0.13	0.06	0.14	5.13e-03	2d8/10 L=74 23,1,38
		37.2	0.38	7.7	7.7	0.0	0.13	0.06	0.14	3.62e-03	2d8/10 L=74 23,1,35
		46.5	0.38	7.7	7.7	0.0	0.13	0.06	0.14	5.86e-03	2d8/10 L=74 23,1,35
		55.8	0.38	7.7	7.7	0.0	0.13	0.06	0.14	8.15e-03	2d8/10 L=74 23,1,35
		65.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.01	2d8/10 L=74 23,1,35
		74.3	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.01	2d8/10 L=74 23,1,35

425	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.03	2d8/10 L=74	23,1,26
		9.3	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=74	23,1,26
		18.6	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.03	2d8/10 L=74	23,1,26
		27.9	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.02	2d8/10 L=74	23,1,26
		37.2	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.02	2d8/10 L=74	23,1,26
		46.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.02	2d8/10 L=74	23,1,23
		55.7	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.02	2d8/10 L=74	23,1,23
		65.0	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.02	2d8/10 L=74	23,1,23
		74.3	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=74	23,1,23
453	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.02	2d8/10 L=74	23,1,26
		9.3	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.01	2d8/10 L=74	27,1,26
		18.6	0.38	7.7	7.7	0.0	0.13	0.01	0.13	0.01	2d8/10 L=74	27,1,26
		27.9	0.38	7.7	7.7	0.0	0.13	9.48e-03	0.12	9.88e-03	2d8/10 L=74	27,1,26
		37.2	0.38	7.7	7.7	0.0	0.13	7.16e-03	0.12	7.64e-03	2d8/10 L=74	27,1,26
		46.5	0.38	7.7	7.7	0.0	0.13	6.37e-03	0.12	7.36e-03	2d8/10 L=74	43,1,23
		55.8	0.38	7.7	7.7	0.0	0.13	6.79e-03	0.13	8.99e-03	2d8/10 L=74	43,1,27
		65.0	0.38	7.7	7.7	0.0	0.13	8.45e-03	0.13	0.01	2d8/10 L=74	27,1,27
		74.3	0.38	7.7	7.7	0.0	0.13	0.01	0.13	0.01	2d8/10 L=74	27,1,27
354	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.01	2d8/10 L=83	27,35,1
		10.4	0.38	7.7	7.7	0.0	0.13	9.18e-03	0.14	0.01	2d8/10 L=83	27,35,1
		20.8	0.38	7.7	7.7	0.0	0.13	7.39e-03	0.14	7.15e-03	2d8/10 L=83	27,35,1
		31.3	0.38	7.7	7.7	0.0	0.13	6.20e-03	0.14	3.94e-03	2d8/10 L=83	27,35,38
		41.7	0.38	7.7	7.7	0.0	0.13	5.62e-03	0.14	2.46e-03	2d8/10 L=83	23,35,38
		52.1	0.38	7.7	7.7	0.0	0.13	5.92e-03	0.14	4.74e-03	2d8/10 L=83	23,35,35
		62.5	0.38	7.7	7.7	0.0	0.13	6.95e-03	0.14	7.38e-03	2d8/10 L=83	23,35,35
		72.9	0.38	7.7	7.7	0.0	0.13	9.03e-03	0.14	0.01	2d8/10 L=83	35,35,1
		83.3	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.01	2d8/10 L=83	35,35,1
392	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.16	0.01	2d8/10 L=83	35,35,38
		10.4	0.38	7.7	7.7	0.0	0.13	0.01	0.16	0.01	2d8/10 L=83	35,35,38
		20.8	0.38	7.7	7.7	0.0	0.13	0.01	0.17	0.01	2d8/10 L=83	35,35,38
		31.2	0.38	7.7	7.7	0.0	0.13	0.01	0.17	0.01	2d8/10 L=83	35,35,38
		41.7	0.38	7.7	7.7	0.0	0.13	0.02	0.17	9.62e-03	2d8/10 L=83	35,35,35
		52.1	0.38	7.7	7.7	0.0	0.13	0.02	0.17	0.01	2d8/10 L=83	35,35,35
		62.5	0.38	7.7	7.7	0.0	0.13	0.02	0.17	0.01	2d8/10 L=83	35,35,35
		72.9	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=83	35,35,35
		83.3	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=83	35,35,35
429	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=29	35,35,38
		3.6	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=29	35,35,38
		7.2	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=29	35,35,38
		10.8	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=29	35,35,38
		14.4	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=29	35,35,38
		18.0	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.01	2d8/10 L=29	35,35,38
		21.6	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.01	2d8/10 L=29	35,35,38
		25.2	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.01	2d8/10 L=29	35,35,38
		28.8	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.01	2d8/10 L=29	35,35,35
456	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=54	35,35,38
		6.8	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=54	35,35,38
		13.6	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=54	35,35,35
		20.4	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=54	35,35,35
		27.3	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.01	2d8/10 L=54	35,35,35
		34.1	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.01	2d8/10 L=54	35,35,35
		40.9	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.01	2d8/10 L=54	35,35,35
		47.7	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.01	2d8/10 L=54	35,35,35
		54.5	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=54	35,35,35
341	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=81	35,35,38
		10.1	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=81	35,35,38
		20.3	0.38	7.7	7.7	0.0	0.13	0.03	0.14	8.75e-03	2d8/10 L=81	35,35,38
		30.4	0.38	7.7	7.7	0.0	0.13	0.02	0.14	6.15e-03	2d8/10 L=81	35,35,38
		40.5	0.38	7.7	7.7	0.0	0.13	0.02	0.14	6.97e-03	2d8/10 L=81	35,35,35
		50.6	0.38	7.7	7.7	0.0	0.13	0.02	0.14	8.08e-03	2d8/10 L=81	1,35,35
		60.8	0.38	7.7	7.7	0.0	0.13	0.02	0.14	9.41e-03	2d8/10 L=81	1,35,1
		70.9	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=81	1,35,1
		81.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=81	1,35,1
366	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01	2d8/10 L=81	1,35,38
		10.1	0.38	7.7	7.7	0.0	0.13	0.03	0.13	8.56e-03	2d8/10 L=81	1,35,34
		20.3	0.38	7.7	7.7	0.0	0.13	0.03	0.13	6.09e-03	2d8/10 L=81	1,35,34
		30.4	0.38	7.7	7.7	0.0	0.13	0.03	0.13	3.68e-03	2d8/10 L=81	9,35,34
		40.5	0.38	7.7	7.7	0.0	0.13	0.03	0.14	3.11e-03	2d8/10 L=81	9,35,9
		50.6	0.38	7.7	7.7	0.0	0.13	0.03	0.14	5.72e-03	2d8/10 L=81	9,35,9
		60.8	0.38	7.7	7.7	0.0	0.13	0.03	0.14	8.31e-03	2d8/10 L=81	9,35,9
		70.9	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=81	9,35,9
		81.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=81	9,35,1
399	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.03	2d8/10 L=81	9,1,1
		10.1	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.03	2d8/10 L=81	9,1,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.03	2d8/10 L=81	9,35,1
		30.4	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=81	9,35,1

		40.5	0.38	7.7	7.7	0.0	0.13	9.56e-03	0.14	0.02	2d8/10 L=81	9,35,1
		50.6	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.02	2d8/10 L=81	38,35,1
		60.8	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=81	38,35,1
		70.9	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.01	2d8/10 L=81	38,35,1
		81.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=81	38,35,1
		M_T= 95 Z=0.0 N=533 N=1242										
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
328	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.17	0.13	0.05	2d8/10 L=87	42,27,42
	s=7,m=3	10.9	0.38	7.7	7.7	0.0	0.13	0.15	0.13	0.05	2d8/10 L=87	42,27,42
		21.8	0.38	7.7	7.7	0.0	0.13	0.14	0.13	0.05	2d8/10 L=87	42,27,42
		32.6	0.38	7.7	7.7	0.0	0.13	0.13	0.13	0.05	2d8/10 L=87	42,27,42
		43.5	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.05	2d8/10 L=87	42,27,46
		54.4	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.05	2d8/10 L=87	42,27,46
		65.3	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.05	2d8/10 L=87	42,27,43
		76.1	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.05	2d8/10 L=87	46,27,43
		87.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.05	2d8/10 L=87	46,27,43
463	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=140	42,27,43
	s=7,m=3	17.5	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.03	2d8/10 L=140	42,27,39
		35.0	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.03	2d8/10 L=140	42,27,39
		52.5	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.03	2d8/10 L=140	42,27,39
		70.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.04	2d8/10 L=140	42,27,39
		87.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.04	2d8/10 L=140	42,27,39
		105.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.05	2d8/10 L=140	19,27,1
		122.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.05	2d8/10 L=140	19,27,1
		140.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.06	2d8/10 L=140	1,27,1
440	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.03	2d8/10 L=58	1,27,1
	s=7,m=3	7.3	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=58	1,27,1
		14.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.04	2d8/10 L=58	1,27,1
		21.8	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.04	2d8/10 L=58	1,27,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.05	2d8/10 L=58	1,27,1
		36.3	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.05	2d8/10 L=58	1,27,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.05	2d8/10 L=58	1,27,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.06	2d8/10 L=58	1,27,1
		58.0	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.06	2d8/10 L=58	1,27,1
473	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=35	1,27,43
	s=7,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=35	1,27,43
		8.8	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.02	2d8/10 L=35	1,27,43
		13.1	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.02	2d8/10 L=35	1,27,43
		17.5	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.02	2d8/10 L=35	1,27,43
		21.9	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.02	2d8/10 L=35	1,27,43
		26.3	0.38	7.7	7.7	0.0	0.13	0.13	0.13	0.02	2d8/10 L=35	1,27,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.13	0.13	0.03	2d8/10 L=35	1,27,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.13	0.13	0.03	2d8/10 L=35	1,27,1
495	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.06	2d8/10 L=54	1,46,1
	s=7,m=3	6.8	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.06	2d8/10 L=54	1,46,1
		13.6	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.06	2d8/10 L=54	1,46,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.06	2d8/10 L=54	1,46,1
		27.1	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.05	2d8/10 L=54	1,46,1
		33.9	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.05	2d8/10 L=54	1,46,1
		40.7	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.05	2d8/10 L=54	1,46,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=54	1,46,1
		54.3	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.04	2d8/10 L=54	35,46,1
410	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.06	2d8/10 L=210	31,46,1
	s=7,m=3	26.3	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=210	31,46,1
		52.5	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.04	2d8/10 L=210	38,46,1
		78.8	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.03	2d8/10 L=210	38,46,38
		105.0	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.03	2d8/10 L=210	1,46,38
		131.3	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=210	1,46,34
		157.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=210	1,46,31
		183.8	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=210	46,43,31
		210.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.04	2d8/10 L=210	42,43,31
380	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	9.24e-03	2d8/10 L=81	1,30,1
	s=7,m=3	10.1	0.38	7.7	7.7	0.0	0.13	0.03	0.05	4.69e-03	2d8/10 L=81	1,30,1
		20.2	0.38	7.7	7.7	0.0	0.13	0.03	0.05	3.13e-03	2d8/10 L=81	1,30,31
		30.3	0.38	7.7	7.7	0.0	0.13	0.03	0.05	5.57e-03	2d8/10 L=81	1,30,31
		40.4	0.38	7.7	7.7	0.0	0.13	0.03	0.05	9.06e-03	2d8/10 L=81	1,30,1
		50.5	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.01	2d8/10 L=81	42,30,1
		60.6	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.02	2d8/10 L=81	42,30,1
		70.7	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.02	2d8/10 L=81	42,30,1
		80.8	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.03	2d8/10 L=81	39,30,1
357	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=95	39,18,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=95	42,18,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=95	42,18,42
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.06	7.49e-03	2d8/10 L=95	42,18,42
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.06	5.53e-03	2d8/10 L=95	1,18,39
		59.4	0.38	7.7	7.7	0.0	0.13	0.01	0.06	8.29e-03	2d8/10 L=95	1,18,39

		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.06	0.01	2d8/10 L=95	1,18,1
		83.1	0.38	7.7	7.7	0.0	0.13	5.72e-03	0.06	0.02	2d8/10 L=95	42,18,1
		95.0	0.38	7.7	7.7	0.0	0.13	7.49e-03	0.06	0.02	2d8/10 L=95	39,18,1
345	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	7.47e-03	0.08	9.92e-03	2d8/10 L=54	39,22,1
	s=7,m=3	6.8	0.38	7.7	7.7	0.0	0.13	6.47e-03	0.08	7.04e-03	2d8/10 L=54	35,22,46
		13.6	0.38	7.7	7.7	0.0	0.13	5.94e-03	0.07	5.35e-03	2d8/10 L=54	35,22,46
		20.4	0.38	7.7	7.7	0.0	0.13	6.01e-03	0.07	3.66e-03	2d8/10 L=54	6,22,46
		27.3	0.38	7.7	7.7	0.0	0.13	6.43e-03	0.07	4.15e-03	2d8/10 L=54	6,22,43
		34.1	0.38	7.7	7.7	0.0	0.13	7.13e-03	0.07	6.58e-03	2d8/10 L=54	6,18,1
		40.9	0.38	7.7	7.7	0.0	0.13	8.11e-03	0.07	9.91e-03	2d8/10 L=54	6,18,1
		47.7	0.38	7.7	7.7	0.0	0.13	9.68e-03	0.07	0.01	2d8/10 L=54	43,18,1
		54.5	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.02	2d8/10 L=54	43,18,1
414	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=40	43,22,46
	s=7,m=3	5.1	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=40	43,22,46
		10.1	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=40	43,22,46
		15.2	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=40	43,22,46
		20.3	0.38	7.7	7.7	0.0	0.13	0.02	0.08	9.04e-03	2d8/10 L=40	43,22,46
		25.3	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=40	43,22,43
		30.4	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=40	43,22,43
		35.4	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=40	43,22,39
		40.5	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=40	43,22,39
387	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.03	2d8/10 L=95	43,42,46
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=95	43,42,46
		23.8	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.03	2d8/10 L=95	46,42,46
		35.6	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=95	46,42,46
		47.5	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=95	46,42,43
		59.4	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=95	46,39,43
		71.3	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=95	46,39,43
		83.1	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.03	2d8/10 L=95	43,39,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.04	2d8/10 L=95	43,39,39
369	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.13	0.05	2d8/10 L=65	39,24,42
	s=7,m=3	8.1	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.05	2d8/10 L=65	39,24,42
		16.1	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.05	2d8/10 L=65	39,24,42
		24.2	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.04	2d8/10 L=65	39,27,42
		32.3	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.04	2d8/10 L=65	39,27,42
		40.3	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.04	2d8/10 L=65	39,27,42
		48.4	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.04	2d8/10 L=65	39,27,46
		56.4	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=65	39,27,43
		64.5	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.04	2d8/10 L=65	39,27,43
402	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.03	2d8/10 L=130	46,27,43
	s=7,m=3	16.3	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.04	2d8/10 L=130	46,27,35
		32.5	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=130	46,27,35
		48.8	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.05	2d8/10 L=130	43,27,35
		65.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.05	2d8/10 L=130	39,27,35
		81.3	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.06	2d8/10 L=130	1,27,35
		97.5	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.06	2d8/10 L=130	1,27,35
		113.8	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.07	2d8/10 L=130	1,27,35
		130.0	0.38	7.7	7.7	0.0	0.13	0.13	0.16	0.07	2d8/10 L=130	1,27,35
434	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.03	2d8/10 L=67	1,23,1
	s=7,m=3	8.3	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.03	2d8/10 L=67	1,23,1
		16.7	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=67	1,23,1
		25.0	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.04	2d8/10 L=67	1,23,1
		33.3	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.04	2d8/10 L=67	1,23,1
		41.7	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.05	2d8/10 L=67	1,23,1
		50.0	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.05	2d8/10 L=67	1,23,1
		58.3	0.38	7.7	7.7	0.0	0.13	0.12	0.15	0.06	2d8/10 L=67	1,23,1
		66.7	0.38	7.7	7.7	0.0	0.13	0.14	0.15	0.06	2d8/10 L=67	1,23,1
458	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.11	4.99e-03	2d8/10 L=39	1,23,31
	s=7,m=3	4.9	0.38	7.7	7.7	0.0	0.13	0.14	0.11	6.44e-03	2d8/10 L=39	1,23,39
		9.7	0.38	7.7	7.7	0.0	0.13	0.14	0.11	7.93e-03	2d8/10 L=39	1,23,39
		14.6	0.38	7.7	7.7	0.0	0.13	0.14	0.12	9.43e-03	2d8/10 L=39	1,27,39
		19.4	0.38	7.7	7.7	0.0	0.13	0.14	0.12	0.01	2d8/10 L=39	1,27,39
		24.3	0.38	7.7	7.7	0.0	0.13	0.14	0.12	0.01	2d8/10 L=39	1,27,1
		29.1	0.38	7.7	7.7	0.0	0.13	0.14	0.12	0.02	2d8/10 L=39	1,27,1
		34.0	0.38	7.7	7.7	0.0	0.13	0.15	0.12	0.02	2d8/10 L=39	1,27,1
		38.8	0.38	7.7	7.7	0.0	0.13	0.15	0.12	0.02	2d8/10 L=39	1,27,1
491	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.10	0.01	2d8/10 L=28	1,27,1
	s=7,m=3	3.5	0.38	7.7	7.7	0.0	0.13	0.15	0.10	0.01	2d8/10 L=28	1,27,1
		7.0	0.38	7.7	7.7	0.0	0.13	0.15	0.10	0.01	2d8/10 L=28	1,27,34
		10.4	0.38	7.7	7.7	0.0	0.13	0.15	0.10	0.01	2d8/10 L=28	1,27,34
		13.9	0.38	7.7	7.7	0.0	0.13	0.14	0.10	9.23e-03	2d8/10 L=28	1,27,34
		17.4	0.38	7.7	7.7	0.0	0.13	0.14	0.10	8.23e-03	2d8/10 L=28	1,23,34
		20.9	0.38	7.7	7.7	0.0	0.13	0.14	0.10	7.24e-03	2d8/10 L=28	1,23,34
		24.4	0.38	7.7	7.7	0.0	0.13	0.14	0.10	6.26e-03	2d8/10 L=28	1,23,34
		27.8	0.38	7.7	7.7	0.0	0.13	0.14	0.10	6.10e-03	2d8/10 L=28	1,23,39
482	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.04	2d8/10 L=67	1,23,1

498	ok,ok s=7,m=3	8.3	0.38	7.7	7.7	0.0	0.13	0.13	0.08	0.03	2d8/10 L=67	1,23,1		
		16.7	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.03	2d8/10 L=67	1,23,1		
		25.0	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.02	2d8/10 L=67	1,23,1		
		33.3	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.02	2d8/10 L=67	1,23,1		
		41.7	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.01	2d8/10 L=67	1,23,1		
		50.0	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.01	2d8/10 L=67	1,23,38		
		58.3	0.38	7.7	7.7	0.0	0.13	0.10	0.07	7.82e-03	2d8/10 L=67	1,23,38		
		66.7	0.38	7.7	7.7	0.0	0.13	0.10	0.07	5.62e-03	2d8/10 L=67	1,23,38		
		0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.03	2d8/10 L=70	1,15,1		
		8.8	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=70	1,15,1		
		17.6	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.03	2d8/10 L=70	1,15,1		
		26.4	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=70	1,15,1		
		35.3	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=70	1,15,1		
		44.1	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.01	2d8/10 L=70	1,15,26		
		52.9	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.01	2d8/10 L=70	1,23,26		
		61.7	0.38	7.7	7.7	0.0	0.13	0.06	0.05	8.06e-03	2d8/10 L=70	1,23,26		
		70.5	0.38	7.7	7.7	0.0	0.13	0.06	0.05	7.90e-03	2d8/10 L=70	1,23,23		
		0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=70	1,15,1		
		8.8	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.01	2d8/10 L=70	1,15,1		
		511	ok,ok s=7,m=3	17.6	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.01	2d8/10 L=70	1,15,1
26.4	0.38			7.7	7.7	0.0	0.13	0.05	0.07	6.18e-03	2d8/10 L=70	1,15,22		
35.3	0.38			7.7	7.7	0.0	0.13	0.05	0.07	3.96e-03	2d8/10 L=70	1,15,22		
44.1	0.38			7.7	7.7	0.0	0.13	0.05	0.07	4.69e-03	2d8/10 L=70	1,15,19		
52.9	0.38			7.7	7.7	0.0	0.13	0.05	0.08	7.20e-03	2d8/10 L=70	1,15,19		
61.7	0.38			7.7	7.7	0.0	0.13	0.05	0.08	0.01	2d8/10 L=70	1,15,1		
70.5	0.38			7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=70	1,15,1		
0.0	0.38			7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=39	1,15,30		
4.9	0.38			7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=39	1,15,30		
9.9	0.38			7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=39	1,15,30		
14.8	0.38			7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=39	1,15,30		
19.8	0.38			7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=39	1,15,30		
24.7	0.38			7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=39	1,15,27		
29.6	0.38			7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=39	1,15,27		
34.6	0.38			7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=39	1,15,27		
39.5	0.38			7.7	7.7	0.0	0.13	0.06	0.10	0.03	2d8/10 L=39	1,15,27		
0.0	0.38			7.7	7.7	0.0	0.13	0.04	0.20	0.05	2d8/10 L=31	27,26,1		
3.9	0.38			7.7	7.7	0.0	0.13	0.04	0.20	0.05	2d8/10 L=31	27,26,1		
7.8	0.38			7.7	7.7	0.0	0.13	0.03	0.20	0.04	2d8/10 L=31	19,26,1		
323	ok,ok s=7,m=3			11.6	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.04	2d8/10 L=31	19,26,1
		15.5	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.04	2d8/10 L=31	19,26,30		
		19.4	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.04	2d8/10 L=31	19,26,30		
		23.3	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.04	2d8/10 L=31	19,26,30		
		27.1	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.04	2d8/10 L=31	22,26,30		
		31.0	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.04	2d8/10 L=31	22,26,30		
		0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.19	0.06	2d8/10 L=140	1,30,1		
		17.5	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.05	2d8/10 L=140	1,30,1		
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.05	2d8/10 L=140	1,30,1		
		52.5	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.04	2d8/10 L=140	19,30,1		
		70.0	0.38	7.7	7.7	0.0	0.13	0.01	0.18	0.03	2d8/10 L=140	19,30,46		
		87.5	0.38	7.7	7.7	0.0	0.13	0.02	0.18	0.03	2d8/10 L=140	42,30,46		
		105.0	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=140	42,30,46		
		122.5	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=140	46,30,46		
		140.0	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.01	2d8/10 L=140	46,26,46		
		0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	7.39e-03	2d8/10 L=52	39,30,46		
		6.5	0.38	7.7	7.7	0.0	0.13	0.02	0.16	8.45e-03	2d8/10 L=52	39,30,43		
		13.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	9.53e-03	2d8/10 L=52	39,30,43		
		19.5	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=52	39,26,43		
		342	ok,ok s=7,m=3	26.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=52	39,26,43
32.5	0.38			7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=52	39,26,1		
39.0	0.38			7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=52	39,26,1		
45.5	0.38			7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=52	39,26,1		
52.0	0.38			7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=52	39,26,1		
0.0	0.38			7.7	7.7	0.0	0.13	0.03	0.18	0.02	2d8/10 L=52	39,30,30		
6.5	0.38			7.7	7.7	0.0	0.13	0.03	0.18	0.01	2d8/10 L=52	39,30,30		
13.0	0.38			7.7	7.7	0.0	0.13	0.03	0.17	0.01	2d8/10 L=52	39,30,30		
19.5	0.38			7.7	7.7	0.0	0.13	0.03	0.17	0.01	2d8/10 L=52	39,30,30		
26.0	0.38			7.7	7.7	0.0	0.13	0.03	0.17	0.01	2d8/10 L=52	43,30,30		
32.5	0.38			7.7	7.7	0.0	0.13	0.03	0.17	9.21e-03	2d8/10 L=52	43,30,30		
39.0	0.38			7.7	7.7	0.0	0.13	0.03	0.17	7.98e-03	2d8/10 L=52	43,30,30		
45.5	0.38			7.7	7.7	0.0	0.13	0.03	0.17	6.76e-03	2d8/10 L=52	43,30,30		
52.0	0.38			7.7	7.7	0.0	0.13	0.04	0.17	7.00e-03	2d8/10 L=52	43,30,27		
						M_T= 96	Z=0.0	N=1242	N=1288					
Trave	Note			Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
324	ok,ok			0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.23	8.87e-03	2d8/10 L=42	5,46,46
	s=7,m=3			5.2	0.38	7.7	7.7	0.0	0.13	0.03	0.23	9.15e-03	2d8/10 L=42	5,46,43
				10.4	0.38	7.7	7.7	0.0	0.13	0.03	0.23	9.81e-03	2d8/10 L=42	5,46,43

		15.6	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=42	5,46,43
		20.8	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=42	5,46,43
		26.0	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=42	5,46,43
		31.3	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=42	5,46,43
		36.5	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=42	5,46,43
		41.7	0.38	7.7	7.7	0.0	0.13	0.03	0.22	0.01	2d8/10 L=42	5,46,43
408	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01	2d8/10 L=42	5,46,5
	s=7,m=3	5.2	0.38	7.7	7.7	0.0	0.13	0.03	0.22	9.86e-03	2d8/10 L=42	5,46,5
		10.4	0.38	7.7	7.7	0.0	0.13	0.02	0.22	8.57e-03	2d8/10 L=42	5,46,5
		15.6	0.38	7.7	7.7	0.0	0.13	0.02	0.22	7.28e-03	2d8/10 L=42	5,46,5
		20.8	0.38	7.7	7.7	0.0	0.13	0.02	0.22	5.99e-03	2d8/10 L=42	5,46,5
		26.0	0.38	7.7	7.7	0.0	0.13	0.02	0.22	4.69e-03	2d8/10 L=42	5,46,5
		31.3	0.38	7.7	7.7	0.0	0.13	0.02	0.22	3.84e-03	2d8/10 L=42	5,46,6
		36.5	0.38	7.7	7.7	0.0	0.13	0.02	0.22	4.62e-03	2d8/10 L=42	5,46,27
		41.7	0.38	7.7	7.7	0.0	0.13	0.02	0.22	5.77e-03	2d8/10 L=42	5,46,9
378	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.22	0.01	2d8/10 L=42	5,46,5
	s=7,m=3	5.2	0.38	7.7	7.7	0.0	0.13	0.02	0.21	0.01	2d8/10 L=42	5,46,5
		10.4	0.38	7.7	7.7	0.0	0.13	0.02	0.21	0.01	2d8/10 L=42	5,46,5
		15.6	0.38	7.7	7.7	0.0	0.13	0.01	0.21	9.99e-03	2d8/10 L=42	5,46,5
		20.8	0.38	7.7	7.7	0.0	0.13	0.01	0.21	8.66e-03	2d8/10 L=42	5,46,5
		26.0	0.38	7.7	7.7	0.0	0.13	0.01	0.21	7.32e-03	2d8/10 L=42	5,46,5
		31.2	0.38	7.7	7.7	0.0	0.13	0.01	0.21	5.98e-03	2d8/10 L=42	5,46,5
		36.5	0.38	7.7	7.7	0.0	0.13	9.74e-03	0.21	4.64e-03	2d8/10 L=42	5,46,5
		41.7	0.38	7.7	7.7	0.0	0.13	9.41e-03	0.21	3.29e-03	2d8/10 L=42	27,46,5
355	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	9.41e-03	0.19	0.01	2d8/10 L=56	27,46,5
	s=7,m=3	7.0	0.38	7.7	7.7	0.0	0.13	8.20e-03	0.19	0.01	2d8/10 L=56	30,46,5
		13.9	0.38	7.7	7.7	0.0	0.13	9.37e-03	0.19	0.01	2d8/10 L=56	30,46,5
		20.9	0.38	7.7	7.7	0.0	0.13	0.01	0.19	8.47e-03	2d8/10 L=56	30,46,5
		27.8	0.38	7.7	7.7	0.0	0.13	0.01	0.19	6.65e-03	2d8/10 L=56	46,46,5
		34.8	0.38	7.7	7.7	0.0	0.13	0.01	0.19	4.81e-03	2d8/10 L=56	46,46,5
		41.8	0.38	7.7	7.7	0.0	0.13	0.01	0.19	2.97e-03	2d8/10 L=56	46,46,5
		48.7	0.38	7.7	7.7	0.0	0.13	0.01	0.19	2.93e-03	2d8/10 L=56	46,46,27
		55.7	0.38	7.7	7.7	0.0	0.13	0.01	0.19	4.41e-03	2d8/10 L=56	46,46,27
502	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.17	7.61e-03	2d8/10 L=56	46,1,5
	s=7,m=3	7.0	0.38	7.7	7.7	0.0	0.13	0.01	0.17	5.75e-03	2d8/10 L=56	46,1,5
		13.9	0.38	7.7	7.7	0.0	0.13	0.01	0.17	4.27e-03	2d8/10 L=56	46,1,30
		20.9	0.38	7.7	7.7	0.0	0.13	0.01	0.17	3.04e-03	2d8/10 L=56	46,1,30
		27.8	0.38	7.7	7.7	0.0	0.13	0.01	0.17	2.42e-03	2d8/10 L=56	46,1,27
		34.8	0.38	7.7	7.7	0.0	0.13	0.01	0.17	3.78e-03	2d8/10 L=56	46,1,27
		41.7	0.38	7.7	7.7	0.0	0.13	0.01	0.17	5.18e-03	2d8/10 L=56	46,1,1
		48.7	0.38	7.7	7.7	0.0	0.13	0.01	0.17	7.34e-03	2d8/10 L=56	46,1,1
		55.7	0.38	7.7	7.7	0.0	0.13	8.73e-03	0.17	9.50e-03	2d8/10 L=56	46,1,1
487	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	8.74e-03	0.17	4.85e-03	2d8/10 L=56	46,1,30
	s=7,m=3	7.0	0.38	7.7	7.7	0.0	0.13	9.23e-03	0.17	3.73e-03	2d8/10 L=56	46,1,27
		13.9	0.38	7.7	7.7	0.0	0.13	9.41e-03	0.17	4.92e-03	2d8/10 L=56	46,1,27
		20.9	0.38	7.7	7.7	0.0	0.13	9.27e-03	0.17	6.13e-03	2d8/10 L=56	46,1,23
		27.8	0.38	7.7	7.7	0.0	0.13	8.81e-03	0.17	8.27e-03	2d8/10 L=56	46,1,1
		34.8	0.38	7.7	7.7	0.0	0.13	8.03e-03	0.18	0.01	2d8/10 L=56	46,1,1
		41.7	0.38	7.7	7.7	0.0	0.13	7.49e-03	0.18	0.01	2d8/10 L=56	27,1,1
		48.7	0.38	7.7	7.7	0.0	0.13	9.69e-03	0.18	0.01	2d8/10 L=56	27,1,1
		55.7	0.38	7.7	7.7	0.0	0.13	0.01	0.18	0.02	2d8/10 L=56	27,1,1
466	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.17	0.01	2d8/10 L=51	27,46,27
	s=7,m=3	6.4	0.38	7.7	7.7	0.0	0.13	0.02	0.17	0.02	2d8/10 L=51	27,46,27
		12.8	0.38	7.7	7.7	0.0	0.13	0.02	0.17	0.02	2d8/10 L=51	27,1,27
		19.2	0.38	7.7	7.7	0.0	0.13	0.02	0.18	0.02	2d8/10 L=51	27,1,27
		25.7	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.02	2d8/10 L=51	27,1,27
		32.1	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.02	2d8/10 L=51	27,1,27
		38.5	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.02	2d8/10 L=51	27,1,27
		44.9	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=51	27,1,27
		51.3	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=51	27,1,27
443	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.24	0.02	2d8/10 L=51	27,46,23
	s=7,m=3	6.4	0.38	7.7	7.7	0.0	0.13	0.05	0.24	0.02	2d8/10 L=51	27,46,23
		12.8	0.38	7.7	7.7	0.0	0.13	0.05	0.24	0.02	2d8/10 L=51	27,46,23
		19.3	0.38	7.7	7.7	0.0	0.13	0.06	0.24	0.02	2d8/10 L=51	27,46,23
		25.7	0.38	7.7	7.7	0.0	0.13	0.06	0.24	0.03	2d8/10 L=51	27,46,23
		32.1	0.38	7.7	7.7	0.0	0.13	0.07	0.23	0.03	2d8/10 L=51	23,46,23
		38.5	0.38	7.7	7.7	0.0	0.13	0.07	0.23	0.03	2d8/10 L=51	23,46,23
		44.9	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.03	2d8/10 L=51	23,46,23
		51.3	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.03	2d8/10 L=51	23,46,23
417	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.29	9.02e-03	2d8/10 L=17	23,46,26
	s=7,m=3	2.2	0.38	7.7	7.7	0.0	0.13	0.08	0.29	8.68e-03	2d8/10 L=17	23,46,26
		4.3	0.38	7.7	7.7	0.0	0.13	0.08	0.29	8.34e-03	2d8/10 L=17	23,46,26
		6.5	0.38	7.7	7.7	0.0	0.13	0.09	0.29	8.57e-03	2d8/10 L=17	23,46,23
		8.7	0.38	7.7	7.7	0.0	0.13	0.09	0.29	9.05e-03	2d8/10 L=17	23,46,23
		10.8	0.38	7.7	7.7	0.0	0.13	0.09	0.29	9.54e-03	2d8/10 L=17	23,46,23
		13.0	0.38	7.7	7.7	0.0	0.13	0.09	0.29	0.01	2d8/10 L=17	23,46,23

514	ok,ok s=7,m=3	15.2	0.38	7.7	7.7	0.0	0.13	0.09	0.29	0.01	2d8/10 L=17 23,46,23		
		17.3	0.38	7.7	7.7	0.0	0.13	0.09	0.29	0.01	2d8/10 L=17 23,46,23		
		0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.14	0.03	2d8/10 L=34 27,1,30		
		4.3	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.03	2d8/10 L=34 27,1,30		
		8.5	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.03	2d8/10 L=34 27,1,30		
		12.8	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.02	2d8/10 L=34 27,1,30		
		17.0	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.02	2d8/10 L=34 27,1,30		
		21.3	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.02	2d8/10 L=34 27,1,30		
		25.5	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.02	2d8/10 L=34 27,1,30		
		29.8	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.02	2d8/10 L=34 27,1,30		
393	ok,ok s=7,m=3	34.0	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.02	2d8/10 L=34 27,1,30		
		0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.14	0.04	2d8/10 L=184 27,1,30		
		23.0	0.38	7.7	7.7	0.0	0.13	0.14	0.13	0.04	2d8/10 L=184 27,1,30		
		46.0	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.03	2d8/10 L=184 27,1,30		
		69.0	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.02	2d8/10 L=184 27,1,30		
		92.0	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.02	2d8/10 L=184 30,43,30		
		115.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.02	2d8/10 L=184 27,43,27		
		138.0	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=184 27,43,27		
		161.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.03	2d8/10 L=184 27,43,27		
		184.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=184 1,43,27		
343	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=220 1,1,1		
		27.5	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.03	2d8/10 L=220 43,1,26		
		55.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.03	2d8/10 L=220 46,1,30		
		82.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.02	2d8/10 L=220 30,1,30		
		110.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=220 30,43,30		
		137.5	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.02	2d8/10 L=220 30,43,27		
		165.0	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=220 30,43,27		
		192.5	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=220 23,43,27		
		220.0	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.04	2d8/10 L=220 27,43,27		
M_T= 97 Z=0.0 N=435 N=441													
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb		
329	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.04	2d8/10 L=100 27,43,27		
		12.5	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.05	2d8/10 L=100 27,43,27		
		25.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.05	2d8/10 L=100 27,43,27		
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.05	2d8/10 L=100 27,43,27		
		50.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.05	2d8/10 L=100 27,43,27		
		62.5	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.05	2d8/10 L=100 1,43,27		
		75.0	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.06	2d8/10 L=100 1,43,27		
		87.5	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.06	2d8/10 L=100 1,43,27		
		100.0	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.06	2d8/10 L=100 1,43,27		
		0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.06	0.04	2d8/10 L=95 1,46,1		
358	ok,ok s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.04	2d8/10 L=95 5,46,1		
		23.8	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.03	2d8/10 L=95 27,46,1		
		35.6	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.03	2d8/10 L=95 27,46,1		
		47.5	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.02	2d8/10 L=95 27,46,30		
		59.4	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.02	2d8/10 L=95 27,46,30		
		71.3	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.02	2d8/10 L=95 27,46,30		
		83.1	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.01	2d8/10 L=95 27,46,30		
		95.0	0.38	7.7	7.7	0.0	0.13	0.11	0.05	0.01	2d8/10 L=95 27,43,30		
		0.0	0.38	7.7	7.7	0.0	0.13	0.24	0.08	0.08	2d8/10 L=410 27,30,1		
		51.3	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.06	2d8/10 L=410 30,30,1		
394	ok,ok s=7,m=3	102.5	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.05	2d8/10 L=410 30,30,30		
		153.8	0.38	7.7	7.7	0.0	0.13	0.14	0.05	0.04	2d8/10 L=410 1,30,30		
		205.0	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=410 1,27,30		
		256.3	0.38	7.7	7.7	0.0	0.13	0.15	0.05	0.03	2d8/10 L=410 1,27,27		
		307.5	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.04	2d8/10 L=410 30,27,27		
		358.8	0.38	7.7	7.7	0.0	0.13	0.14	0.07	0.05	2d8/10 L=410 30,27,1		
		410.0	0.38	7.7	7.7	0.0	0.13	0.19	0.07	0.08	2d8/10 L=410 27,19,1		
		0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.04	2d8/10 L=95 27,46,26		
		11.9	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.04	2d8/10 L=95 27,43,26		
		23.8	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=95 23,43,23		
430	ok,ok s=7,m=3	35.6	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.04	2d8/10 L=95 15,43,23		
		47.5	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04	2d8/10 L=95 31,43,23		
		59.4	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=95 35,43,23		
		71.3	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.05	2d8/10 L=95 35,43,23		
		83.1	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.05	2d8/10 L=95 35,43,23		
		95.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.06	2d8/10 L=95 35,43,23		
		M_T= 98 Z=0.0 N=34 N=1247											
		Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
		330	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.15	0.03	2d8/10 L=95 34,30,38
11.9	0.38			7.7	7.7	0.0	0.13	0.11	0.15	0.03	2d8/10 L=95 34,30,38		
23.8	0.38			7.7	7.7	0.0	0.13	0.10	0.15	0.03	2d8/10 L=95 34,30,38		
35.6	0.38			7.7	7.7	0.0	0.13	0.09	0.15	0.03	2d8/10 L=95 34,30,34		
47.5	0.38			7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=95 34,30,34		
59.4	0.38			7.7	7.7	0.0	0.13	0.07	0.14	0.03	2d8/10 L=95 34,30,31		
71.3	0.38			7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=95 34,30,35		

		83.1	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.03	2d8/10 L=95 38,30,35
		95.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.04	2d8/10 L=95 38,30,35
411	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=95 38,30,38
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.01	2d8/10 L=95 38,30,34
		23.8	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=95 38,30,34
		35.6	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=95 38,30,31
		47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=95 38,30,31
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=95 38,30,35
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.02	2d8/10 L=95 38,30,35
		83.1	0.38	7.7	7.7	0.0	0.13	9.02e-03	0.14	0.02	2d8/10 L=95 35,30,35
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.03	2d8/10 L=95 27,30,1
381	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.14	4.22e-03	2d8/10 L=53 27,30,22
	s=7,m=3	6.6	0.38	7.7	7.7	0.0	0.13	0.01	0.14	4.90e-03	2d8/10 L=53 27,30,15
		13.3	0.38	7.7	7.7	0.0	0.13	0.01	0.14	7.00e-03	2d8/10 L=53 27,30,1
		19.9	0.38	7.7	7.7	0.0	0.13	0.01	0.14	9.65e-03	2d8/10 L=53 27,30,1
		26.5	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.01	2d8/10 L=53 27,30,1
		33.1	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.01	2d8/10 L=53 1,30,1
		39.8	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=53 1,30,1
		46.4	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02	2d8/10 L=53 1,30,1
		53.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02	2d8/10 L=53 1,30,1
426	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	5.94e-03	2d8/10 L=42 1,30,22
	s=7,m=3	5.3	0.38	7.7	7.7	0.0	0.13	0.03	0.15	6.49e-03	2d8/10 L=42 1,30,19
		10.5	0.38	7.7	7.7	0.0	0.13	0.03	0.14	7.14e-03	2d8/10 L=42 1,30,19
		15.8	0.38	7.7	7.7	0.0	0.13	0.03	0.14	8.84e-03	2d8/10 L=42 1,22,1
		21.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=42 1,22,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=42 1,30,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.02	2d8/10 L=42 1,30,1
		36.8	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.02	2d8/10 L=42 1,30,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=42 1,30,1
359	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=35 1,30,30
	s=7,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=35 1,30,30
		8.8	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=35 1,22,30
		13.1	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=35 1,22,30
		17.5	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=35 1,22,27
		21.9	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=35 1,22,27
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=35 1,22,27
		30.6	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=35 1,22,27
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=35 1,22,27
347	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=60 1,31,1
	s=7,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.02	2d8/10 L=60 1,31,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01	2d8/10 L=60 35,31,46
		22.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01	2d8/10 L=60 35,31,46
		30.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01	2d8/10 L=60 35,31,46
		37.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01	2d8/10 L=60 35,31,30
		45.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01	2d8/10 L=60 35,31,27
		52.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01	2d8/10 L=60 1,31,27
		60.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02	2d8/10 L=60 23,31,27
501	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.03	2d8/10 L=95 23,31,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=95 23,31,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.02	2d8/10 L=95 23,31,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.01	2d8/10 L=95 23,31,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.10	8.37e-03	2d8/10 L=95 23,31,1
		59.4	0.38	7.7	7.7	0.0	0.13	0.01	0.10	4.32e-03	2d8/10 L=95 23,31,46
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.10	5.89e-03	2d8/10 L=95 23,31,35
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.11	8.59e-03	2d8/10 L=95 23,31,35
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.11	0.01	2d8/10 L=95 23,31,1
486	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.06	0.01	2d8/10 L=18 23,31,1
	s=7,m=3	2.3	0.38	7.7	7.7	0.0	0.13	0.01	0.06	0.01	2d8/10 L=18 23,31,1
		4.5	0.38	7.7	7.7	0.0	0.13	0.01	0.06	0.01	2d8/10 L=18 23,31,1
		6.8	0.38	7.7	7.7	0.0	0.13	0.01	0.06	9.11e-03	2d8/10 L=18 23,31,1
		9.0	0.38	7.7	7.7	0.0	0.13	0.01	0.06	8.11e-03	2d8/10 L=18 23,31,1
		11.3	0.38	7.7	7.7	0.0	0.13	9.99e-03	0.06	7.11e-03	2d8/10 L=18 23,31,1
		13.5	0.38	7.7	7.7	0.0	0.13	9.61e-03	0.06	6.12e-03	2d8/10 L=18 23,35,1
		15.8	0.38	7.7	7.7	0.0	0.13	9.26e-03	0.06	5.12e-03	2d8/10 L=18 23,31,1
		18.0	0.38	7.7	7.7	0.0	0.13	8.95e-03	0.06	4.12e-03	2d8/10 L=18 23,31,26
505	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	8.95e-03	0.05	0.02	2d8/10 L=77 23,35,1
	s=7,m=3	9.6	0.38	7.7	7.7	0.0	0.13	7.45e-03	0.05	0.02	2d8/10 L=77 38,35,1
		19.3	0.38	7.7	7.7	0.0	0.13	9.40e-03	0.05	0.01	2d8/10 L=77 38,35,1
		28.9	0.38	7.7	7.7	0.0	0.13	0.01	0.04	0.01	2d8/10 L=77 1,35,1
		38.5	0.38	7.7	7.7	0.0	0.13	0.01	0.04	6.33e-03	2d8/10 L=77 1,35,1
		48.1	0.38	7.7	7.7	0.0	0.13	0.02	0.04	2.16e-03	2d8/10 L=77 1,35,38
		57.8	0.38	7.7	7.7	0.0	0.13	0.02	0.04	3.41e-03	2d8/10 L=77 1,35,35
		67.4	0.38	7.7	7.7	0.0	0.13	0.01	0.05	6.67e-03	2d8/10 L=77 1,35,1
		77.0	0.38	7.7	7.7	0.0	0.13	0.01	0.05	0.01	2d8/10 L=77 1,35,1
465	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.05	0.02	2d8/10 L=95 1,43,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.02	2d8/10 L=95 1,43,1

		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.01	2d8/10 L=95	1,43,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.03	0.05	6.46e-03	2d8/10 L=95	1,43,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	1.17e-03	2d8/10 L=95	1,43,38
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.05	4.45e-03	2d8/10 L=95	1,43,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.05	9.93e-03	2d8/10 L=95	1,43,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.02	2d8/10 L=95	1,43,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.06	0.02	2d8/10 L=95	1,43,1
442	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=78	1,43,1
	s=7,m=3	9.8	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=78	1,43,1
		19.5	0.38	7.7	7.7	0.0	0.13	0.02	0.07	5.69e-03	2d8/10 L=78	1,43,1
		29.3	0.38	7.7	7.7	0.0	0.13	0.02	0.07	1.56e-03	2d8/10 L=78	1,43,22
		39.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	3.50e-03	2d8/10 L=78	1,43,1
		48.8	0.38	7.7	7.7	0.0	0.13	0.02	0.07	8.12e-03	2d8/10 L=78	1,43,1
		58.5	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=78	1,43,1
		68.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.02	2d8/10 L=78	1,43,1
		78.0	0.38	7.7	7.7	0.0	0.13	5.86e-03	0.07	0.02	2d8/10 L=78	1,43,1
475	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	5.86e-03	0.07	2.74e-03	2d8/10 L=17	1,15,18
	s=7,m=3	2.1	0.38	7.7	7.7	0.0	0.13	5.85e-03	0.07	2.18e-03	2d8/10 L=17	1,15,18
		4.3	0.38	7.7	7.7	0.0	0.13	5.77e-03	0.07	2.44e-03	2d8/10 L=17	1,15,15
		6.4	0.38	7.7	7.7	0.0	0.13	5.62e-03	0.07	2.90e-03	2d8/10 L=17	1,15,15
		8.5	0.38	7.7	7.7	0.0	0.13	5.40e-03	0.07	3.78e-03	2d8/10 L=17	1,15,1
		10.6	0.38	7.7	7.7	0.0	0.13	5.12e-03	0.07	4.80e-03	2d8/10 L=17	1,15,1
		12.8	0.38	7.7	7.7	0.0	0.13	4.77e-03	0.07	5.83e-03	2d8/10 L=17	1,15,1
		14.9	0.38	7.7	7.7	0.0	0.13	4.37e-03	0.07	6.85e-03	2d8/10 L=17	22,15,1
		17.0	0.38	7.7	7.7	0.0	0.13	4.25e-03	0.07	7.88e-03	2d8/10 L=17	22,15,1
415	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	4.25e-03	0.08	0.02	2d8/10 L=95	22,15,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.02	2d8/10 L=95	18,15,18
		23.8	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=95	18,15,18
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.08	8.51e-03	2d8/10 L=95	18,15,18
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.09	7.70e-03	2d8/10 L=95	18,15,19
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=95	18,15,19
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=95	18,15,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=95	18,15,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.03	2d8/10 L=95	15,15,1
388	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=95	15,15,22
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=95	15,15,22
		23.8	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.02	2d8/10 L=95	18,15,22
		35.6	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.02	2d8/10 L=95	18,15,22
		47.5	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.02	2d8/10 L=95	22,15,19
		59.4	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=95	19,15,39
		71.3	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.03	2d8/10 L=95	19,15,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.03	2d8/10 L=95	19,15,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.03	2d8/10 L=95	19,15,1
371	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.22	0.04	2d8/10 L=43	19,18,22
	s=7,m=3	5.4	0.38	7.7	7.7	0.0	0.13	0.14	0.22	0.04	2d8/10 L=43	19,18,22
		10.8	0.38	7.7	7.7	0.0	0.13	0.13	0.22	0.04	2d8/10 L=43	19,18,19
		16.1	0.38	7.7	7.7	0.0	0.13	0.12	0.22	0.04	2d8/10 L=43	19,18,19
		21.5	0.38	7.7	7.7	0.0	0.13	0.12	0.22	0.04	2d8/10 L=43	19,18,19
		26.9	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.05	2d8/10 L=43	19,18,19
		32.3	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.05	2d8/10 L=43	19,18,19
		37.6	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.05	2d8/10 L=43	19,18,19
		43.0	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.05	2d8/10 L=43	19,15,19
404	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.03	2d8/10 L=86	19,18,22
	s=7,m=3	10.7	0.38	7.7	7.7	0.0	0.13	0.08	0.22	0.03	2d8/10 L=86	19,18,22
		21.4	0.38	7.7	7.7	0.0	0.13	0.07	0.22	0.03	2d8/10 L=86	19,18,19
		32.1	0.38	7.7	7.7	0.0	0.13	0.06	0.22	0.04	2d8/10 L=86	19,18,19
		42.8	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.04	2d8/10 L=86	19,18,19
		53.5	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.04	2d8/10 L=86	19,15,19
		64.3	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.05	2d8/10 L=86	23,15,19
		75.0	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.05	2d8/10 L=86	1,15,19
		85.7	0.38	7.7	7.7	0.0	0.13	0.06	0.23	0.06	2d8/10 L=86	1,15,19
436	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.23	0.06	2d8/10 L=86	1,15,15
	s=7,m=3	10.7	0.38	7.7	7.7	0.0	0.13	0.06	0.23	0.06	2d8/10 L=86	1,15,15
		21.4	0.38	7.7	7.7	0.0	0.13	0.08	0.24	0.07	2d8/10 L=86	15,15,15
		32.1	0.38	7.7	7.7	0.0	0.13	0.10	0.24	0.07	2d8/10 L=86	15,15,15
		42.8	0.38	7.7	7.7	0.0	0.13	0.13	0.24	0.07	2d8/10 L=86	15,15,15
		53.5	0.38	7.7	7.7	0.0	0.13	0.15	0.25	0.08	2d8/10 L=86	15,15,15
		64.2	0.38	7.7	7.7	0.0	0.13	0.18	0.25	0.08	2d8/10 L=86	15,15,15
		75.0	0.38	7.7	7.7	0.0	0.13	0.21	0.25	0.09	2d8/10 L=86	15,15,15
		85.7	0.38	7.7	7.7	0.0	0.13	0.24	0.26	0.09	2d8/10 L=86	15,15,15
459	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.24	0.22	0.02	2d8/10 L=86	15,18,22
	s=7,m=3	10.7	0.38	7.7	7.7	0.0	0.13	0.24	0.22	0.02	2d8/10 L=86	19,18,19
		21.4	0.38	7.7	7.7	0.0	0.13	0.25	0.22	0.03	2d8/10 L=86	19,18,19
		32.1	0.38	7.7	7.7	0.0	0.13	0.26	0.22	0.03	2d8/10 L=86	19,18,19
		42.8	0.38	7.7	7.7	0.0	0.13	0.27	0.22	0.04	2d8/10 L=86	19,15,19
		53.5	0.38	7.7	7.7	0.0	0.13	0.29	0.22	0.04	2d8/10 L=86	19,15,19

		64.3	0.38	7.7	7.7	0.0	0.13	0.30	0.22	0.05	2d8/10 L=86 19,15,19
		75.0	0.38	7.7	7.7	0.0	0.13	0.32	0.23	0.05	2d8/10 L=86 19,15,19
		85.7	0.38	7.7	7.7	0.0	0.13	0.34	0.23	0.06	2d8/10 L=86 19,15,19
563	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.64	0.30	0.15	2d8/10 L=275 15,26,18
	s=7,m=3	34.4	0.38	7.7	7.7	0.0	0.13	0.49	0.29	0.13	2d8/10 L=275 15,26,18
		68.8	0.38	7.7	7.7	0.0	0.13	0.36	0.28	0.12	2d8/10 L=275 15,26,18
		103.1	0.38	7.7	7.7	0.0	0.13	0.25	0.27	0.10	2d8/10 L=275 15,26,18
		137.5	0.38	7.7	7.7	0.0	0.13	0.15	0.26	0.09	2d8/10 L=275 15,26,18
		171.9	0.38	7.7	7.7	0.0	0.13	0.07	0.25	0.07	2d8/10 L=275 19,26,18
		206.3	0.38	7.7	7.7	0.0	0.13	0.05	0.24	0.06	2d8/10 L=275 42,26,18
		240.6	0.38	7.7	7.7	0.0	0.13	0.09	0.24	0.05	2d8/10 L=275 42,23,18
		275.0	0.38	7.7	7.7	0.0	0.13	0.13	0.24	0.04	2d8/10 L=275 34,23,15
							M_T= 99	Z=0.0	N=678	N=1517	
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
335	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.07	0.06	2d8/10 L=814 1,1,1
	s=7,m=3	101.8	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.04	2d8/10 L=814 38,1,1
		203.6	0.38	7.7	7.7	0.0	0.13	0.10	0.04	0.02	2d8/10 L=814 1,1,1
		305.4	0.38	7.7	7.7	0.0	0.13	0.15	0.03	0.01	2d8/10 L=814 1,1,1
		407.3	0.38	7.7	7.7	0.0	0.13	0.17	0.03	6.52e-03	2d8/10 L=814 1,35,38
		509.1	0.38	7.7	7.7	0.0	0.13	0.15	0.03	0.02	2d8/10 L=814 1,35,35
		610.9	0.38	7.7	7.7	0.0	0.13	0.10	0.04	0.03	2d8/10 L=814 38,35,35
		712.7	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.05	2d8/10 L=814 35,1,35
		814.5	0.38	7.7	7.7	0.0	0.13	0.33	0.08	0.08	2d8/10 L=814 35,1,1
334	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.04	0.02	2d8/10 L=68 35,15,35
	s=7,m=3	8.5	0.38	7.7	7.7	0.0	0.13	0.16	0.04	0.02	2d8/10 L=68 35,15,35
		16.9	0.38	7.7	7.7	0.0	0.13	0.16	0.04	0.02	2d8/10 L=68 35,15,35
		25.4	0.38	7.7	7.7	0.0	0.13	0.16	0.04	0.03	2d8/10 L=68 35,15,35
		33.9	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=68 35,1,1
		42.3	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=68 35,1,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=68 35,1,1
		59.3	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.04	2d8/10 L=68 35,1,1
		67.8	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.04	2d8/10 L=68 35,1,1
384	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.09	0.10	2d8/10 L=68 35,32,38
	s=7,m=3	8.5	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.10	2d8/10 L=68 35,32,38
		16.9	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.10	2d8/10 L=68 1,32,38
		25.4	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.10	2d8/10 L=68 1,32,38
		33.9	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.10	2d8/10 L=68 1,32,38
		42.3	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.09	2d8/10 L=68 1,32,38
		50.8	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.09	2d8/10 L=68 1,32,38
		59.3	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.09	2d8/10 L=68 35,32,38
		67.8	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.09	2d8/10 L=68 35,32,38
362	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=64 38,23,35
	s=7,m=3	8.1	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.05	2d8/10 L=64 38,23,35
		16.1	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.05	2d8/10 L=64 38,23,35
		24.2	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.05	2d8/10 L=64 38,23,35
		32.3	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.05	2d8/10 L=64 38,23,35
		40.3	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.06	2d8/10 L=64 10,23,1
		48.4	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.06	2d8/10 L=64 1,23,1
		56.4	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.06	2d8/10 L=64 1,23,1
		64.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.07	2d8/10 L=64 1,23,1
396	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.01	2d8/10 L=118 1,23,35
	s=7,m=3	14.7	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=118 35,23,35
		29.4	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.02	2d8/10 L=118 35,23,35
		44.2	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=118 35,23,35
		58.9	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03	2d8/10 L=118 35,23,35
		73.6	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.03	2d8/10 L=118 35,23,31
		88.3	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.04	2d8/10 L=118 35,23,1
		103.0	0.38	7.7	7.7	0.0	0.13	0.14	0.07	0.04	2d8/10 L=118 35,23,1
		117.8	0.38	7.7	7.7	0.0	0.13	0.16	0.08	0.05	2d8/10 L=118 35,23,1
350	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.03	2d8/10 L=118 31,23,1
	s=7,m=3	14.7	0.38	7.7	7.7	0.0	0.13	0.15	0.05	0.02	2d8/10 L=118 35,23,1
		29.4	0.38	7.7	7.7	0.0	0.13	0.14	0.04	0.02	2d8/10 L=118 35,23,1
		44.2	0.38	7.7	7.7	0.0	0.13	0.14	0.04	0.01	2d8/10 L=118 35,23,1
		58.9	0.38	7.7	7.7	0.0	0.13	0.14	0.04	5.58e-03	2d8/10 L=118 35,23,38
		73.6	0.38	7.7	7.7	0.0	0.13	0.14	0.04	4.07e-03	2d8/10 L=118 35,23,35
		88.3	0.38	7.7	7.7	0.0	0.13	0.14	0.04	8.50e-03	2d8/10 L=118 35,23,35
		103.0	0.38	7.7	7.7	0.0	0.13	0.15	0.04	0.01	2d8/10 L=118 35,23,1
		117.8	0.38	7.7	7.7	0.0	0.13	0.15	0.05	0.02	2d8/10 L=118 35,23,1
331	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.41	0.08	0.11	2d8/10 L=275 35,36,38
	s=7,m=3	34.4	0.38	7.7	7.7	0.0	0.13	0.30	0.08	0.09	2d8/10 L=275 35,36,38
		68.8	0.38	7.7	7.7	0.0	0.13	0.21	0.07	0.08	2d8/10 L=275 35,36,38
		103.1	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.07	2d8/10 L=275 35,36,38
		137.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.06	2d8/10 L=275 35,36,38
		171.9	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.05	2d8/10 L=275 46,36,38
		206.3	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.04	2d8/10 L=275 38,36,38
		240.6	0.38	7.7	7.7	0.0	0.13	0.10	0.04	0.04	2d8/10 L=275 38,31,35

		275.0	0.38	7.7	7.7	0.0	0.13	0.13	0.05	0.04	2d8/10 L=275 38,35,35
							M_T= 100	Z=0.0	N=17	N=1683	
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
332	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.12	0.04	2d8/10 L=87 31,19,34
	s=7,m=3	10.9	0.38	7.7	7.7	0.0	0.13	0.11	0.12	0.04	2d8/10 L=87 34,19,34
		21.8	0.38	7.7	7.7	0.0	0.13	0.11	0.12	0.04	2d8/10 L=87 34,19,34
		32.6	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.04	2d8/10 L=87 34,19,34
		43.5	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.04	2d8/10 L=87 34,19,34
		54.4	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.03	2d8/10 L=87 34,19,34
		65.3	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=87 38,27,31
		76.1	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.04	2d8/10 L=87 38,27,31
		87.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.04	2d8/10 L=87 38,27,35
412	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.03	2d8/10 L=140 34,19,34
	s=7,m=3	17.5	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.03	2d8/10 L=140 34,19,34
		35.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=140 34,19,34
		52.5	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=140 34,19,31
		70.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.04	2d8/10 L=140 38,19,31
		87.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=140 42,19,31
		105.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.05	2d8/10 L=140 22,19,31
		122.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.05	2d8/10 L=140 31,19,31
		140.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.05	2d8/10 L=140 31,19,31
382	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=58 27,19,35
	s=7,m=3	7.3	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=58 19,19,35
		14.5	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=58 19,19,31
		21.8	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.03	2d8/10 L=58 19,19,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.03	2d8/10 L=58 19,19,1
		36.3	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.03	2d8/10 L=58 1,19,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.03	2d8/10 L=58 1,19,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.04	2d8/10 L=58 1,19,1
		58.0	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.04	2d8/10 L=58 1,19,1
447	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.02	2d8/10 L=35 1,15,23
	s=7,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.02	2d8/10 L=35 1,15,23
		8.8	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=35 1,15,23
		13.1	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=35 1,15,23
		17.5	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=35 1,15,23
		21.9	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=35 1,15,23
		26.3	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=35 1,15,23
		30.6	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=35 1,15,23
		35.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=35 1,15,23
427	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.17	0.02	2d8/10 L=60 1,26,1
	s=7,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.02	2d8/10 L=60 1,26,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.02	2d8/10 L=60 1,26,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.02	2d8/10 L=60 1,26,26
		30.0	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.01	2d8/10 L=60 1,26,26
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.01	2d8/10 L=60 1,26,26
		45.0	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.01	2d8/10 L=60 1,26,26
		52.5	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.01	2d8/10 L=60 1,26,23
		60.0	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.01	2d8/10 L=60 1,26,23
489	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=47 1,26,1
	s=7,m=3	5.9	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=47 1,26,1
		11.8	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=47 1,26,1
		17.6	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=47 1,26,1
		23.5	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.01	2d8/10 L=47 1,26,1
		29.4	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.01	2d8/10 L=47 1,26,1
		35.3	0.38	7.7	7.7	0.0	0.13	0.04	0.16	7.73e-03	2d8/10 L=47 1,26,1
		41.1	0.38	7.7	7.7	0.0	0.13	0.04	0.16	5.20e-03	2d8/10 L=47 1,26,1
		47.0	0.38	7.7	7.7	0.0	0.13	0.04	0.16	4.37e-03	2d8/10 L=47 1,26,19
507	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=48 1,26,1
	s=7,m=3	6.0	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=48 1,26,1
		12.0	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.02	2d8/10 L=48 1,26,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=48 1,26,1
		24.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=48 1,26,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	9.45e-03	2d8/10 L=48 1,26,1
		36.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	6.84e-03	2d8/10 L=48 35,26,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	5.16e-03	2d8/10 L=48 35,26,18
		48.0	0.38	7.7	7.7	0.0	0.13	0.02	0.16	4.50e-03	2d8/10 L=48 35,26,15
469	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.03	2d8/10 L=95 35,26,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=95 35,26,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=95 31,26,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.01	2d8/10 L=95 34,26,34
		47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.01	2d8/10 L=95 34,26,34
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.11	7.69e-03	2d8/10 L=95 34,26,34
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.11	9.00e-03	2d8/10 L=95 34,26,31
		83.1	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=95 34,26,31
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=95 34,26,31
454	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41 34,18,1

	s=7,m=3	5.2	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41	34,18,1
		10.4	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=41	34,18,1
		15.6	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=41	34,18,34
		20.8	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=41	34,18,34
		25.9	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=41	34,18,34
		31.1	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	34,18,34
		36.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	34,18,34
		41.5	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	34,18,34
360	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.12	0.05	2d8/10 L=210	34,34,34
		26.3	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.04	2d8/10 L=210	34,34,34
		52.6	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.04	2d8/10 L=210	34,34,34
		78.9	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.03	2d8/10 L=210	1,34,34
		105.3	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.03	2d8/10 L=210	1,34,31
		131.6	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.04	2d8/10 L=210	34,34,31
		157.9	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.04	2d8/10 L=210	34,34,31
		184.2	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05	2d8/10 L=210	31,34,31
		210.5	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.06	2d8/10 L=210	31,34,1
348	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.03	2d8/10 L=33	15,34,1
		4.1	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.03	2d8/10 L=33	15,34,1
		8.3	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.04	2d8/10 L=33	15,34,1
		12.4	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.04	2d8/10 L=33	15,34,1
		16.5	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.04	2d8/10 L=33	15,34,1
		20.6	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.04	2d8/10 L=33	15,34,1
		24.8	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.04	2d8/10 L=33	19,34,1
		28.9	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.05	2d8/10 L=33	19,34,1
		33.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.05	2d8/10 L=33	1,34,1
389	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.07	2d8/10 L=95	1,38,38
		11.9	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.07	2d8/10 L=95	19,38,38
		23.8	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.07	2d8/10 L=95	15,38,38
		35.6	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.07	2d8/10 L=95	15,38,38
		47.5	0.38	7.7	7.7	0.0	0.13	0.09	0.19	0.06	2d8/10 L=95	15,38,38
		59.4	0.38	7.7	7.7	0.0	0.13	0.11	0.18	0.06	2d8/10 L=95	18,38,38
		71.3	0.38	7.7	7.7	0.0	0.13	0.12	0.18	0.06	2d8/10 L=95	18,38,38
		83.1	0.38	7.7	7.7	0.0	0.13	0.14	0.18	0.06	2d8/10 L=95	38,38,38
		95.0	0.38	7.7	7.7	0.0	0.13	0.16	0.18	0.05	2d8/10 L=95	38,38,38
372	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.20	0.29	0.06	2d8/10 L=300	26,18,18
		37.5	0.38	7.7	7.7	0.0	0.13	0.16	0.28	0.05	2d8/10 L=300	26,18,18
		75.0	0.38	7.7	7.7	0.0	0.13	0.11	0.28	0.05	2d8/10 L=300	26,18,15
		112.5	0.38	7.7	7.7	0.0	0.13	0.04	0.27	0.07	2d8/10 L=300	26,18,15
		150.0	0.38	7.7	7.7	0.0	0.13	0.06	0.27	0.08	2d8/10 L=300	19,18,15
		187.5	0.38	7.7	7.7	0.0	0.13	0.16	0.27	0.09	2d8/10 L=300	19,15,15
		225.0	0.38	7.7	7.7	0.0	0.13	0.27	0.28	0.11	2d8/10 L=300	19,15,15
		262.5	0.38	7.7	7.7	0.0	0.13	0.40	0.29	0.12	2d8/10 L=300	15,15,15
		300.0	0.38	7.7	7.7	0.0	0.13	0.55	0.30	0.14	2d8/10 L=300	15,15,15
337	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.54	0.27	0.13	2d8/10 L=275	15,22,22
		34.4	0.38	7.7	7.7	0.0	0.13	0.42	0.26	0.11	2d8/10 L=275	15,22,22
		68.8	0.38	7.7	7.7	0.0	0.13	0.31	0.26	0.10	2d8/10 L=275	15,19,22
		103.1	0.38	7.7	7.7	0.0	0.13	0.21	0.26	0.08	2d8/10 L=275	15,19,22
		137.5	0.38	7.7	7.7	0.0	0.13	0.14	0.26	0.07	2d8/10 L=275	15,19,22
		171.9	0.38	7.7	7.7	0.0	0.13	0.07	0.27	0.06	2d8/10 L=275	39,19,22
		206.3	0.38	7.7	7.7	0.0	0.13	0.06	0.27	0.05	2d8/10 L=275	39,19,22
		240.6	0.38	7.7	7.7	0.0	0.13	0.07	0.27	0.04	2d8/10 L=275	39,19,22
		275.0	0.38	7.7	7.7	0.0	0.13	0.10	0.27	0.03	2d8/10 L=275	42,19,22
M_T= 101 Z=0.0 N=26 N=1642												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
333	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.01	2d8/10 L=87	1,30,1
		10.9	0.38	7.7	7.7	0.0	0.13	0.04	0.11	9.87e-03	2d8/10 L=87	1,30,1
		21.8	0.38	7.7	7.7	0.0	0.13	0.04	0.11	7.15e-03	2d8/10 L=87	1,30,2
		32.6	0.38	7.7	7.7	0.0	0.13	0.04	0.11	4.49e-03	2d8/10 L=87	1,30,2
		43.5	0.38	7.7	7.7	0.0	0.13	0.04	0.11	5.30e-03	2d8/10 L=87	1,30,39
		54.4	0.38	7.7	7.7	0.0	0.13	0.04	0.11	6.39e-03	2d8/10 L=87	1,30,19
		65.3	0.38	7.7	7.7	0.0	0.13	0.04	0.11	8.20e-03	2d8/10 L=87	1,30,15
		76.1	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.01	2d8/10 L=87	1,30,15
		87.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=87	1,30,1
485	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.02	2d8/10 L=140	38,26,38
		17.5	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.02	2d8/10 L=140	1,26,38
		35.0	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.02	2d8/10 L=140	1,26,35
		52.5	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.03	2d8/10 L=140	1,26,35
		70.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.03	2d8/10 L=140	1,26,35
		87.5	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.03	2d8/10 L=140	1,23,35
		105.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.04	2d8/10 L=140	38,23,35
		122.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.04	2d8/10 L=140	38,23,35
		140.0	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.04	2d8/10 L=140	35,23,1
464	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.11	0.02	2d8/10 L=58	26,23,1
		7.3	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=58	23,23,1
		14.5	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.03	2d8/10 L=58	23,23,1

		21.8	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.03	2d8/10 L=58	23,23,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.03	2d8/10 L=58	23,23,1
		36.3	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.03	2d8/10 L=58	23,23,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.04	2d8/10 L=58	23,23,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.04	2d8/10 L=58	1,23,1
		58.0	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.04	2d8/10 L=58	1,23,1
441	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=35	1,26,43
	s=7,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=35	1,26,43
		8.8	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=35	1,23,43
		13.1	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=35	1,23,43
		17.5	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=35	1,23,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=35	1,23,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=35	1,23,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.02	2d8/10 L=35	1,23,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.03	2d8/10 L=35	1,23,1
474	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.03	2d8/10 L=60	1,23,1
	s=7,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=60	1,23,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=60	1,35,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=60	1,35,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.01	2d8/10 L=60	1,35,38
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.01	2d8/10 L=60	1,35,38
		45.0	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.01	2d8/10 L=60	1,35,38
		52.5	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.01	2d8/10 L=60	1,35,38
		60.0	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.01	2d8/10 L=60	1,35,35
413	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.02	2d8/10 L=47	1,23,1
	s=7,m=3	5.9	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.02	2d8/10 L=47	1,23,1
		11.8	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.02	2d8/10 L=47	1,23,1
		17.6	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.01	2d8/10 L=47	1,23,1
		23.5	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.01	2d8/10 L=47	1,23,1
		29.4	0.38	7.7	7.7	0.0	0.13	0.04	0.08	9.27e-03	2d8/10 L=47	1,23,1
		35.3	0.38	7.7	7.7	0.0	0.13	0.04	0.08	7.65e-03	2d8/10 L=47	1,23,38
		41.1	0.38	7.7	7.7	0.0	0.13	0.04	0.08	6.53e-03	2d8/10 L=47	1,23,38
		47.0	0.38	7.7	7.7	0.0	0.13	0.04	0.08	6.62e-03	2d8/10 L=47	1,23,35
450	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.02	2d8/10 L=48	1,23,1
	s=7,m=3	6.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=48	1,23,1
		12.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=48	1,23,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=48	1,23,1
		24.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	9.91e-03	2d8/10 L=48	1,23,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	7.42e-03	2d8/10 L=48	1,23,1
		36.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	5.53e-03	2d8/10 L=48	1,23,38
		42.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	4.55e-03	2d8/10 L=48	35,23,35
		48.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	5.61e-03	2d8/10 L=48	35,23,35
383	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.03	2d8/10 L=95	35,27,1
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=95	35,27,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=95	35,27,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=95	35,27,38
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.06	8.09e-03	2d8/10 L=95	38,23,38
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.06	6.54e-03	2d8/10 L=95	38,23,31
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.07	9.03e-03	2d8/10 L=95	35,23,31
		83.1	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=95	35,23,31
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=95	35,23,1
361	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41	35,24,1
	s=7,m=3	5.2	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41	35,24,1
		10.4	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41	38,24,1
		15.6	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41	38,24,1
		20.8	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.03	2d8/10 L=41	38,24,1
		25.9	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	38,24,1
		31.1	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	38,24,34
		36.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	38,24,34
		41.5	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=41	38,24,34
418	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.05	2d8/10 L=210	38,20,34
	s=7,m=3	26.3	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.04	2d8/10 L=210	38,20,34
		52.6	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.04	2d8/10 L=210	38,20,34
		78.9	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.03	2d8/10 L=210	1,15,34
		105.3	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.02	2d8/10 L=210	1,15,34
		131.6	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.03	2d8/10 L=210	1,15,35
		157.9	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.03	2d8/10 L=210	34,15,35
		184.2	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.04	2d8/10 L=210	34,15,35
		210.5	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05	2d8/10 L=210	34,15,1
395	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=33	42,15,2
	s=7,m=3	4.1	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=33	42,15,2
		8.3	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=33	42,15,1
		12.4	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=33	2,15,1
		16.5	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=33	2,15,1
		20.6	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=33	2,15,1
		24.8	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.02	2d8/10 L=33	2,15,1

		28.9	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.03	2d8/10 L=33	2,15,1
		33.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.03	2d8/10 L=33	2,15,1
349	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.06	2d8/10 L=95	2,15,1
		11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.06	2d8/10 L=95	42,15,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.05	2d8/10 L=95	42,15,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.05	2d8/10 L=95	42,15,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=95	42,15,1
		59.4	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=95	34,15,34
		71.3	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.03	2d8/10 L=95	34,15,34
		83.1	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.03	2d8/10 L=95	34,15,34
		95.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.02	2d8/10 L=95	34,15,34
373	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.28	0.06	0.04	2d8/10 L=300	34,1,31
		37.5	0.38	7.7	7.7	0.0	0.13	0.23	0.07	0.05	2d8/10 L=300	34,1,31
		75.0	0.38	7.7	7.7	0.0	0.13	0.16	0.09	0.06	2d8/10 L=300	38,1,1
		112.5	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.09	2d8/10 L=300	38,1,1
		150.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.11	2d8/10 L=300	43,1,1
		187.5	0.38	7.7	7.7	0.0	0.13	0.20	0.14	0.13	2d8/10 L=300	1,1,1
		225.0	0.38	7.7	7.7	0.0	0.13	0.37	0.15	0.16	2d8/10 L=300	1,1,1
		262.5	0.38	7.7	7.7	0.0	0.13	0.57	0.17	0.19	2d8/10 L=300	1,1,1
		300.0	0.38	7.7	7.7	0.0	0.13	0.80	0.19	0.21	2d8/10 L=300	1,1,1
338	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.80	0.18	0.19	2d8/10 L=275	1,1,1
		34.4	0.38	7.7	7.7	0.0	0.13	0.61	0.16	0.17	2d8/10 L=275	1,1,1
		68.8	0.38	7.7	7.7	0.0	0.13	0.44	0.14	0.15	2d8/10 L=275	1,1,1
		103.1	0.38	7.7	7.7	0.0	0.13	0.30	0.13	0.12	2d8/10 L=275	1,1,1
		137.5	0.38	7.7	7.7	0.0	0.13	0.17	0.12	0.10	2d8/10 L=275	1,1,1
		171.9	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.09	2d8/10 L=275	31,1,1
		206.3	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.07	2d8/10 L=275	34,1,1
		240.6	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.05	2d8/10 L=275	1,26,1
		275.0	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.04	2d8/10 L=275	1,26,1
M_T= 102 Z=0.0 N=1039 N=1319												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb	
336	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.21	0.22	0.08	2d8/10 L=64	23,43,23
		8.0	0.38	7.7	7.7	0.0	0.13	0.20	0.22	0.08	2d8/10 L=64	23,43,27
		16.1	0.38	7.7	7.7	0.0	0.13	0.18	0.22	0.08	2d8/10 L=64	23,43,27
		24.1	0.38	7.7	7.7	0.0	0.13	0.17	0.23	0.08	2d8/10 L=64	23,43,27
		32.2	0.38	7.7	7.7	0.0	0.13	0.17	0.23	0.08	2d8/10 L=64	23,43,27
		40.2	0.38	7.7	7.7	0.0	0.13	0.16	0.23	0.08	2d8/10 L=64	23,43,27
		48.2	0.38	7.7	7.7	0.0	0.13	0.15	0.23	0.09	2d8/10 L=64	23,43,27
		56.3	0.38	7.7	7.7	0.0	0.13	0.14	0.23	0.09	2d8/10 L=64	23,43,27
		64.3	0.38	7.7	7.7	0.0	0.13	0.14	0.23	0.09	2d8/10 L=64	15,43,27
385	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.20	0.05	2d8/10 L=64	15,46,26
		8.0	0.38	7.7	7.7	0.0	0.13	0.12	0.20	0.05	2d8/10 L=64	15,46,26
		16.1	0.38	7.7	7.7	0.0	0.13	0.11	0.20	0.04	2d8/10 L=64	15,46,26
		24.1	0.38	7.7	7.7	0.0	0.13	0.10	0.20	0.04	2d8/10 L=64	15,46,26
		32.2	0.38	7.7	7.7	0.0	0.13	0.09	0.20	0.04	2d8/10 L=64	15,43,26
		40.2	0.38	7.7	7.7	0.0	0.13	0.08	0.20	0.04	2d8/10 L=64	15,43,23
		48.3	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.04	2d8/10 L=64	15,43,23
		56.3	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.04	2d8/10 L=64	15,43,23
		64.3	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.04	2d8/10 L=64	1,43,23
363	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.03	2d8/10 L=64	1,46,18
		8.0	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.03	2d8/10 L=64	1,46,18
		16.1	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=64	1,46,18
		24.1	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=64	1,46,18
		32.2	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=64	1,46,18
		40.2	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=64	1,46,18
		48.2	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.01	2d8/10 L=64	1,46,18
		56.3	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.01	2d8/10 L=64	1,43,15
		64.3	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=64	1,43,15
351	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.03	2d8/10 L=67	1,46,1
		8.3	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=67	1,46,1
		16.7	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.02	2d8/10 L=67	1,46,1
		25.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.01	2d8/10 L=67	1,46,1
		33.3	0.38	7.7	7.7	0.0	0.13	0.03	0.14	9.25e-03	2d8/10 L=67	1,46,18
		41.7	0.38	7.7	7.7	0.0	0.13	0.02	0.14	6.46e-03	2d8/10 L=67	1,46,18
		50.0	0.38	7.7	7.7	0.0	0.13	0.02	0.14	4.71e-03	2d8/10 L=67	1,46,15
		58.3	0.38	7.7	7.7	0.0	0.13	0.02	0.14	6.84e-03	2d8/10 L=67	1,46,15
		66.7	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.01	2d8/10 L=67	1,46,1
416	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=67	1,46,1
		8.3	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=67	1,46,1
		16.7	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.01	2d8/10 L=67	15,46,18
		25.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.01	2d8/10 L=67	15,46,18
		33.3	0.38	7.7	7.7	0.0	0.13	0.02	0.11	7.10e-03	2d8/10 L=67	15,46,18
		41.7	0.38	7.7	7.7	0.0	0.13	0.02	0.11	5.87e-03	2d8/10 L=67	15,46,15
		50.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	7.63e-03	2d8/10 L=67	15,46,15
		58.3	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=67	19,46,1
		66.7	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=67	19,46,1

390	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=67	19,46,1		
		8.3	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.01	2d8/10 L=67	19,46,22		
		16.7	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.01	2d8/10 L=67	19,46,22		
		25.0	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.01	2d8/10 L=67	19,46,22		
		33.3	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.01	2d8/10 L=67	27,46,19		
		41.7	0.38	7.7	7.7	0.0	0.13	0.01	0.04	0.01	2d8/10 L=67	27,46,19		
		50.0	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.02	2d8/10 L=67	27,46,19		
		58.3	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.02	2d8/10 L=67	27,43,19		
	374	ok,ok s=7,m=3	66.7	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.03	2d8/10 L=67	19,43,19	
			0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.06	2d8/10 L=65	19,26,18	
			8.2	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.06	2d8/10 L=65	19,26,18	
			16.3	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.05	2d8/10 L=65	19,26,18	
			24.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.05	2d8/10 L=65	19,26,18	
			32.7	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.05	2d8/10 L=65	19,26,18	
			40.8	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.06	2d8/10 L=65	19,26,15	
			49.0	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.06	2d8/10 L=65	19,26,15	
445	ok,ok s=7,m=3	57.2	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.06	2d8/10 L=65	15,23,15		
		65.3	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.07	2d8/10 L=65	15,23,15		
		0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.12	0.11	2d8/10 L=65	15,26,18		
		8.2	0.38	7.7	7.7	0.0	0.13	0.15	0.12	0.11	2d8/10 L=65	15,26,18		
		16.3	0.38	7.7	7.7	0.0	0.13	0.17	0.12	0.11	2d8/10 L=65	15,26,18		
		24.5	0.38	7.7	7.7	0.0	0.13	0.20	0.12	0.11	2d8/10 L=65	15,26,18		
		32.7	0.38	7.7	7.7	0.0	0.13	0.22	0.12	0.11	2d8/10 L=65	15,26,18		
		40.8	0.38	7.7	7.7	0.0	0.13	0.25	0.12	0.11	2d8/10 L=65	18,26,18		
		49.0	0.38	7.7	7.7	0.0	0.13	0.28	0.12	0.11	2d8/10 L=65	18,26,15		
		57.2	0.38	7.7	7.7	0.0	0.13	0.30	0.12	0.11	2d8/10 L=65	18,26,15		
422	ok,ok s=7,m=3	65.3	0.38	7.7	7.7	0.0	0.13	0.33	0.12	0.12	2d8/10 L=65	18,26,15		
		0.0	0.38	7.7	7.7	0.0	0.13	0.34	0.17	0.05	2d8/10 L=65	18,46,22		
		8.2	0.38	7.7	7.7	0.0	0.13	0.33	0.17	0.05	2d8/10 L=65	18,46,22		
		16.3	0.38	7.7	7.7	0.0	0.13	0.33	0.16	0.04	2d8/10 L=65	18,46,22		
		24.5	0.38	7.7	7.7	0.0	0.13	0.33	0.16	0.04	2d8/10 L=65	18,46,22		
		32.7	0.38	7.7	7.7	0.0	0.13	0.33	0.16	0.03	2d8/10 L=65	18,46,22		
		40.8	0.38	7.7	7.7	0.0	0.13	0.33	0.16	0.03	2d8/10 L=65	18,46,22		
		49.0	0.38	7.7	7.7	0.0	0.13	0.33	0.15	0.02	2d8/10 L=65	18,46,22		
		57.2	0.38	7.7	7.7	0.0	0.13	0.33	0.15	0.02	2d8/10 L=65	18,46,22		
		65.3	0.38	7.7	7.7	0.0	0.13	0.33	0.15	0.01	2d8/10 L=65	18,46,22		
405	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.88	0.22	0.19	2d8/10 L=261	18,42,18		
		32.6	0.38	7.7	7.7	0.0	0.13	0.73	0.22	0.17	2d8/10 L=261	18,42,18		
		65.3	0.38	7.7	7.7	0.0	0.13	0.59	0.21	0.15	2d8/10 L=261	18,42,18		
		97.9	0.38	7.7	7.7	0.0	0.13	0.44	0.20	0.13	2d8/10 L=261	18,46,18		
		130.5	0.38	7.7	7.7	0.0	0.13	0.30	0.19	0.13	2d8/10 L=261	18,43,15		
		163.1	0.38	7.7	7.7	0.0	0.13	0.15	0.20	0.13	2d8/10 L=261	26,43,15		
		195.8	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.13	2d8/10 L=261	18,43,15		
		228.4	0.38	7.7	7.7	0.0	0.13	0.15	0.21	0.14	2d8/10 L=261	18,43,15		
		261.0	0.38	7.7	7.7	0.0	0.13	0.25	0.21	0.14	2d8/10 L=261	15,43,15		
		M_T= 103 Z=0.0 P=5 P=6												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb		
344	ok,ok s=7,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.31	0.04	0.05	2d8/10 L=332	42,44,42		
		41.5	0.38	7.7	7.7	0.0	0.13	0.29	0.03	0.03	2d8/10 L=332	46,44,42		
		83.0	0.38	7.7	7.7	0.0	0.13	0.26	0.03	0.03	2d8/10 L=332	42,27,39		
		124.5	0.38	7.7	7.7	0.0	0.13	0.21	0.04	0.04	2d8/10 L=332	42,27,39		
		166.0	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.06	2d8/10 L=332	42,1,1		
		207.5	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.09	2d8/10 L=332	39,1,1		
		249.0	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.12	2d8/10 L=332	39,1,1		
		290.5	0.38	7.7	7.7	0.0	0.13	0.31	0.11	0.15	2d8/10 L=332	1,1,1		
		332.0	0.38	7.7	7.7	0.0	0.13	0.53	0.13	0.18	2d8/10 L=332	1,1,1		
		0.0	0.38	7.7	7.7	0.0	0.13	0.53	0.08	0.10	2d8/10 L=243	1,1,1		
529	ok,ok s=7,m=3	30.4	0.38	7.7	7.7	0.0	0.13	0.44	0.06	0.08	2d8/10 L=243	1,1,1		
		60.8	0.38	7.7	7.7	0.0	0.13	0.38	0.04	0.05	2d8/10 L=243	1,1,1		
		91.1	0.38	7.7	7.7	0.0	0.13	0.34	0.03	0.03	2d8/10 L=243	1,1,1		
		121.5	0.38	7.7	7.7	0.0	0.13	0.33	0.02	0.01	2d8/10 L=243	1,27,46		
		151.9	0.38	7.7	7.7	0.0	0.13	0.33	0.03	0.02	2d8/10 L=243	1,27,1		
		182.3	0.38	7.7	7.7	0.0	0.13	0.37	0.04	0.05	2d8/10 L=243	1,1,1		
		212.6	0.38	7.7	7.7	0.0	0.13	0.42	0.05	0.07	2d8/10 L=243	1,1,1		
		243.0	0.38	7.7	7.7	0.0	0.13	0.50	0.07	0.09	2d8/10 L=243	1,1,1		
		0.0	0.38	7.7	7.7	0.0	0.13	0.50	0.12	0.17	2d8/10 L=275	1,1,1		
		34.4	0.38	7.7	7.7	0.0	0.13	0.33	0.10	0.14	2d8/10 L=275	1,1,1		
530	ok,ok s=7,m=3	68.8	0.38	7.7	7.7	0.0	0.13	0.20	0.09	0.12	2d8/10 L=275	1,1,1		
		103.1	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.10	2d8/10 L=275	39,1,1		
		137.5	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.08	2d8/10 L=275	42,1,1		
		171.9	0.38	7.7	7.7	0.0	0.13	0.16	0.05	0.06	2d8/10 L=275	46,1,1		
		206.3	0.38	7.7	7.7	0.0	0.13	0.20	0.04	0.04	2d8/10 L=275	46,1,1		
		240.6	0.38	7.7	7.7	0.0	0.13	0.23	0.03	0.03	2d8/10 L=275	46,30,1		
		275.0	0.38	7.7	7.7	0.0	0.13	0.26	0.03	0.02	2d8/10 L=275	46,30,46		
		M_T= 105 Z=0.0 N=17 N=34												
		Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb

352	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.03	2d8/10 L=85 27,38,26
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=85 27,38,26
		21.3	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=85 27,38,27
		31.9	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.03	2d8/10 L=85 27,38,27
		42.5	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.03	2d8/10 L=85 27,38,27
		53.1	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.03	2d8/10 L=85 27,38,27
		63.8	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.03	2d8/10 L=85 27,35,27
		74.4	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.03	2d8/10 L=85 27,35,27
		85.0	0.38	7.7	7.7	0.0	0.13	0.08	0.17	0.03	2d8/10 L=85 1,35,27
391	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.03	2d8/10 L=85 1,38,1
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.03	2d8/10 L=85 27,38,1
		21.3	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=85 27,38,26
		31.9	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=85 27,38,30
		42.5	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=85 27,38,30
		53.1	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.02	2d8/10 L=85 19,38,30
		63.8	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.01	2d8/10 L=85 19,38,30
		74.4	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.01	2d8/10 L=85 19,38,30
		85.0	0.38	7.7	7.7	0.0	0.13	0.07	0.10	8.68e-03	2d8/10 L=85 19,38,30
428	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.07	0.06	2d8/10 L=410 19,34,1
	s=7,m=3	51.3	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.05	2d8/10 L=410 30,34,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.03	2d8/10 L=410 26,34,26
		153.8	0.38	7.7	7.7	0.0	0.13	0.11	0.05	0.02	2d8/10 L=410 1,34,22
		205.0	0.38	7.7	7.7	0.0	0.13	0.13	0.04	0.02	2d8/10 L=410 1,31,30
		256.3	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.02	2d8/10 L=410 1,31,27
		307.5	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=410 18,31,23
		358.8	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.04	2d8/10 L=410 30,31,1
		410.0	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.06	2d8/10 L=410 27,31,1
470	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	5.78e-03	2d8/10 L=100 27,34,26
	s=7,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.06	0.05	4.63e-03	2d8/10 L=100 27,31,23
		25.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	5.84e-03	2d8/10 L=100 27,31,15
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.05	8.54e-03	2d8/10 L=100 27,31,1
		50.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.01	2d8/10 L=100 27,31,1
		62.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=100 27,31,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=100 27,31,1
		87.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=100 27,31,1
		100.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=100 1,31,1
455	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.02	2d8/10 L=85 1,34,26
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.02	2d8/10 L=85 1,34,26
		21.3	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.02	2d8/10 L=85 1,34,26
		31.9	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=85 1,34,30
		42.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=85 1,34,30
		53.1	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=85 1,34,30
		63.8	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=85 1,34,19
		74.4	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=85 1,34,19
		85.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.02	2d8/10 L=85 1,34,19
481	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.02	2d8/10 L=85 1,34,30
	s=7,m=3	10.6	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.02	2d8/10 L=85 19,34,30
		21.3	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.02	2d8/10 L=85 19,34,30
		31.9	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=85 19,34,30
		42.5	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=85 19,34,30
		53.1	0.38	7.7	7.7	0.0	0.13	0.06	0.19	0.02	2d8/10 L=85 19,34,27
		63.8	0.38	7.7	7.7	0.0	0.13	0.06	0.19	0.02	2d8/10 L=85 19,34,27
		74.4	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.02	2d8/10 L=85 19,34,15
		85.0	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.03	2d8/10 L=85 19,31,15
M_T= 106 Z=0.0 N=454 N=466											
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
370	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.07	2d8/10 L=95 23,38,26
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.07	2d8/10 L=95 23,38,26
		23.8	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.06	2d8/10 L=95 23,38,26
		35.6	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.06	2d8/10 L=95 23,38,26
		47.5	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.06	2d8/10 L=95 23,38,26
		59.4	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=95 23,35,26
		71.3	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=95 15,35,26
		83.1	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.05	2d8/10 L=95 23,35,23
		95.0	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.05	2d8/10 L=95 23,35,23
421	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.06	0.07	2d8/10 L=410 23,30,1
	s=7,m=3	51.3	0.38	7.7	7.7	0.0	0.13	0.13	0.05	0.05	2d8/10 L=410 30,30,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.12	0.04	0.04	2d8/10 L=410 30,30,26
		153.8	0.38	7.7	7.7	0.0	0.13	0.14	0.04	0.03	2d8/10 L=410 1,30,26
		205.0	0.38	7.7	7.7	0.0	0.13	0.15	0.04	0.03	2d8/10 L=410 1,27,27
		256.3	0.38	7.7	7.7	0.0	0.13	0.14	0.05	0.04	2d8/10 L=410 1,27,27
		307.5	0.38	7.7	7.7	0.0	0.13	0.14	0.05	0.05	2d8/10 L=410 26,27,27
		358.8	0.38	7.7	7.7	0.0	0.13	0.16	0.06	0.06	2d8/10 L=410 26,27,27
		410.0	0.38	7.7	7.7	0.0	0.13	0.24	0.07	0.08	2d8/10 L=410 27,27,1
403	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.01	2d8/10 L=95 27,35,30
	s=7,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.01	2d8/10 L=95 27,35,27

435	ok,ok s=7,m=3	23.8	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02	2d8/10 L=95 27,35,27
		35.6	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02	2d8/10 L=95 27,35,27
		47.5	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02	2d8/10 L=95 27,35,27
		59.4	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02	2d8/10 L=95 27,35,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=95 27,35,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03	2d8/10 L=95 27,35,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.04	2d8/10 L=95 1,35,1
		0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.05	2d8/10 L=100 1,38,30
		12.5	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.05	2d8/10 L=100 1,38,30
		25.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.05	2d8/10 L=100 1,38,30
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.05	2d8/10 L=100 1,38,30
		50.0	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.05	2d8/10 L=100 1,38,30
		62.5	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.04	2d8/10 L=100 27,38,30
		75.0	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.04	2d8/10 L=100 27,35,30
		87.5	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.04	2d8/10 L=100 27,35,30
		100.0	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.04	2d8/10 L=100 27,35,27
Trave		%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc		
		0.38	7.70	7.70	0.0	0.13	0.88	0.30	0.21		

STATI LIMITE D' ESERCIZIO

LEGENDA TABELLA STATI LIMITE D' ESERCIZIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastr	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck wR dR	rRfyk wF dF	rPfck wP dP	per sezioni significative per sezioni significative massimi in campata
setti e gusci	rRfck wR	rRfyk wF	rPfck wP	massimi nei nodi dell'elemento massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	cm					mm	mm	mm		cm	cm	cm	
27	0.0	0.02	0.05	0.01	80,80,90	0.0	0.0	0.0	0,0,0	-2.03e-03	1.97e-03	1.97e-03	80,88,90
	7.5	0.02	0.05	0.01	80,80,90	0.0	0.0	0.0	0,0,0				
	15.0	0.02	0.05	0.01	80,80,90	0.0	0.0	0.0	0,0,0				
...													
563	275.0	0.02	0.03	0.01	85,85,90	0.0	0.0	0.0	0,0,0	0.20	0.15	0.13	80,87,90
Trave		rRfck	rRfyk	rPfck		wR	wF	wP		dR	dF	dP	
		0.32	0.62	0.31		0.19	0.15	0.14		0.39	0.24	0.25	

LEGENDA TABELLA VERIFICHE S.L. ELEMENTI IN LEGNO

Il programma consente la verifica dei seguenti tipi di elementi:

- 1. aste**

L'esito delle verifiche è espresso con un codice come di seguito indicato:

- ok:** verifica con esito positivo
NV: verifica con esito negativo

Le verifiche sono condotte in ottemperanza alle NTC 14 Gennaio 2008 seguendo anche le indicazioni analitiche riportate nella norma tecnica UNI EN 1995-1-1:2005 "Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1: Regole generali - Regole comuni e regole per gli edifici"; in particolare le verifiche effettuate sono riconducibili ai punti:

- 4.4.8 Stati limite ultimi
- 4.4.8.1.7 Tensoflessione
- 4.4.8.1.8 Pressoflessione
- 4.4.8.1.11 Taglio e torsione
- 4.4.8.2.1 Elementi inflessi
- 4.4.8.2.2 Elementi compressi

Le verifiche effettuate sono dettagliatamente riportate come da tabella seguente:

Elem.	Numero dell'elemento
Tipo	Codice di individuazione del tipo di elemento: trave (T) pilastro (P) asta (A)
Stato	Codice della verifica: ok verificato, NV non verificato
Note	Numero della sezione (s) e del materiale (m) dell'archivio
Ver N+/M	Verifica come da formule 4.4.6a e 4.4.6b per tensoflessione I valori di Km utilizzati nelle formule sono definiti dal paragrafo 4.4.8.1.6 (0,7 per sezioni trasversali rettangolari; 1 per altre sezioni trasversali)
Ver N-/M	Verifica come da formule 4.4.7a e 4.4.7b per pressoflessione I valori di Km utilizzati nelle formule sono definiti dal paragrafo 4.4.8.1.6 (0,7 per sezioni trasversali rettangolari; 1 per altre sezioni trasversali)
Ver V/T	Verifica come da formula 4.4.10 (taglio torsione) con interazione ottenuta per quadratura del termine di taglio
Ver N(s)	Verifica instabilità come da formula 4.4.13
Kcy(z)	Fattore di instabilità utilizzato nella formula 4.4.13. Per elementi con snellezza relativa $\leq 0,3$ Kcy(z) è posto = 1 , altrimenti Kcy(z) viene definito dalla 4.4.15
Ver M(s)	Verifica come da formula 4.4.11 (effettuata in entrambi i piani principali) per instabilità laterale
Kcrit (y) / (z)	Fattore di instabilità laterale utilizzato nella formula 4.4.11 rispettivamente per la flessione y e z. Kcrit (y) / (z) viene definito dalla 4.4.12
w_{net R}	Massima deformazione in combinazione rara (F frequente, P quasi permanente)
w_{net Ri}	Massima deformazione in combinazione rara (F frequente, P quasi permanente) valutata a tempo infinito
kdef	Fattore di deformazione dell' elemento
Rif. cmb	Numero della combinazione in cui si è attinto il valore riportato per le verifiche

Si sottolinea che le cinque verifiche sono espresse dal rapporto tra domanda e capacità, affinché la verifica sia positiva il rapporto deve essere inferiore o uguale a 1. La capacità è affetta dal termine **kmod**, espressione della classe di servizio e della durata dei carichi (si considera a livello di combinazione il caso di carico di minor durata).

Le deformazioni dell' elemento espresse in rapporto ad un millesimo di lunghezza sono rappresentate dal valore istantaneo e dal valore a tempo infinito. Il valore della deformazione a tempo infinito per una combinazione di carichi è ottenuta sommando per ogni caso di carico sia il valore istantaneo che il valore ottenuto dall' aliquota quasi-permanente amplificata del fattore k_{def} (formula 2.2 e 2.3).

In termini analitici il contributo del caso di carico con coefficiente di combinazione **Psi** (diverso da 0) è **Psi + kdef * Psi2**

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
97	FATTORE DI STRUTTURA
98	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
99	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
101	VERIFICHE EC5
102	SNELLEZZE EC5

Elem.	Note	Pos. cm	Ver N+/M	Ver N-/M	Ver V/T	Rif. cmb	Ver N(s)	Kcy	Kcz	Ver M(s)	Kcrit(y)	Kcrit(z)	Rif. cmb
1 ok	T,s=6,m=50	0.0	2.18e-04	2.99e-06	4.82e-02	44,1,1	5.75e-03	0.9	0.3	5.75e-03	1.0	1.0	1,1
		80.2	3.01e-02	0.1	4.32e-02	44,1,1	0.1	0.9	0.3	1.61e-02	1.0	1.0	1,1
		160.3	5.14e-02	0.2	3.96e-02	44,1,1	0.2	0.9	0.3	3.78e-02	1.0	1.0	1,1
...													
568 ok	T,s=6,m=50	54.0	0.3	0.3	5.64e-03	11,1,1	0.3	0.6	0.2	0.1	1.0	1.0	1,1
Elem.			Ver N+/M	Ver N-/M	Ver V/T		Ver N(s)	Kcy	Kcz	Ver M(s)	Kcrit(y)	Kcrit(z)	
								0.36	0.13		1.00	1.00	
			0.93	0.93	0.82		0.94			0.87			
Elem.	w,net R	w,net F	w,net P		Rif. cmb	Kdef	w,net Ri	w,net Fi	w,net Pi		Rif. cmb		
1	2.5	1.5	1.2		80,87,90	0.6	4.0	3.0	1.9		80,87,90		
2	2.9	1.7	1.4		80,87,90	0.6	4.6	3.4	2.3		80,87,90		
3	2.9	1.7	1.4		80,87,90	0.6	4.6	3.4	2.2		80,87,90		
4	2.5	1.5	1.2		80,87,90	0.6	4.0	2.9	1.9		80,87,90		
...													
568	9.54e-02	7.99e-02	7.97e-02		80,87,90	0.6	0.2	0.1	0.1		80,87,90		
Elem.	w,net R	w,net F	w,net P				w,net Ri	w,net Fi	w,net Pi				
	19.98	10.22	7.77				31.97	22.20	12.44				

Gli strati sono costituiti da tavole che possono o meno essere incollate lungo il lato lungo.

Gli strati sono caratterizzati dai moduli E0, G0, E90, G90 e Gori, rispettivamente in direzione 0 (parallela alle fibre), 90 (ortogonale alle fibre) e orizzontale.

Per convenzione la direzione 0 del pannello è quella parallela alle fibre del primo (e ultimo) strato. La direzione 0 pertanto ha caratteristiche di resistenza e rigidità superiore alla direzione 1. Il programma ipotizza che la direzione 0 sia verticale per i setti e inclinata rispetto all'asse X per i gusci (inclinazione settabile da criterio di progetto). In fase di verifica non esiste interazione tra direzione 0 e 1.

La peculiarità del pannello XLAM è data dalla presenza di strati molto deformabili a taglio (G90 è di un ordine di grandezza inferiore a G0) così da invalidare l'ipotesi di conservazione delle sezioni piane. L'appendice D della DIN 1052 (D) - 2008 fornisce indicazioni per la valutazione delle rigidità e delle tensioni sui pannelli XLAM, anche considerando la cedevolezza a taglio degli strati. In sostanza le azioni di piastra vengono ripartite su due piani ideali A e B mentre le azioni di lastra sono riportate sul piano ideale C. La deformabilità a taglio regola la ripartizione tra i piani A e B. Utilizzando il riferimento tecnico dell'Università di Monaco "Teilprojekt 15 – TP 15 Flächen aus Brettstapeln, Brettsperrholz und Verbundkonstruktionen" si è implementato l'algoritmo di ripartizione indicato al cap. 5.4.2.3 basato sull'analogia del taglio per carico sinusoidale. In base a questa analogia la quota di carico afferente al piano B viene ridotta in funzione delle caratteristiche statiche del pacchetto di strati e della luce del pannello nella direzione di studio.

Per entrambe le direzioni 0 e 1 si avranno 8 componenti di sollecitazione:

- Momento flettente ripartito su piano A e piano B
- Momento torcente ripartito su piano A e piano B
- Taglio ortogonale ripartito su piano A e piano B
- Sforzo normale su piano C
- Taglio membranale su piano C

Inoltre:

nel caso in cui le tavole siano incollate

- il momento di incollaggio è nullo
- il momento torcente viene ripartito sul piano A e B e verificato per la parte competente allo strato e al pannello (quota di Steiner)
- la resistenza al taglio di piano è offerta dall'intero spessore del pannello
- la dimensione "a" di fig. 16 par. 8.9.3 DIN 1052 (D) è identica nelle due direzioni

in caso contrario

- il momento di incollaggio viene computato secondo DIN D.26
- il momento torcente non viene verificato
- la resistenza al taglio di piano è offerta dallo spessore del pannello ridotto del 75%
- E90 DEVE ESSERE ASSUNTO PARI 0 (gli strati esterni si trascurano per tutti gli effetti in direzione debole)
- la dimensione "a" di fig. 16 par. 8.9.3 DIN 1052 (D) è minore in direzione (1)

Le verifiche V.127, V.128, V.545, V129 (ossia le verifiche per le tensioni normali e tangenziali) sono effettuate per gli strati pari in direzione 0 e per gli strati dispari in direzione 1 (ovvero gli strati con E0), le verifiche V130 e V131 sono effettuate per gli strati pari in direzione 1 e per gli strati dispari in direzione 0 (ovvero gli strati con G90).

Ai fini della verifica a taglio di piastra, è consentita una verifica semplificata che affida al piano B l'intero taglio e determina la tensione tangenziale dividendo il taglio per la dimensione "a" di fig. 16 par. 8.9.3. Il programma prevede a scelta dell'utente questa possibilità.

Si sottolinea che le sei verifiche sono espresse dal rapporto tra domanda e capacità, affinché la verifica sia positiva il rapporto deve essere inferiore o uguale a 1. La capacità è affetta dal termine **kmod**, espressione della classe di servizio e della durata dei carichi (si considera a livello di combinazione il caso di carico di minor durata).

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
126	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
127	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI
128	PROGETTO E VERIFICA DI SOLAI IN MATERIALE XLAM
129	VERIFICA HOLD DOWN DI UN PANNELLO IN XLAM

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
1	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

ok	0.08		kN 3.0	41	4.06e-04		kN -0.9	28	0.23		kN 85.1	kN m 3.783e+04	41
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
270	0.04	0.04	0.0	6,5,0	1.40e-03	0.05	0.05	5,6,5	0.0	0	0.93	0.05	0.95
	0.02	0.01	0.0	6,5,0	4.26e-04	0.05	0.04	5,6,6			1.00	0.04	0.96
463	0.02	0.03	0.0	6,5,0	2.70e-03	0.02	0.02	5,6,5	0.0	0	0.93	0.05	0.95
...													
540	0.02	9.68e-03	0.0	44,45,0	2.44e-04	0.03	0.02	5,5,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.04	0.04	0.0		4.08e-03	0.05	0.05		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
2	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.0		0.0	0	0.0		0.0	0		0.0	0.0	0.0	0	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
247	0.04	0.02	0.0	5,6,0	3.94e-04	0.04	0.04	22,22,19	0.0	0	0.72	0.07	0.93	
	0.01	7.50e-03	0.0	18,15,0	2.76e-04	0.03	0.03	22,21,21			1.00	0.04	0.96	
255	0.04	0.02	0.0	5,6,0	3.94e-04	0.04	0.04	22,22,19	0.0	0	0.72	0.07	0.93	
...														
531	0.01	0.02	0.0	6,5,0	2.33e-04	0.04	0.01	1,6,5	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.04	0.03	0.0		2.71e-03	0.15	0.15		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
3	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.0		0.0	0	0.0		0.0	0		0.0	0.0	0.0	0	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
1170	0.04	0.05	0.0	44,45,0	1.90e-03	0.07	0.10	40,44,45	0.0	0	0.49	0.09	0.91	
	0.05	0.04	0.0	41,40,0	9.49e-04	0.14	0.06	40,41,40			1.00	0.04	0.96	
1173	0.04	0.05	0.0	44,45,0	1.90e-03	0.07	0.10	40,44,45	0.0	0	0.49	0.09	0.91	
...														
1510	0.05	0.04	0.0	41,43,0	9.49e-04	0.14	0.06	40,41,43	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.05	0.05	0.0		1.92e-03	0.14	0.10		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
4	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.03		1.3	1	8.30e-05		-0.2		43	0.35	-1887.8	-8.049e+04	1	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb		V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1224	0.03	0.02	0.0	5,5,0	1.10e-04	0.05	0.05	5,5,6		0.0	0	0.91	0.05	0.95
	3.24e-03	2.12e-03	0.0	5,6,0	3.86e-05	8.04e-03	7.07e-03	5,5,28				1.00	0.04	0.96
1226	0.03	0.02	0.0	5,5,0	1.10e-03	0.05	0.05	5,5,6		0.0	0	0.91	0.05	0.95
...														
1246	0.02	0.01	0.0	5,6,0	3.55e-04	0.06	0.03	5,5,6		0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131			V. D.26				
	0.03	0.05	0.0		1.38e-03	0.10	0.07			0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato								
5	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok								
V. connes.		V. piede	Azione V		Rif. cmb		V. testa		Azione V		Rif. cmb		V. h-d	Azione N		Azione M		Rif. cmb	
			kN						kN					kN		m			
ok		0.0	0.0		0		0.0		0.0		0		0.0	0.0		0.0		0	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B						
11	0.15	0.11	0.0	37,36,0	0.01	0.36	0.44	34,37,36	0.0	0	0.49	0.09	0.91						
	2.19e-03	0.02	0.0	16,11,0	0.01	0.48	0.48	45,44,44			1.00	0.04	0.96						
15	0.15	0.11	0.0	37,36,0	4.49e-03	0.18	0.27	32,37,36	0.0	0	0.49	0.09	0.91						
...																			
644	6.08e-03	0.01	0.0	36,1,0	7.89e-04	0.03	0.03	17,36,37	0.0	0	1.00	0.04	0.96						
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26										
	0.19	0.14	0.0		0.01	0.48	0.48		0.0										

Setto	Mat.							N. strati	Spessore	Incoll.	Stato								
									cm										
6	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok								
V. connes.	V. piede	Azione V			Rif. cmb		V. testa		Azione V		Rif. cmb		V. h-d	Azione N		Azione M		Rif. cmb	
				kN						kN					kN		kN m		
ok	0.04			-1.5		39		2.83e-04		-0.6		28		0.13		-139.6	2.299e+04		42
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B						
16	0.04	0.04	0.0	10,9,0	3.51e-03	0.04	0.05	10,10,9	0.0	0	0.93	0.05	0.95						
	0.01	0.01	0.0	10,9,0	1.20e-03	0.04	0.04	10,10,9			1.00	0.04	0.96						
17	0.04	0.04	0.0	10,9,0	1.30e-03	0.04	0.05	10,10,9	0.0	0	0.93	0.05	0.95						
...																			
1372	7.29e-03	0.02	0.0	31,9,0	1.24e-03	0.02	0.01	10,10,9	0.0	0	1.00	0.04	0.96						
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26										
	0.04	0.04	0.0		3.54e-03	0.04	0.05		0.0										

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
7	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
			kN				kN			kN		kN m	
ok	0.0		0.0	0	0.0		0.0	0	0.0	0.0		0.0	0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
10	0.09	0.07	0.0	42,39,0	0.01	0.41	0.41	45,44,45	0.0	0	0.49	0.09	0.91
	0.17	0.16	0.0	45,44,0	3.47e-03	0.46	0.11	40,45,11			1.00	0.04	0.96
516	0.11	0.08	0.0	44,45,0	3.89e-03	0.10	0.16	45,44,45	0.0	0	0.49	0.09	0.91
...													
1134	0.07	0.09	0.0	12,11,0	0.01	0.48	0.48	45,44,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.38	0.28	0.0		0.03	0.53	0.69		0.0				

Setto	Mat.	N. strati							Spessore	Incoll.	Stato		
									cm				
8	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5							13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
		kN					kN				kN	m	
ok	0.0	0.0		0	0.0		0.0		0	0.0	0.0	0.0	0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
291	9.38e-03	3.00e-03	0.0	17,16,0	2.40e-04	0.01	4.17e-03	23,17,20	0.0	0	0.85	0.06	0.94
	6.61e-03	7.81e-03	0.0	15,18,0	1.31e-04	0.02	0.01	35,19,30			1.00	0.04	0.96
292	9.38e-03	3.20e-03	0.0	17,32,0	6.43e-04	0.01	4.17e-03	34,17,20	0.0	0	0.85	0.06	0.94
...													
402	0.01	0.01	0.0	42,39,0	1.43e-04	0.03	0.02	33,42,45	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.04	0.02	0.0		1.73e-03	0.05	0.04		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
9	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M		Rif. cmb
			kN				kN					kN	kN	m	
ok	0.0	0.0		0	0.0	0.0		0		0.0	0.0		0.0		0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1221	8.64e-03	0.02	0.0	6,5,0	6.51e-04	0.02	0.03	29,6,5	0.0	0	0.49	0.09	0.91
	3.20e-03	6.14e-03	0.0	27,5,0	5.76e-04	0.01	0.01	1,27,25			1.00	0.04	0.96
1222	8.64e-03	0.02	0.0	6,5,0	6.51e-04	0.02	0.03	29,6,5	0.0	0	0.49	0.09	0.91
...													
1497	0.01	0.02	0.0	27,30,0	9.35e-04	0.04	0.02	5,27,29	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.02	0.02	0.0		1.50e-03	0.04	0.04		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato
									cm		
10	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
		kN				kN					kN	kN m	
ok	0.0	0.0		0	0.0	0.0		0		0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1460	0.02	0.02	0.0	35,38,0	3.13e-04	0.03	0.03	32,35,26	0.0	0	0.35	0.12	0.88
	0.0	0.03	0.0	0,1,0	2.51e-04	7.08e-03	0.01	32,16,16			0.0	0.0	0.0
1469	0.02	0.02	0.0	35,38,0	3.13e-04	0.03	0.03	32,35,26	0.0	0	0.35	0.12	0.88
...													
1565	1.04e-03	5.63e-03	0.0	36,1,0	2.09e-03	6.32e-03	6.70e-03	37,25,24	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.03	0.0		2.93e-03	0.04	0.04		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
14	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb	
ok	0.27	kN 24.8		18	2.57e-03	kN -16.9		31	0.41	kN -5323.3	kN m -4.989e+05	21	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1004	0.01	0.01	0.0	41,40,0	1.51e-03	0.02	0.02	18,21,20	0.0	0	0.91	0.05	0.95
	8.79e-03	0.02	0.0	19,22,0	1.28e-03	0.02	9.46e-03	18,15,18			1.00	0.04	0.96
1005	6.63e-03	0.01	0.0	41,40,0	1.51e-03	0.01	0.02	18,28,28	0.0	0	0.91	0.05	0.95
...													
1043	0.08	0.05	0.0	31,34,0	8.46e-04	0.11	0.03	38,31,20	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.07	0.0		1.51e-03	0.18	0.06		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
									cm					
16	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		m	
ok	0.21	-16.5		1	1.23e-03		-6.7		43	0.26	-4339.4		-2.329e+05	29
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
1193	0.07	0.06	0.0	28,28,0	2.13e-03	0.09	0.10	21,21,21	0.0	0	0.91	0.05	0.95	
	0.0	0.02	0.0	0,1,0	1.56e-03	0.01	0.01	1,20,20			0.0	0.0	0.0	
1194	0.06	0.06	0.0	21,21,0	1.29e-03	0.08	0.08	1,20,20	0.0	0	0.91	0.05	0.95	
...														

1375	0.03	0.04	0.0	28,29,0	7.41e-04	0.10	0.07	25,28,29	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.07	0.06	0.0		2.96e-03	0.10	0.10		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
18	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.04	kN 1.6	23	2.41e-03	kN 7.2	27	0.52	kN 1072.0	kN m 1.110e+05	30			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1195	2.89e-03	0.08	0.0	29,1,0	3.21e-03	0.08	0.10	44,45,45	0.0	0	0.91	0.05	0.95
	0.13	0.07	0.0	29,28,0	2.71e-03	0.29	0.23	44,45,44			1.00	0.04	0.96
1337	0.02	0.04	0.0	44,45,0	2.60e-04	0.02	0.04	43,44,45	0.0	0	0.91	0.05	0.95
...													
1425	0.10	0.06	0.0	29,28,0	1.54e-03	0.12	0.03	43,29,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.13	0.11	0.0		3.70e-03	0.29	0.23		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
20	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.09	kN -6.6	43	1.81e-03	kN -9.3	43	0.17	kN -4048.6	kN m 1.366e+05	46			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1174	0.02	0.06	0.0	31,1,0	4.45e-04	0.03	0.06	32,36,34	0.0	0	0.91	0.05	0.95
	0.0	0.02	0.0	0,1,0	2.53e-04	9.17e-03	0.01	40,44,44			0.0	0.0	0.0
1175	0.02	0.06	0.0	19,1,0	1.43e-03	0.03	0.06	32,36,34	0.0	0	0.91	0.05	0.95
...													
1701	0.28	0.26	0.0	44,44,0	2.45e-03	0.79	0.18	42,44,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.28	0.27	0.0		7.75e-03	0.79	0.44		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
22	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.03	kN -1.0	33	8.21e-04	kN 2.4	36	0.16	kN -2170.9	kN m -5.279e+04	37			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
845	0.02	0.04	0.0	16,9,0	1.33e-03	0.03	0.04	18,25,24	0.0	0	0.91	0.05	0.95
	2.46e-03	9.21e-03	0.0	34,9,0	4.58e-04	0.01	0.01	18,16,16			1.00	0.04	0.96
847	0.02	0.04	0.0	16,9,0	2.80e-04	0.03	0.04	29,25,24	0.0	0	0.91	0.05	0.95
...													
1503	8.12e-03	0.01	0.0	9,9,0	1.14e-04	0.03	0.01	9,9,16	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.06	0.09	0.0		1.92e-03	0.08	0.09		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
24	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.19	kN 17.3	34	2.50e-03	kN 15.7	1	0.36	kN -6447.7	kN m -4.261e+05	33			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1430	0.03	0.06	0.0	16,15,0	8.70e-04	0.03	0.06	37,16,17	0.0	0	0.91	0.05	0.95

1435	1.91e-03	0.02	0.0	36,1,0	7.71e-04	5.40e-03	9.17e-03	37,26,1			1.00	0.04	0.96
...	0.03	0.06	0.0	16,15,0	2.90e-03	0.03	0.06	37,16,17	0.0	0	0.91	0.05	0.95
1507	0.03	0.02	0.0	34,31,0	3.74e-04	0.05	0.02	32,18,17	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.06	0.0		2.90e-03	0.05	0.06		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
26	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.08		7.1	35	7.79e-04		4.9	23	0.18		-3979.0	-1.567e+05	1
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
542	0.02	0.03	0.0	32,1,0	9.41e-05	0.03	0.03	35,38,32	0.0	0	0.91	0.05	0.95
	0.08	0.05	0.0	38,32,0	2.69e-04	0.19	0.09	32,32,32			1.00	0.04	0.96
546	6.07e-03	0.04	0.0	14,13,0	3.28e-04	0.03	0.04	13,13,13	0.0	0	0.91	0.05	0.95
...													
910	0.03	3.83e-03	0.0	13,38,0	2.13e-04	0.05	0.03	13,13,33	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.05	0.0		3.28e-04	0.19	0.09		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
30	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.06		-5.6	25	6.51e-04		-4.2	25	0.03		-2548.4	-2.496e+04	13
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
518	0.02	0.02	0.0	38,13,0	2.12e-04	0.03	0.04	37,14,13	0.0	0	0.91	0.05	0.95
	0.02	0.03	0.0	38,35,0	1.15e-04	0.05	0.03	36,37,36			1.00	0.04	0.96
519	0.03	0.03	0.0	37,35,0	6.17e-03	0.20	0.20	37,37,37	0.0	0	0.91	0.05	0.95
...													
1534	0.31	0.25	0.0	32,33,0	0.01	0.83	0.60	37,37,37	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.31	0.25	0.0		0.02	0.83	0.63		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
32	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.10		9.9	1	2.09e-03		3.0	1		0.05	-719.7	-3.743e+04		24
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
1	6.07e-03	0.01	0.0	10,9,0	1.51e-04	3.74e-03	8.62e-03	1,28,9	0.0	0	0.94	0.05	0.95	
	0.02	0.01	0.0	9,9,0	1.38e-04	0.04	0.02	1,9,9			1.00	0.04	0.96	
2	6.07e-03	0.01	0.0	10,9,0	1.89e-04	3.14e-03	6.71e-03	9,10,9	0.0	0	0.94	0.05	0.95	
...														
1447	0.02	0.04	0.0	10,9,0	5.75e-04	0.08	0.06	9,10,9	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.07	0.06	0.0		1.40e-03	0.20	0.06		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
33	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.08	-5.7	25	1.58e-03	9.0	24	0.24	-58.7	-1.444e+05	24

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
507	0.01	0.02	0.0	14,13,0	1.17e-03	0.05	0.05	36,35,35	0.0	0	0.91	0.05	0.95
	0.10	0.08	0.0	37,36,0	6.10e-04	0.22	0.08	37,37,36			1.00	0.04	0.96
513	0.02	0.03	0.0	37,13,0	4.09e-04	0.04	0.05	37,31,35	0.0	0	0.91	0.05	0.95
...													
950	0.18	0.14	0.0	38,36,0	3.96e-03	0.49	0.34	35,38,35	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.18	0.14	0.0		3.96e-03	0.49	0.34		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
34	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.07	kN			kN			kN	kN m	
		-6.2	31	7.63e-04	0.4	10	0.04	-2542.7	3.315e+04	2

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
477	0.03	0.05	0.0	10,9,0	8.98e-04	0.06	0.07	9,10,9	0.0	0	0.95	0.05	0.95
	3.20e-03	1.21e-03	0.0	17,16,0	2.94e-04	0.05	0.05	9,9,9			1.00	0.04	0.96
479	0.03	0.05	0.0	10,9,0	1.65e-03	0.06	0.07	9,10,9	0.0	0	0.95	0.05	0.95
...													
1456	1.34e-03	0.01	0.0	15,10,0	9.71e-04	0.04	0.05	9,9,10	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.24	0.24	0.0		8.06e-03	0.69	0.35		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
36	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.08	kN			kN			kN	kN m	
		-7.8	33	6.50e-04	-1.4	1	0.03	-1819.6	-2.039e+04	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
515	0.18	0.14	0.0	10,9,0	7.85e-04	0.18	0.14	9,10,9	0.0	0	0.96	0.05	0.95
	0.03	0.02	0.0	10,9,0	2.21e-04	0.08	0.02	9,10,9			1.00	0.04	0.96
684	0.18	0.14	0.0	10,9,0	6.36e-04	0.18	0.14	9,10,9	0.0	0	0.96	0.05	0.95
...													
1470	0.03	0.02	0.0	9,10,0	2.40e-05	0.09	0.02	9,9,10	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.18	0.14	0.0		1.02e-03	0.18	0.14		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
37	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.43	kN			kN			kN	kN m	
		24.0	16	7.80e-03	39.2	15	0.66	4984.2	7.026e+05	17

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
572	0.13	0.13	0.0	45,41,0	0.02	0.67	0.67	40,44,44	0.0	0	0.91	0.05	0.95
	0.41	0.26	0.0	16,17,0	6.84e-03	0.87	0.43	42,32,42			1.00	0.04	0.96
1069	0.10	0.09	0.0	40,41,0	1.15e-03	0.11	0.10	16,40,42	0.0	0	0.91	0.05	0.95
...													
1162	0.20	0.15	0.0	19,22,0	3.18e-03	0.40	0.09	19,39,17	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.41	0.26	0.0		0.03	0.99	0.85		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
38	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
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ok	0.06		kN 4.3	32	1.78e-04		kN 0.4	36	0.05	kN -2267.8	kN m -3.326e+04		9
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
405	0.03	0.06	0.0	10,9,0	1.78e-03	0.08	0.12	10,9,9	0.0	0	0.96	0.05	0.95
	7.47e-03	8.66e-03	0.0	15,9,0	6.30e-04	0.06	0.06	10,9,9			1.00	0.04	0.96
409	0.03	0.06	0.0	10,9,0	4.46e-03	0.08	0.12	9,9,9	0.0	0	0.96	0.05	0.95
...													
1549	0.01	8.59e-03	0.0	9,10,0	1.70e-03	0.03	0.02	9,10,10	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.22	0.18	0.0		0.01	0.53	0.51		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
40	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.05	3.8	1	0.01	20.6	36	0.51	-875.0	-2.998e+05	33			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1477	9.10e-03	0.06	0.0	34,1,0	1.09e-03	0.03	0.05	35,15,15	0.0	0	0.96	0.05	0.95
	0.02	0.02	0.0	31,38,0	9.37e-04	0.02	5.42e-03	35,31,1			1.00	0.04	0.96
1485	0.02	0.08	0.0	32,1,0	3.02e-03	0.03	0.04	33,32,1	0.0	0	0.96	0.05	0.95
....													
1538	0.05	0.03	0.0	38,35,0	4.49e-03	0.08	0.02	34,38,35	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.11	0.11	0.0		7.30e-03	0.17	0.07		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
41	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
445	0.02	0.02	0.0	33,35,0	9.07e-04	0.05	0.04	1,33,38	0.0	0	0.86	0.05	0.95
	0.01	0.01	0.0	35,38,0	8.59e-04	0.03	0.03	1,31,31			1.00	0.04	0.96
455	8.33e-03	6.92e-03	0.0	38,35,0	5.53e-04	0.02	0.02	1,31,36	0.0	0	0.86	0.05	0.95
....													
1734	0.0	0.05	0.0	0,1,0	4.62e-04	0.02	0.02	1,37,33	0.0	0	0.0	0.0	0.0
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.26	0.21	0.0		0.02	0.75	0.76		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
42	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
205	0.12	0.11	0.0	38,34,0	7.95e-04	0.11	0.12	38,32,38	0.0	0	0.86	0.05	0.95
	0.06	0.06	0.0	36,36,0	6.56e-04	0.17	0.13	38,36,38			1.00	0.04	0.96
717	0.10	0.08	0.0	38,35,0	3.09e-03	0.19	0.20	1,36,37	0.0	0	0.86	0.05	0.95
....													
1736	0.06	0.04	0.0	32,33,0	1.59e-03	0.16	0.05	1,32,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.20	0.15	0.0		8.03e-03	0.34	0.34		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
44	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V	Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
ok	0.13	kN 4.7		32	1.05e-03		kN 2.5	34	0.34	kN -2842.7	kN m 1.369e+05		34
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
279	0.03	0.10	0.0	33,1,0	3.03e-03	0.04	0.07	32,37,44	0.0	0	0.96	0.05	0.95
	0.02	0.01	0.0	35,38,0	2.46e-03	0.04	0.03	38,43,46			1.00	0.04	0.96
281	0.03	0.10	0.0	33,1,0	2.94e-04	0.04	0.07	32,37,44	0.0	0	0.96	0.05	0.95
...													
1172	0.16	0.11	0.0	31,34,0	1.76e-03	0.32	0.17	34,31,19	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.16	0.11	0.0		5.38e-03	0.32	0.34		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
45	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V	Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
ok	0.14	kN -10.5		31	2.47e-03		kN -2.7	1	0.22	kN -2374.3	kN m -1.419e+05		31
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
291	2.43e-03	6.58e-03	0.0	33,1,0	2.03e-04	8.22e-03	9.98e-03	20,21,20	0.0	0	0.95	0.05	0.95
	0.02	2.69e-03	0.0	1,20,0	6.47e-05	0.04	2.54e-03	40,21,44			1.00	0.04	0.96
292	6.37e-03	0.01	0.0	33,32,0	3.43e-04	0.02	0.02	40,20,20	0.0	0	0.95	0.05	0.95
...													
1498	0.02	4.96e-03	0.0	18,15,0	2.29e-04	0.04	0.02	21,21,20	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.10	0.0		1.84e-03	0.10	0.10		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
47	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V	Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
ok	0.14	kN -8.4		37	2.93e-03		kN -3.7	1	0.13	kN 312.6	kN m -6.269e+04		37
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
334	0.02	0.03	0.0	10,9,0	6.65e-04	0.03	0.04	9,10,9	0.0	0	0.94	0.05	0.95
	0.01	0.01	0.0	9,9,0	5.60e-04	0.03	0.02	31,9,9			1.00	0.04	0.96
336	0.02	0.03	0.0	10,9,0	4.38e-04	0.03	0.04	9,10,9	0.0	0	0.94	0.05	0.95
...													
1498	0.02	0.01	0.0	18,15,0	4.81e-04	0.05	0.03	1,21,20	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.06	0.06	0.0		8.54e-04	0.14	0.05		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
48	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V	Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
ok	0.37	kN 27.9		15	3.32e-03		kN -17.0	17	0.11	kN -1992.8	kN m -7.680e+04		17
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
570	0.12	0.11	0.0	41,41,0	2.42e-03	0.21	0.22	43,41,41	0.0	0	0.91	0.05	0.95
	0.19	0.15	0.0	35,38,0	6.08e-04	0.50	0.10	19,38,38			1.00	0.04	0.96
571	0.13	0.11	0.0	41,41,0	1.07e-03	0.16	0.16	41,41,45	0.0	0	0.91	0.05	0.95
...													
1097	0.19	0.15	0.0	35,38,0	1.44e-03	0.50	0.10	22,38,38	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.15	0.0		4.67e-03	0.50	0.23		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
49	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN					kN	kN m	
ok	0.0	0.0		0	0.0	0.0		0		0.0	0.0		0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
357	0.02	0.02	0.0	37,36,0	1.19e-03	0.05	0.05	6,9,10	0.0	0	0.72	0.07	0.93
	0.02	0.03	0.0	9,10,0	1.16e-03	0.15	0.14	6,9,10			1.00	0.04	0.96
359	2.65e-03	1.76e-03	0.0	26,23,0	3.25e-04	0.01	8.85e-03	36,9,9	0.0	0	0.72	0.07	0.93
...													
415	6.81e-03	0.01	0.0	10,9,0	1.04e-04	0.02	0.01	36,10,9	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.03	0.0		1.19e-03	0.15	0.14		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
51	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.06	-2.1		37	4.70e-04		1.0		24	0.17	-666.4		-3.156e+04	37

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
24	0.03	0.03	0.0	10,9,0	2.58e-03	0.03	0.03	10,10,9	0.0	0	0.93	0.05	0.95
	0.02	0.01	0.0	10,9,0	7.06e-04	0.05	0.04	10,10,9			1.00	0.04	0.96
26	0.03	0.03	0.0	10,9,0	1.14e-03	0.03	0.03	9,10,9	0.0	0	0.93	0.05	0.95
...													
416	0.02	0.01	0.0	10,9,0	3.87e-04	0.05	0.04	9,10,9	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.03	0.0		2.66e-03	0.05	0.04		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
52	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb	
		kN				kN				kN	kN m		
ok	0.10	-10.6		29	1.24e-03	-9.4		26	0.23	-3283.8	-2.842e+05		24

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
448	0.01	0.02	0.0	45,13,0	3.48e-04	0.03	0.04	38,45,43	0.0	0	0.91	0.05	0.95
	0.05	0.04	0.0	30,44,0	3.10e-04	0.12	0.07	35,46,35			1.00	0.04	0.96
453	0.01	0.02	0.0	45,13,0	5.33e-04	0.03	0.03	46,45,45	0.0	0	0.91	0.05	0.95
...													
979	0.07	0.05	0.0	25,24,0	1.48e-03	0.19	0.15	38,37,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.08	0.0		1.90e-03	0.19	0.15		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato								
			cm										
53	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok								
V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.04	-4.1	38	1.50e-03	-10.4	26	0.30	-5087.7	3.318e+05		1		
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1	0.01	0.01	0.0	11,11,0	3.14e-04	0.01	0.01	11,11,11	0.0	0	0.92	0.05	0.95
	0.02	0.02	0.0	1,1,0	1.33e-04	0.05	0.01	1,1,13			1.00	0.04	0.96
2	0.02	0.02	0.0	11,11,0	2.85e-04	0.01	0.01	38,11,11	0.0	0	0.92	0.05	0.95
...													

1594	0.01	0.03	0.0	11,1,0	3.67e-04	0.05	0.03	9,11,11	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.26	0.26	0.0		0.03	0.58	0.34		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
55	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.03	-2.2	9	1.25e-03	5.4	24	0.37	-4157.6	-2.119e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
24	0.03	0.03	0.0	37,1,0	9.45e-04	0.04	0.04	33,37,11	0.0	0	0.92	0.05	0.95
	4.40e-03	8.36e-03	0.0	18,11,0	3.71e-04	0.03	0.03	37,11,1			1.00	0.04	0.96
26	0.03	0.03	0.0	37,1,0	7.97e-04	0.04	0.04	1,37,11	0.0	0	0.92	0.05	0.95
...													
1585	0.09	0.04	0.0	32,38,0	5.15e-03	0.22	0.07	1,38,1	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.33	0.31	0.0		0.02	0.55	0.36		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
57	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.12	9.0	19	1.49e-03	-7.4	30	0.35	-3704.4	2.692e+05	30

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
466	0.04	0.04	0.0	37,36,0	7.66e-04	0.05	0.05	11,37,36	0.0	0	0.94	0.05	0.95
	1.81e-03	5.97e-03	0.0	20,1,0	3.36e-04	0.02	0.02	11,11,11			1.00	0.04	0.96
467	0.04	0.04	0.0	37,36,0	1.72e-03	0.05	0.05	31,37,36	0.0	0	0.94	0.05	0.95
...													
585	0.23	0.16	0.0	36,37,0	4.10e-03	0.58	0.22	34,36,37	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.23	0.16	0.0		8.17e-03	0.58	0.22		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
58	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.08	-8.7	30	2.05e-03	-15.5	29	0.30	-3135.3	3.652e+05	30

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
418	0.01	0.03	0.0	14,13,0	1.64e-03	0.04	0.05	29,37,31	0.0	0	0.91	0.05	0.95
	0.14	0.08	0.0	29,28,0	1.42e-03	0.20	0.08	29,29,34			1.00	0.04	0.96
428	0.01	0.02	0.0	45,13,0	7.90e-04	0.03	0.03	26,45,43	0.0	0	0.91	0.05	0.95
...													
1002	0.08	0.05	0.0	26,23,0	1.29e-04	0.13	0.03	30,26,43	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.10	0.0		1.64e-03	0.20	0.17		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
60	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.25	9.3	19	1.41e-03	4.6	18	0.25	-2717.6	9.816e+04	18

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
129	0.06	0.07	0.0	34,31,0	9.41e-03	0.28	0.29	34,34,31	0.0	0	0.96	0.05	0.95

567	0.09	0.08	0.0	32,33,0	4.42e-03	0.28	0.24	34,32,33			1.00	0.04	0.96
...	0.13	0.13	0.0	35,31,0	9.14e-03	0.37	0.35	32,33,32	0.0	0	0.96	0.05	0.95
1172	0.14	0.08	0.0	31,42,0	3.18e-03	0.33	0.21	34,31,33	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.22	0.0		0.02	0.85	0.73		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
62	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
769	0.08	0.06	0.0	39,42,0	4.43e-03	0.24	0.23	34,31,33	0.0	0	0.88	0.05	0.95
	0.19	0.16	0.0	31,34,0	8.39e-03	0.53	0.45	34,38,37			1.00	0.04	0.96
770	0.08	0.06	0.0	39,41,0	3.39e-03	0.11	0.11	1,32,34	0.0	0	0.88	0.05	0.95
...													
836	0.03	0.02	0.0	44,45,0	9.10e-03	0.46	0.45	32,36,37	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.16	0.0		0.03	0.86	0.82		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
64	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.51		-28.4	18	4.56e-03		22.6	16	0.42		-5311.6	3.548e+05	17
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
568	0.05	0.09	0.0	41,1,0	5.11e-03	0.26	0.26	42,46,46	0.0	0	0.91	0.05	0.95
	0.36	0.23	0.0	42,39,0	0.02	0.95	0.75	43,46,43			1.00	0.04	0.96
569	0.06	0.05	0.0	41,43,0	1.06e-03	0.10	0.10	17,41,41	0.0	0	0.91	0.05	0.95
...													
1067	0.23	0.15	0.0	22,19,0	2.82e-03	0.42	0.12	19,22,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.36	0.23	0.0		0.02	0.95	0.75		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
65	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.14		-5.4	18	1.82e-03		-6.3	1	0.33		-2936.8	-1.365e+05	16
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
566	0.15	0.17	0.0	32,33,0	8.85e-03	0.10	0.09	32,32,33	0.0	0	0.96	0.05	0.95
	0.13	0.13	0.0	37,36,0	3.49e-03	0.36	0.23	32,37,36			1.00	0.04	0.96
748	0.04	0.16	0.0	32,1,0	2.02e-03	0.09	0.15	15,38,31	0.0	0	0.96	0.05	0.95
....													
1169	0.08	0.06	0.0	31,34,0	3.44e-03	0.20	0.13	32,31,33	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.17	0.23	0.0		0.02	0.36	0.26		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
67	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.04	-2.4	43	7.72e-04	-3.2	41	0.15	-1743.7	7.498e+04	40

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1248	0.05	0.05	0.0	29,28,0	1.84e-04	0.06	0.06	17,21,25	0.0	0	0.91	0.05	0.95
	4.40e-03	5.57e-03	0.0	41,40,0	4.86e-05	7.24e-03	7.49e-03	40,41,5			1.00	0.04	0.96
1249	0.05	0.05	0.0	29,28,0	5.06e-04	0.06	0.06	20,21,25	0.0	0	0.91	0.05	0.95
...													
1273	0.05	0.05	0.0	6,5,0	4.63e-04	0.14	0.07	5,6,5	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.07	0.0		8.64e-04	0.20	0.07		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
68	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.18	kN			kN			kN	kN m	
		6.8	32	1.99e-03	4.8	32	0.33	-3327.8	1.382e+05	32

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
275	0.09	0.14	0.0	25,24,0	6.91e-04	0.12	0.13	24,25,24	0.0	0	0.96	0.05	0.95
	1.32e-03	8.65e-03	0.0	37,1,0	1.04e-04	9.84e-03	0.01	24,26,26			1.00	0.04	0.96
280	0.09	0.14	0.0	25,24,0	1.80e-03	0.12	0.13	38,25,24	0.0	0	0.96	0.05	0.95
...													
1169	0.06	0.04	0.0	37,36,0	2.64e-03	0.08	0.02	36,37,32	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.14	0.0		5.04e-03	0.13	0.13		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
70	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.0	kN			kN			kN	kN m	
		0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
290	0.02	0.02	0.0	23,26,0	1.49e-03	0.03	0.03	37,23,26	0.0	0	0.85	0.06	0.94
	0.03	0.02	0.0	28,29,0	1.08e-03	0.07	0.03	33,28,23			1.00	0.04	0.96
294	0.02	0.02	0.0	23,26,0	1.49e-03	0.03	0.03	37,23,26	0.0	0	0.85	0.06	0.94
...													
984	9.07e-03	7.44e-03	0.0	17,16,0	3.84e-04	0.02	0.02	37,17,24	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.02	0.0		1.89e-03	0.07	0.05		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
72	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.12	kN			kN			kN	kN m	
		-9.0	35	2.58e-03	-3.2	1	0.14	-3353.7	1.044e+05	34

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
315	0.04	0.05	0.0	27,30,0	4.00e-04	0.04	0.05	9,27,9	0.0	0	0.94	0.05	0.95
	5.83e-03	0.01	0.0	37,9,0	1.41e-04	0.01	0.01	9,37,9			1.00	0.04	0.96
320	0.04	0.05	0.0	27,30,0	9.66e-04	0.04	0.05	9,27,9	0.0	0	0.94	0.05	0.95
...													
1488	0.03	0.02	0.0	24,29,0	7.05e-04	0.07	0.05	25,23,26	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.07	0.07	0.0		1.84e-03	0.18	0.08		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
73	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

ok	0.09		kN -6.8	28	7.90e-04		kN -4.2	43	0.10		kN -253.8	kN m -5.784e+04	46
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1268	0.02	0.02	0.0	6,5,0	2.12e-04	0.02	0.03	5,6,5	0.0	0	0.91	0.05	0.95
	4.66e-03	4.96e-03	0.0	41,40,0	1.07e-04	7.34e-03	6.01e-03	5,41,6			1.00	0.04	0.96
1269	0.01	0.02	0.0	22,21,0	2.12e-04	0.02	0.02	5,6,5	0.0	0	0.91	0.05	0.95
...													
1293	0.03	0.02	0.0	6,5,0	7.51e-05	0.07	0.03	27,6,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.05	0.04	0.0		4.81e-04	0.14	0.03		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
74	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.12		-4.2	17	1.43e-03		3.6	9	0.50		-3286.2	-1.077e+05	5
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
454	0.08	0.09	0.0	33,32,0	1.00e-03	0.06	0.06	11,33,32	0.0	0	0.94	0.05	0.95
	3.69e-03	0.02	0.0	12,11,0	3.70e-04	0.03	0.03	37,35,35			1.00	0.04	0.96
456	0.08	0.09	0.0	33,32,0	5.04e-03	0.06	0.07	33,33,32	0.0	0	0.94	0.05	0.95
...													
639	0.04	0.02	0.0	21,20,0	2.07e-03	0.08	0.05	41,41,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.09	0.0		7.21e-03	0.08	0.07		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
77	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
	ok	0.15	kN				kN				kN	kN m		
			-11.0	33	2.18e-03		-2.4	1		0.20	-2248.3	-1.258e+05	33	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
305	0.23	0.20	0.0	24,25,0	1.36e-03	0.23	0.19	29,24,25	0.0	0	0.95	0.05	0.95	
	7.92e-03	9.76e-03	0.0	38,35,0	1.99e-04	0.01	8.93e-03	35,28,23			1.00	0.04	0.96	
893	5.12e-03	7.35e-03	0.0	15,34,0	9.99e-04	0.02	0.02	23,15,18	0.0	0	0.95	0.05	0.95	
...														
1488	0.02	8.25e-03	0.0	16,17,0	7.33e-04	0.06	0.05	23,23,26	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.23	0.20	0.0		3.38e-03	0.23	0.19		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
78	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.19		-5.5	30	1.69e-03		-7.2	26		0.05	-230.2	2.280e+04	28	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
1294	0.13	0.10	0.0	39,43,0	1.11e-03	0.14	0.16	46,39,43	0.0	0	0.80	0.06	0.94	
	6.32e-03	5.30e-03	0.0	43,46,0	1.18e-04	0.02	0.01	46,43,46			1.00	0.04	0.96	
1295	0.13	0.10	0.0	39,43,0	1.11e-03	0.14	0.16	46,39,43	0.0	0	0.80	0.06	0.94	
...														
1355	0.03	0.02	0.0	45,44,0	3.41e-04	0.08	0.04	43,45,43		0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.21	0.16	0.0		4.34e-03	0.30	0.32		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
79	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN					kN				kN	m		
ok	0.0	0.0		0	0.0		0.0		0	0.0	0.0	0.0		0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
335	0.06	0.04	0.0	26,23,0	1.05e-03	0.08	0.09	23,26,23	0.0	0	0.72	0.07	0.93	
	0.02	0.01	0.0	30,27,0	4.82e-04	0.07	0.05	26,26,26			1.00	0.04	0.96	
340	0.06	0.04	0.0	26,23,0	1.05e-03	0.08	0.09	23,26,23	0.0	0	0.72	0.07	0.93	
...														
1388	0.01	0.02	0.0	10,9,0	2.05e-04	0.04	0.04	38,10,26	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.06	0.04	0.0		2.28e-03	0.15	0.15		0.0					

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
81	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.07	kN 6.1	35	1.46e-03	kN -10.1	38	0.21	kN -4872.2	kN m 2.284e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
16	0.05	0.04	0.0	35,38,0	1.65e-03	0.04	0.04	35,35,38	0.0	0	0.92	0.05	0.95
	2.92e-03	7.36e-03	0.0	12,13,0	6.31e-04	0.02	0.02	35,11,11			1.00	0.04	0.96
17	0.05	0.04	0.0	35,38,0	5.27e-04	0.04	0.04	37,35,38	0.0	0	0.92	0.05	0.95
...													
1126	9.49e-03	0.02	0.0	12,11,0	6.69e-04	0.04	0.01	38,11,34	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.35	0.36	0.0		0.06	0.92	0.75		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
82	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN				kN				kN	kN m		
ok	0.09	-4.9		29	1.04e-03	4.1		28	0.27	384.5	9.543e+04		29
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
363	0.06	0.05	0.0	43,45,0	4.22e-04	0.10	0.10	45,43,45	0.0	0	0.91	0.05	0.95
	0.15	0.10	0.0	43,46,0	3.15e-03	0.38	0.29	43,44,46			1.00	0.04	0.96
1312	0.34	0.26	0.0	45,44,0	1.74e-03	0.24	0.23	44,46,44	0.0	0	0.91	0.05	0.95
...													
1660	0.01	7.06e-03	0.0	29,28,0	4.59e-04	0.02	0.01	28,29,43	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.34	0.26	0.0		3.15e-03	0.38	0.29		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
83	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN				kN				kN	kN m		
ok	0.0	0.0		0	0.0	0.0		0	0.0	0.0	0.0		0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
5	0.25	0.20	0.0	32,34,0	5.74e-03	0.32	0.32	38,32,36	0.0	0	0.88	0.05	0.95
	0.10	0.07	0.0	36,37,0	5.53e-03	0.41	0.36	37,36,36			1.00	0.04	0.96
25	0.09	0.05	0.0	40,41,0	4.28e-03	0.28	0.28	45,32,37	0.0	0	0.88	0.05	0.95
...													
1728	0.10	0.07	0.0	32,36,0	5.92e-03	0.26	0.14	1,32,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.28	0.20	0.0		0.02	0.72	0.67		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
85	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M		Rif. cmb
		kN					kN				kN		kN m		
ok	0.07	-2.5		21	7.85e-05		-0.2		25	0.38	-3485.0		-1.348e+05		20

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
9	0.11	0.21	0.0	46,40,0	8.74e-04	0.08	0.13	15,41,40	0.0	0	0.96	0.05	0.95
	0.02	0.01	0.0	33,32,0	8.13e-04	0.07	0.06	20,34,35			1.00	0.04	0.96
12	0.11	0.21	0.0	46,40,0	4.06e-04	0.08	0.13	43,41,40	0.0	0	0.96	0.05	0.95
...													
633	0.04	0.03	0.0	39,42,0	1.89e-04	0.09	0.07	43,39,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.22	0.25	0.0		0.02	0.72	0.67		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
87	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN					kN	kN m	
ok	0.0	0.0		0	0.0	0.0		0		0.0	0.0		0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
99	0.05	0.04	0.0	40,42,0	3.09e-03	0.26	0.26	31,32,37	0.0	0	0.88	0.05	0.95
	0.20	0.16	0.0	37,36,0	5.52e-03	0.55	0.38	36,37,36			1.00	0.04	0.96
107	0.05	0.04	0.0	32,34,0	1.34e-03	0.10	0.10	36,32,34	0.0	0	0.88	0.05	0.95
...													
776	0.15	0.13	0.0	36,33,0	2.21e-03	0.40	0.21	38,36,38	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.20	0.16	0.0		5.52e-03	0.55	0.38		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
88	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
ok	0.09	kN -3.2		30	5.54e-04	kN 1.8		27	0.07	kN -1215.2	kN m 2.291e+04		46
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
309	0.03	0.04	0.0	46,43,0	5.26e-03	0.03	0.04	46,43,43	0.0	0	0.91	0.05	0.95
	0.04	0.03	0.0	13,13,0	2.49e-03	0.18	0.18	42,45,44			1.00	0.04	0.96
1287	0.01	0.02	0.0	43,46,0	1.27e-03	0.03	0.04	46,43,46	0.0	0	0.91	0.05	0.95
...													
1311	0.02	0.01	0.0	43,43,0	1.26e-03	0.07	0.06	46,43,43	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.08	0.0		5.84e-03	0.21	0.18		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
90	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN				kN				kN		kN m	
ok	0.17	-6.4		21	1.28e-03	-4.4		1	0.15	-2799.2		-5.948e+04	20
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
124	0.09	0.10	0.0	32,33,0	3.39e-03	0.08	0.07	38,40,42	0.0	0	0.96	0.05	0.95
	0.06	0.05	0.0	40,41,0	1.26e-03	0.15	0.09	18,39,42			1.00	0.04	0.96
132	0.08	0.08	0.0	32,33,0	6.35e-03	0.19	0.18	36,32,33	0.0	0	0.96	0.05	0.95

1651	0.02	0.01	0.0	21,20,0	1.39e-03	0.05	0.04	18,46,43	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.16	0.12	0.0		0.01	0.63	0.55		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
92	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.18	16.5	34	1.35e-03	3.3	38	0.02	-2319.1	2.175e+04	41

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
544	8.12e-03	0.03	0.0	19,1,0	8.50e-04	0.04	0.05	18,19,22	0.0	0	0.96	0.05	0.95
	0.01	0.01	0.0	20,21,0	6.47e-04	0.03	0.01	18,20,21			1.00	0.04	0.96
548	8.12e-03	0.03	0.0	19,1,0	8.50e-04	0.04	0.05	18,19,22	0.0	0	0.96	0.05	0.95
...													
1429	0.01	4.72e-03	0.0	17,20,0	1.19e-04	0.02	0.01	31,21,15	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.12	0.10	0.0		1.23e-03	0.28	0.07		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
94	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.15	-13.9	33	9.54e-04	-2.0	1	0.03	-2293.1	-2.100e+04	11

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
600	0.08	0.07	0.0	34,34,0	9.85e-04	0.09	0.07	40,42,42	0.0	0	0.96	0.05	0.95
	0.01	9.32e-03	0.0	41,40,0	5.41e-04	0.03	8.57e-03	40,43,42			1.00	0.04	0.96
601	0.08	0.07	0.0	34,34,0	5.76e-04	0.09	0.07	41,42,42	0.0	0	0.96	0.05	0.95
...													
1429	0.03	0.02	0.0	21,20,0	1.32e-04	0.05	0.02	43,21,19	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.07	0.0		1.27e-03	0.10	0.09		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
96	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.12	-11.3	33	1.19e-03	-0.6	13	0.10	47.9	-6.755e+04	29

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
441	0.03	0.04	0.0	22,28,0	5.16e-04	0.03	0.04	40,45,44	0.0	0	0.95	0.05	0.95
	0.01	7.89e-03	0.0	9,9,0	2.87e-04	0.03	0.02	32,9,11			1.00	0.04	0.96
444	0.03	0.04	0.0	22,28,0	1.53e-03	0.03	0.04	39,45,44	0.0	0	0.95	0.05	0.95
...													
1438	0.07	0.06	0.0	41,40,0	1.43e-03	0.17	0.07	40,43,43	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.35	0.26	0.0		4.30e-03	0.89	0.29		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
98	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.12	11.3	20	1.62e-03	2.2	32	0.09	-132.0	-5.971e+04	30

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
33	0.01	0.01	0.0	44,44,0	2.56e-04	0.01	0.01	6,29,44	0.0	0	0.94	0.05	0.95

34	0.01	9.10e-03	0.0	5,5,0	1.82e-04	0.03	0.01	20,5,5			1.00	0.04	0.96
...	0.01	0.01	0.0	45,44,0	2.33e-04	0.01	0.01	20,29,44	0.0	0	0.94	0.05	0.95
1438	0.01	0.03	0.0	21,5,0	2.06e-04	0.05	0.04	32,5,5	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.07	0.0		7.40e-04	0.16	0.10		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
100	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.05	-2.8	1	1.08e-03	4.7	20	0.28	-4115.7	-1.568e+05	1			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
33	0.06	0.05	0.0	38,35,0	2.85e-03	0.07	0.06	36,38,35	0.0	0	0.92	0.05	0.95
	3.42e-03	6.64e-03	0.0	33,11,0	8.69e-04	0.03	0.03	36,34,34			1.00	0.04	0.96
34	0.06	0.05	0.0	38,35,0	5.77e-04	0.07	0.06	32,38,35	0.0	0	0.92	0.05	0.95
...													
621	0.05	0.03	0.0	11,37,0	8.49e-04	0.12	0.02	1,11,1	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.22	0.20	0.0		0.03	0.94	0.87		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
102	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.11	4.2	20	2.01e-03	-5.1	5	0.59	-2949.1	1.269e+05	9			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
441	3.07e-03	0.04	0.0	44,45,0	3.84e-04	0.04	0.05	5,44,42	0.0	0	0.94	0.05	0.95
		0.02	0.0	6,9,0	2.71e-04	0.01	0.01	5,6,42			1.00	0.04	0.96
444		0.04	0.06	0.0	44,45,0	1.81e-03	0.04	0.05	19,44,42	0.0	0	0.94	0.05
...													
598	0.32	0.23	0.0	40,41,0	4.36e-03	0.81	0.23	44,44,45	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.32	0.23	0.0		9.44e-03	0.81	0.23		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
104	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.12		-9.1	21	1.79e-03		9.0	28	0.35		-4046.3	-2.781e+05	20
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
431	0.02	0.04	0.0	45,11,0	0.01	0.04	0.05	44,45,44	0.0	0	0.94	0.05	0.95
	0.17	0.11	0.0	42,39,0	5.11e-03	0.42	0.19	44,42,44			1.00	0.04	0.96
432	0.01	0.03	0.0	45,1,0	0.01	0.02	0.02	44,45,11	0.0	0	0.94	0.05	0.95
...													
517	0.20	0.13	0.0	42,39,0	2.16e-03	0.47	0.13	42,42,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.23	0.18	0.0		0.01	0.60	0.27		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
107	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.05	2.6	42	5.96e-04	0.9	10	0.19	-1052.8	-7.791e+04	39

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
227	0.01	0.04	0.0	24,1,0	4.94e-04	0.02	0.04	5,5,5	0.0	0	0.94	0.05	0.95
	2.71e-03	0.01	0.0	46,1,0	1.43e-04	0.02	0.02	5,5,5			1.00	0.04	0.96
235	0.02	0.05	0.0	6,5,0	8.17e-04	0.04	0.06	5,6,5	0.0	0	0.94	0.05	0.95
...													
442	0.06	0.06	0.0	20,21,0	4.83e-04	0.14	0.04	9,20,5	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.06	0.07	0.0		1.66e-03	0.14	0.06		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
109	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.05	kN -4.3	30	1.73e-03	kN -12.0	30	0.27	kN -2421.8	kN m 2.712e+05	46

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
59	0.26	0.23	0.0	40,46,0	5.10e-03	0.26	0.24	39,43,46	0.0	0	0.92	0.05	0.95
	5.89e-03	0.02	0.0	1,1,0	1.24e-03	0.03	0.02	46,1,46			1.00	0.04	0.96
61	0.19	0.17	0.0	44,46,0	5.33e-03	0.20	0.19	39,43,46	0.0	0	0.92	0.05	0.95
...													
658	0.20	0.12	0.0	42,40,0	2.57e-03	0.49	0.07	1,44,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.36	0.29	0.0		0.01	0.50	0.30		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
111	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.03	kN 1.9	44	7.55e-04	kN 3.3	28	0.32	kN -2575.7	kN m -1.885e+05	28

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
42	0.24	0.20	0.0	45,44,0	4.32e-03	0.26	0.23	45,45,39	0.0	0	0.92	0.05	0.95
	8.00e-03	0.03	0.0	12,1,0	1.22e-03	0.04	0.04	44,11,43			1.00	0.04	0.96
43	0.24	0.20	0.0	45,44,0	2.19e-03	0.26	0.23	39,45,39	0.0	0	0.92	0.05	0.95
...													
195	0.21	0.13	0.0	42,42,0	5.74e-03	0.53	0.38	1,42,1	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.33	0.32	0.0		0.02	0.53	0.38		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
113	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.0	kN 0.0	0	0.0	kN 0.0	0	0.0	kN 0.0	kN m 0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
201	0.02	0.02	0.0	19,22,0	1.20e-03	0.03	0.04	21,19,22	0.0	0	0.80	0.06	0.94
	0.02	0.02	0.0	22,22,0	5.91e-04	0.08	0.08	21,20,20			1.00	0.04	0.96
220	0.10	0.08	0.0	19,22,0	2.67e-03	0.09	0.10	17,19,22	0.0	0	0.80	0.06	0.94
...													
383	0.02	0.04	0.0	20,1,0	7.22e-04	0.12	0.13	20,20,20	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.10	0.08	0.0		8.12e-03	0.47	0.43		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
115	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
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	ok	0.14	kN 12.2	40	1.15e-03	kN -1.6	45	0.17	kN -2295.6	kN m 1.430e+05	44		
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
105	0.08	0.07	0.0	40,41,0	1.08e-03	0.09	0.08	42,40,46	0.0	0	0.96	0.05	0.95
	0.01	0.02	0.0	17,22,0	6.98e-04	0.04	0.01	42,22,22			1.00	0.04	0.96
112	0.08	0.07	0.0	40,41,0	6.68e-04	0.09	0.08	46,40,46	0.0	0	0.96	0.05	0.95
...													
1413	0.01	8.34e-03	0.0	39,40,0	1.11e-04	0.03	0.02	19,19,22	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.07	0.0		1.27e-03	0.17	0.10		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
117	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.13	kN 9.9	40	1.03e-03	kN 2.5	44	0.15	kN -2037.7	kN m 8.502e+04	13			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
73	0.02	0.03	0.0	44,45,0	3.05e-03	0.05	0.05	40,44,36	0.0	0	0.96	0.05	0.95
	0.10	0.11	0.0	43,46,0	1.87e-03	0.29	0.16	40,46,40			1.00	0.04	0.96
82	0.04	0.04	0.0	40,41,0	3.05e-03	0.05	0.05	40,44,36	0.0	0	0.96	0.05	0.95
...													
1413	0.06	0.04	0.0	39,42,0	6.83e-04	0.13	0.05	44,39,42	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.11	0.0		3.05e-03	0.37	0.16		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
118	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN					kN				kN	kN m	
ok	0.11		-4.2	21	2.67e-03			6.8	1	0.14		-1657.9	3.368e+04	21
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
80	0.06	0.08	0.0	40,41,0	2.06e-03	0.08	0.09	20,44,45	0.0	0	0.96	0.05	0.95	
	0.01	9.18e-03	0.0	20,18,0	1.53e-03	0.03	0.02	20,40,41			1.00	0.04	0.96	
92	0.02	0.03	0.0	37,36,0	5.35e-03	0.08	0.08	39,34,39	0.0	0	0.96	0.05	0.95	
....														
1122	0.03	0.02	0.0	19,22,0	1.98e-03	0.05	0.04	31,15,44	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.06	0.08	0.0		5.35e-03	0.08	0.09		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
122	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
66	0.11	0.08	0.0	40,41,0	2.87e-03	0.13	0.12	41,39,41	0.0	0	0.88	0.05	0.95
	0.15	0.14	0.0	46,46,0	1.99e-03	0.43	0.21	41,46,46			1.00	0.04	0.96
96	0.07	0.05	0.0	39,42,0	5.32e-03	0.08	0.08	41,45,39	0.0	0	0.88	0.05	0.95
...													
1738	0.15	0.14	0.0	46,46,0	2.75e-03	0.43	0.21	46,46,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.21	0.18	0.0		0.02	0.74	0.65		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
124	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		m	
ok	0.15	11.2		20	1.19e-03		-3.9		1	0.20	-3381.6		-1.451e+05	20
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
492	0.12	0.13	0.0	45,44,0	1.07e-03	0.14	0.13	45,45,45	0.0	0	0.96	0.05	0.95	
	0.27	0.21	0.0	45,45,0	4.93e-04	0.71	0.12	45,45,45			1.00	0.04	0.96	
686	0.12	0.11	0.0	44,45,0	1.12e-03	0.13	0.12	40,44,45	0.0	0	0.96	0.05	0.95	
...														
1719	0.07	0.06	0.0	45,44,0	2.22e-03	0.23	0.20	44,45,44	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.27	0.21	0.0		6.47e-03	0.71	0.42		0.0					

Setto	Mat.							N. strati	Spessore	Incoll.	Stato
									cm		
126	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
		kN			kN			kN	kN m	
ok	0.18	-13.3	21	6.63e-04	-1.8	1	0.02	-2542.3	-1.520e+04	5

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
73	0.04	0.04	0.0	44,45,0	4.77e-03	0.08	0.07	42,44,45	0.0	0	0.96	0.05	0.95
	0.11	0.08	0.0	39,46,0	3.53e-03	0.32	0.27	41,45,44			1.00	0.04	0.96
83	0.04	0.04	0.0	44,44,0	5.34e-03	0.07	0.07	46,40,44	0.0	0	0.96	0.05	0.95
...													
1167	0.11	0.08	0.0	39,46,0	3.53e-03	0.32	0.27	41,45,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.13	0.10	0.0		7.40e-03	0.36	0.36		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
127	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.0	0.0		0	0.0		0.0		0	0.0	0.0		0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
197	0.14	0.11	0.0	45,44,0	0.02	0.21	0.34	44,45,44	0.0	0	0.30	0.14	0.86
	9.65e-04	0.01	0.0	39,1,0	3.02e-03	0.03	0.04	44,44,44			1.00	0.04	0.96
683	0.14	0.11	0.0	45,44,0	0.02	0.21	0.34	44,45,44	0.0	0	0.30	0.14	0.86
...													
1719	1.99e-03	0.01	0.0	45,11,0	1.19e-03	0.04	0.05	1,46,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.11	0.0		0.02	0.23	0.34		0.0				

Setto	Mat.	N. strati						Spessore	Incoll.	Stato			
								cm					
130	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5						13.7	SI	ok			
V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
147	0.03	0.03	0.0	41,40,0	0.01	0.21	0.24	44,41,40	0.0	0	0.30	0.14	0.86
	0.04	0.04	0.0	42,42,0	1.74e-03	0.11	0.07	44,42,1			1.00	0.04	0.96
149	0.03	0.03	0.0	41,40,0	0.01	0.21	0.24	44,41,40	0.0	0	0.30	0.14	0.86
...													
1710	0.10	0.09	0.0	42,42,0	0.01	0.59	0.55	39,39,39	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.10	0.09	0.0		0.01	0.59	0.55		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
131	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.22	16.0	20	5.90e-04	0.8	28	0.05	-3587.9	-4.126e+04	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
73	9.65e-03	0.02	0.0	40,1,0	4.61e-03	0.06	0.06	40,44,44	0.0	0	0.96	0.05	0.95
	0.12	0.08	0.0	39,43,0	2.30e-03	0.31	0.18	40,39,45			1.00	0.04	0.96
83	0.03	0.04	0.0	42,39,0	4.61e-03	0.10	0.10	40,42,42	0.0	0	0.96	0.05	0.95
...													
1711	0.12	0.08	0.0	39,43,0	3.42e-03	0.31	0.23	42,39,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.30	0.23	0.0		0.01	0.83	0.60		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
132	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.13	-9.8	21	3.37e-04	1.6	27	0.04	-2787.2	-2.400e+04	5

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
162	0.26	0.20	0.0	44,44,0	1.90e-03	0.27	0.22	40,44,44	0.0	0	0.96	0.05	0.95
	0.02	0.02	0.0	40,41,0	5.63e-04	0.06	0.05	20,40,44			1.00	0.04	0.96
164	0.26	0.20	0.0	44,44,0	1.90e-03	0.27	0.22	40,44,44	0.0	0	0.96	0.05	0.95
...													
1480	0.05	0.05	0.0	39,42,0	6.42e-04	0.14	0.12	46,39,42	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.26	0.20	0.0		0.02	0.78	0.71		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
135	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.14	-10.2	22	4.31e-04	2.3	27	0.20	-6428.6	1.708e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
202	0.15	0.12	0.0	43,43,0	2.31e-03	0.26	0.22	43,46,43	0.0	0	0.96	0.05	0.95
	0.19	0.14	0.0	42,40,0	6.03e-03	0.51	0.40	46,42,46			1.00	0.04	0.96
203	0.35	0.27	0.0	40,42,0	5.60e-03	0.44	0.39	41,45,41	0.0	0	0.96	0.05	0.95
...													
675	0.02	0.02	0.0	39,42,0	1.90e-04	0.05	0.03	22,39,13	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.35	0.27	0.0		6.03e-03	0.59	0.40		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
136	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
231	0.11	0.07	0.0	42,40,0	2.74e-03	0.19	0.12	39,42,40	0.0	0	0.88	0.05	0.95
	0.12	0.10	0.0	41,39,0	3.08e-03	0.34	0.25	43,43,43			1.00	0.04	0.96
232	0.11	0.08	0.0	46,46,0	5.01e-03	0.20	0.20	46,40,40	0.0	0	0.88	0.05	0.95
...													

1675	0.03	0.03	0.0	44,42,0	2.13e-03	0.09	0.04	46,42,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.15	0.13	0.0		0.01	0.56	0.52		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
138	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.09	7.0	42	1.25e-03	3.0	42	0.20	-3699.7	-1.857e+05	41

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1234	0.02	0.02	0.0	44,5,0	2.11e-03	0.06	0.05	5,42,42	0.0	0	0.96	0.05	0.95
	0.06	0.04	0.0	45,44,0	6.34e-04	0.13	0.02	5,45,44			1.00	0.04	0.96
1382	0.18	0.17	0.0	6,5,0	3.71e-03	0.26	0.24	5,6,5	0.0	0	0.96	0.05	0.95
...													
1682	0.06	0.04	0.0	45,44,0	6.53e-04	0.13	0.03	6,45,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.30	0.23	0.0		7.16e-03	0.79	0.33		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
140	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.10	-9.2	39	1.05e-03	-2.2	1	0.02	-1787.8	-1.472e+04	11

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1349	0.15	0.12	0.0	6,5,0	4.97e-04	0.14	0.11	42,6,5	0.0	0	0.96	0.05	0.95
	0.02	0.02	0.0	6,5,0	2.58e-04	0.06	0.01	39,6,5			1.00	0.04	0.96
1350	0.15	0.12	0.0	6,5,0	4.13e-04	0.14	0.11	42,6,5	0.0	0	0.96	0.05	0.95
...													
1599	0.07	0.05	0.0	5,6,0	1.91e-04	0.17	0.04	5,5,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.15	0.12	0.0		5.89e-04	0.17	0.11		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
142	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.09	-8.5	45	5.16e-04	0.2	44	0.04	-4010.5	3.838e+04	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
419	0.03	0.05	0.0	6,5,0	8.75e-04	0.06	0.07	5,6,5	0.0	0	0.95	0.05	0.95
	3.98e-03	2.19e-03	0.0	20,21,0	2.90e-04	0.05	0.04	5,5,6			1.00	0.04	0.96
421	0.03	0.05	0.0	6,5,0	1.58e-03	0.06	0.07	5,6,5	0.0	0	0.95	0.05	0.95
...													
1625	0.24	0.23	0.0	6,5,0	2.02e-03	0.67	0.19	1,6,5	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.24	0.23	0.0		7.58e-03	0.67	0.34		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
145	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.11	10.4	1	2.04e-03	2.9	1	0.09	-331.0	5.963e+04	45

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
104	0.03	0.03	0.0	6,5,0	6.47e-04	0.02	0.02	5,6,5	0.0	0	0.94	0.05	0.95

108	0.03	0.03	0.0	6,5,0	3.83e-04	0.09	0.02	5,6,5			1.00	0.04	0.96
...	0.02	0.03	0.0	6,5,0	7.51e-04	0.02	0.02	5,6,5	0.0	0	0.94	0.05	0.95
1639	0.02	0.02	0.0	6,5,0	3.21e-04	0.06	0.02	5,6,5	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.07	0.06	0.0		1.51e-03	0.20	0.06		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
146	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
749	0.09	0.08	0.0	42,46,0	7.94e-03	0.13	0.24	46,44,46	0.0	0	0.27	0.16	0.84
	0.03	0.03	0.0	44,45,0	1.23e-03	0.08	0.08	46,44,44			1.00	0.04	0.96
1301	0.04	0.04	0.0	43,46,0	7.94e-03	0.08	0.13	46,44,46	0.0	0	0.27	0.16	0.84
...													
1529	0.06	0.07	0.0	45,39,0	9.26e-04	0.18	0.10	43,45,13		0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.08	0.0		7.94e-03	0.20	0.24		0.0				

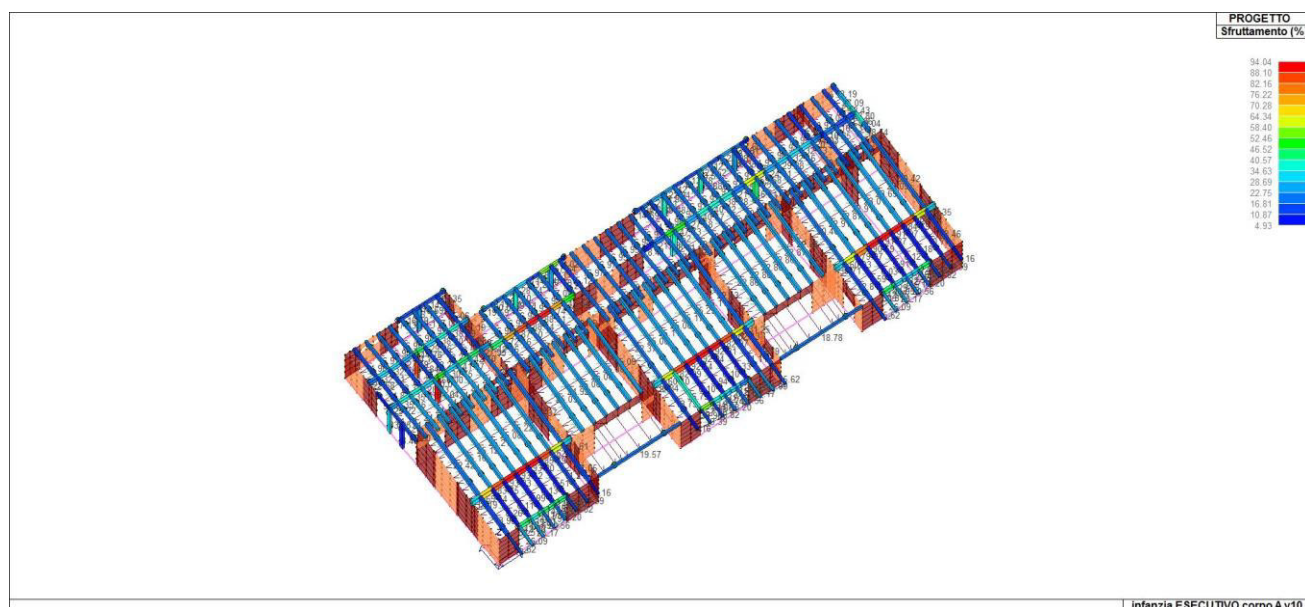


Fig.4 Sfruttamento %

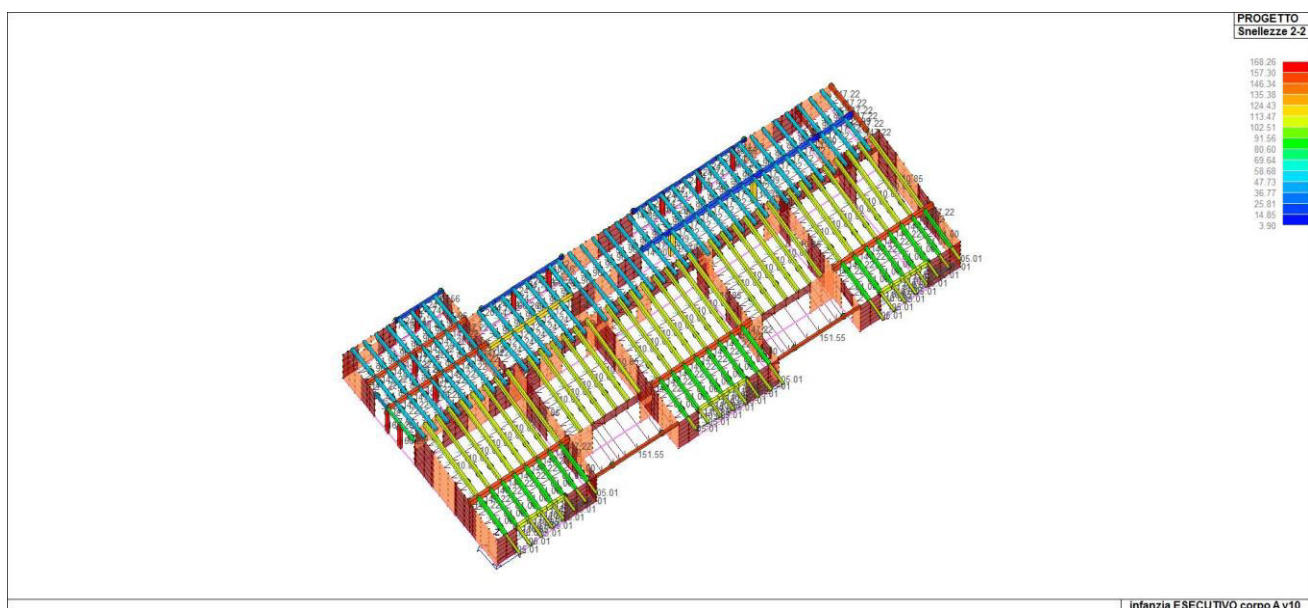


Fig.5 Snellezza Adimensionale 2-2

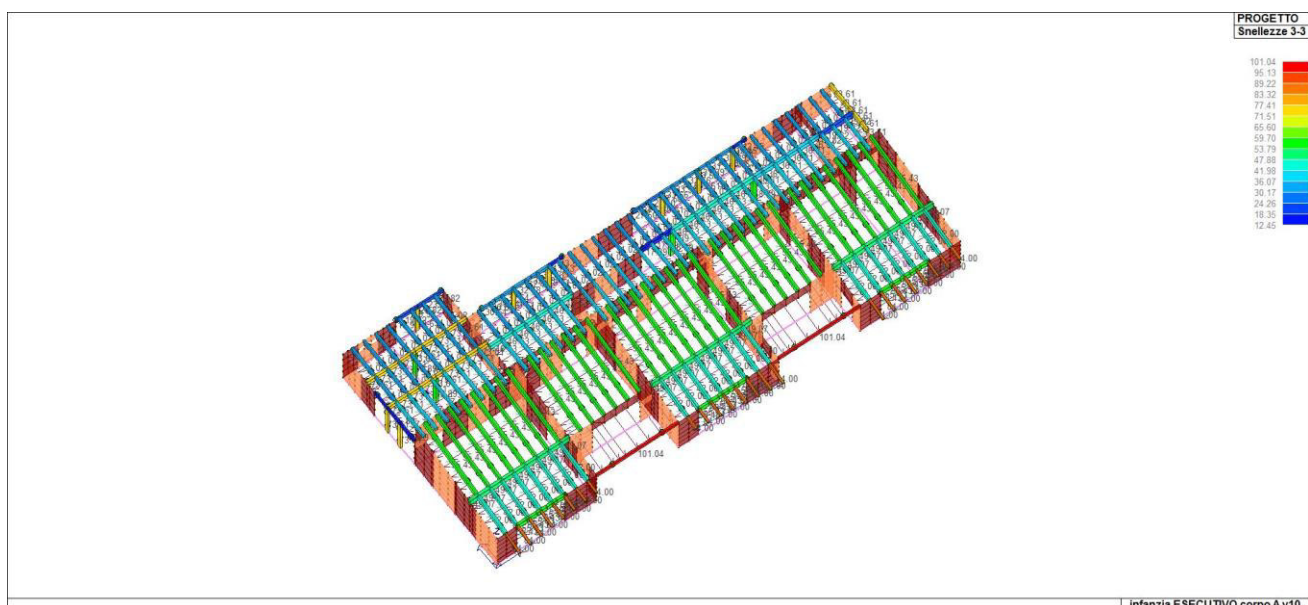


Fig.6 Snellezza Adimensionale 3-3